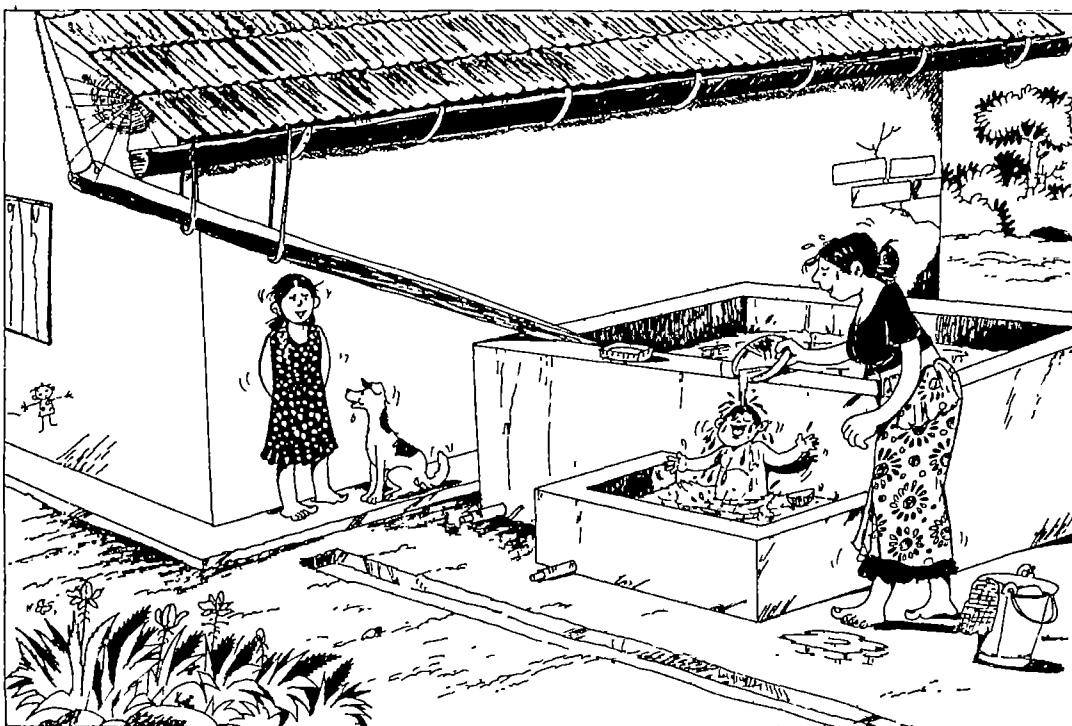


CWSSP

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ACTION RESEARCH STUDY ON RAIN WATER HARVESTING



Project Report 2

Community Water Supply & Sanitation Project
Ministry of Housing, Construction & Public Utilities



INGEKOMEN - 3 NOV. 1995

C W S S P

- The Community Water Supply and Sanitation Project is an initiative of the Government of Sri Lanka with the support of the World Bank.
- The CWSS Programme Unit located within the Ministry of Housing, Construction & Public Utilities coordinates the project. The Regional Directorates in Badulla, Matara and Ratnapura, support Partner Organizations and Community Based Organizations in implementing their projects.
- CWSSP supports improvements in water supply and sanitation for approximately 650,000 rural people in 2,500 villages and 17 small towns in Badulla, Matara, Ratnapura and Monaragala Districts.
- Some 1600 schools in these districts will be eligible for support to improve personal hygiene through school water supply and sanitation, and hygiene education.
- CWSSP works with over 80 partner organizations (NGOs, co-operatives, government and quasi-government bodies) to support, motivate, organize and train communities to implement and manage their own water supply and sanitation schemes.

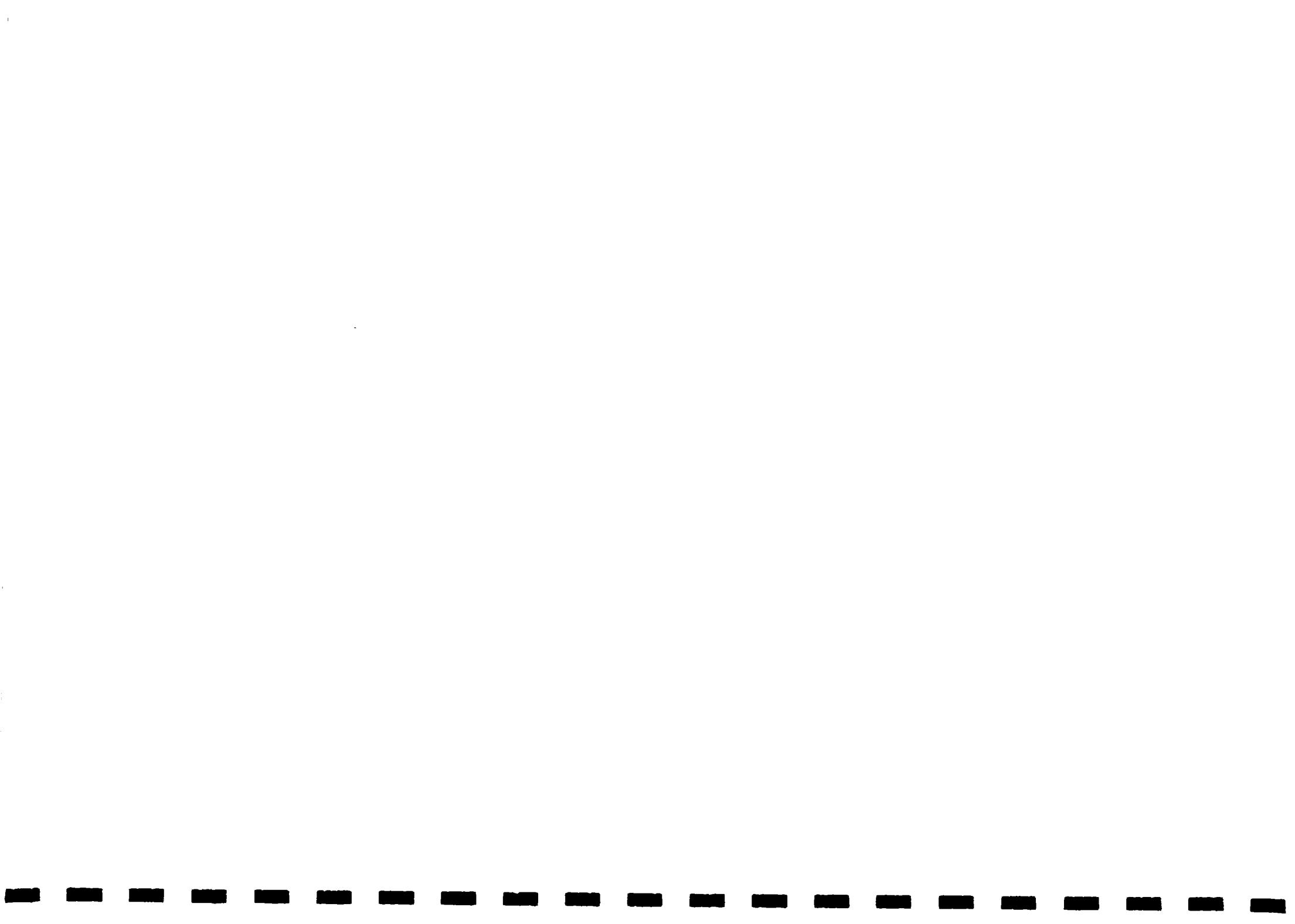
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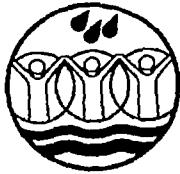
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CWSSP

ACTION RESEARCH STUDY ON RAIN WATER HARVESTING

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Project Report 2

Community Water Supply & Sanitation Project
Ministry of Housing, Construction & Public Utilities

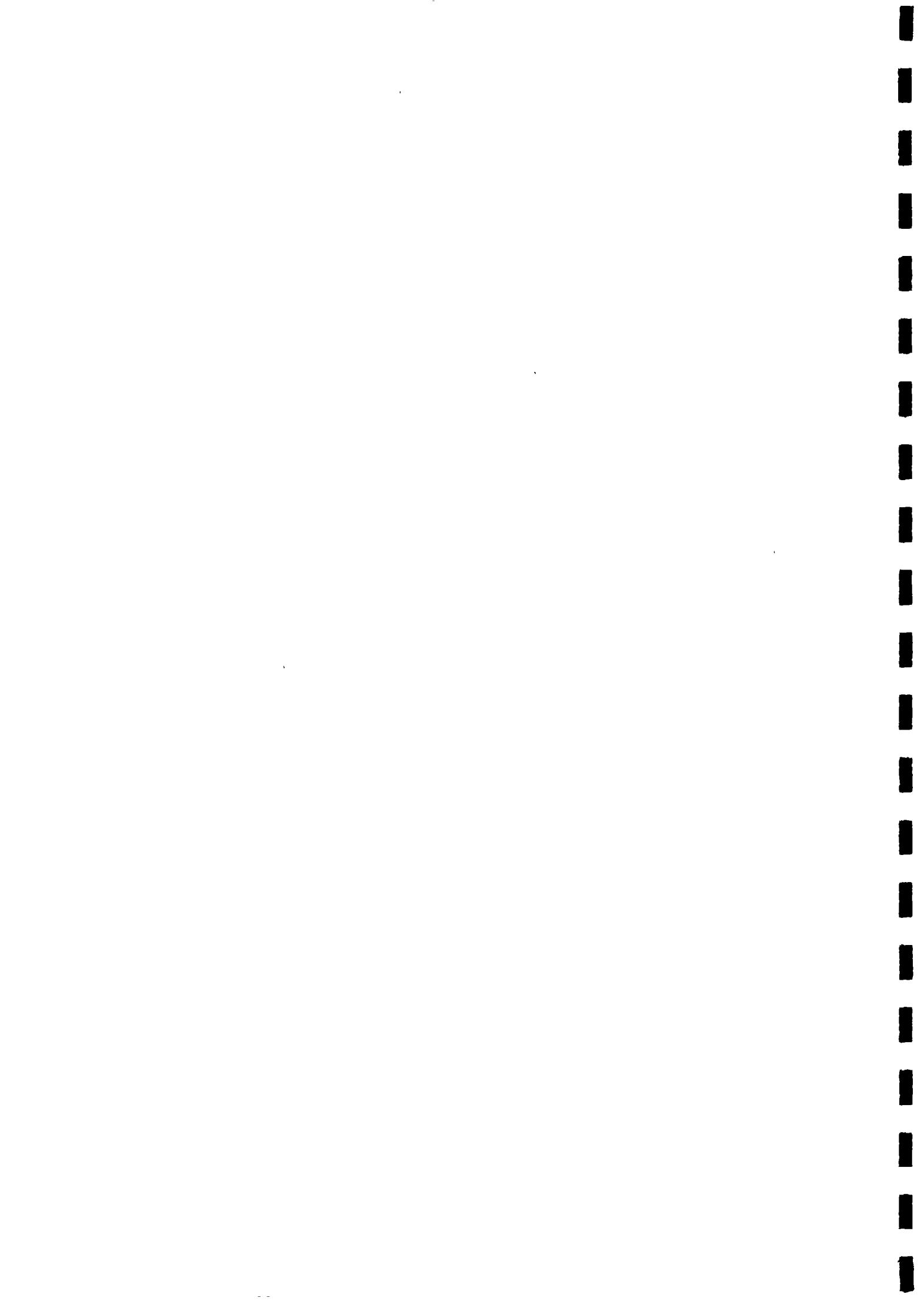


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C	-	Kolonne]	
D	-	Ratnapura (City)]	Ratnapura District
E	-	Ambilipitiya]	
F	-	Kekenadora	}	
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Q	-	Haputale	}	Badulla District
T	-	Ratnapura (City)]	
O	-	Ambilipitiya]	Ratnapura District
S	-	Kekenadora]	
P	-	AninKanda	}	Matara District



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- | | | | | |
|---|---|------------------|---|--------------------|
| X | - | Badulla (City) | } | |
| W | - | Haputale | } | Badulla District |
| Z | - | Ratnapura (City) |] | |
| U | - | Ambilipitiya |] | Ratnapura District |
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Abbreviations

CBO	<i>Community Based Organization</i>
CRO	<i>Community Relations Officer</i>
CRO/T	<i>Community Relations/Technical Officer</i>
CWSSP	<i>Community Water Supply & Sanitation Project</i>
DD/T	<i>Deputy Director/Technical</i>
G.I.	<i>Galvanized Iron</i>
ITDG	<i>International Technology Development Group</i>
LPCD	<i>Liters per capita per day</i>
M ³	<i>Cubic Meter</i>
NERD	<i>National Engineering Research and Development Centre</i>
PO	<i>Partner Organization</i>
PVC	<i>Poly Vinyl Chlorine</i>
Qty	<i>Quantity</i>
R.C.	<i>Run off coefficient</i>
R.F.	<i>Rain Fall</i>
Rs	<i>Sri Lanka Rupees (IRS = 0.02 US\$ in June 95)</i>
TO	<i>Technical Officer</i>
TSC	<i>Technical Support Cell</i>
UV	<i>Ultra Violet</i>



1. Abstract

Rain water harvesting is becoming an important option for underserved households and communities in Sri Lanka. Many areas in Sri Lanka offer a good potential for the introduction of rainwater harvesting, however as many people do not appreciate the potential of rainwater harvesting for domestic and drinking water purpose this technology is undervalued.

A policy for the Community Water Supply and Sanitation Project is formulated to enhance the application of rain water harvesting methods.

In rain water harvesting reliability of the supply depends on the size of the catchment area - often the roof -, the volume of the storage tank and the management of the daily consumption, all in relation to the local rainfall pattern. The study attempts to develop a suitable technical and economical solution to the storage of drinking water, and as a result proposes brick dome and ferrocement as the two most economical options.

Quality of rain water in storage is addressed on the basis of a literature study. Maps are provided indicating areas of high suitability for rain water harvesting.

Recommendations are given in respect of further trials and field level monitoring. Promotion and awareness raising for greater appreciation of rain water harvesting is advocated.



2. Preface

This report has been drafted in the framework of the World Bank financed Community Water Supply & Sanitation Project, executed by the Ministry of Housing, Construction & Public Utilities, Sri Lanka.

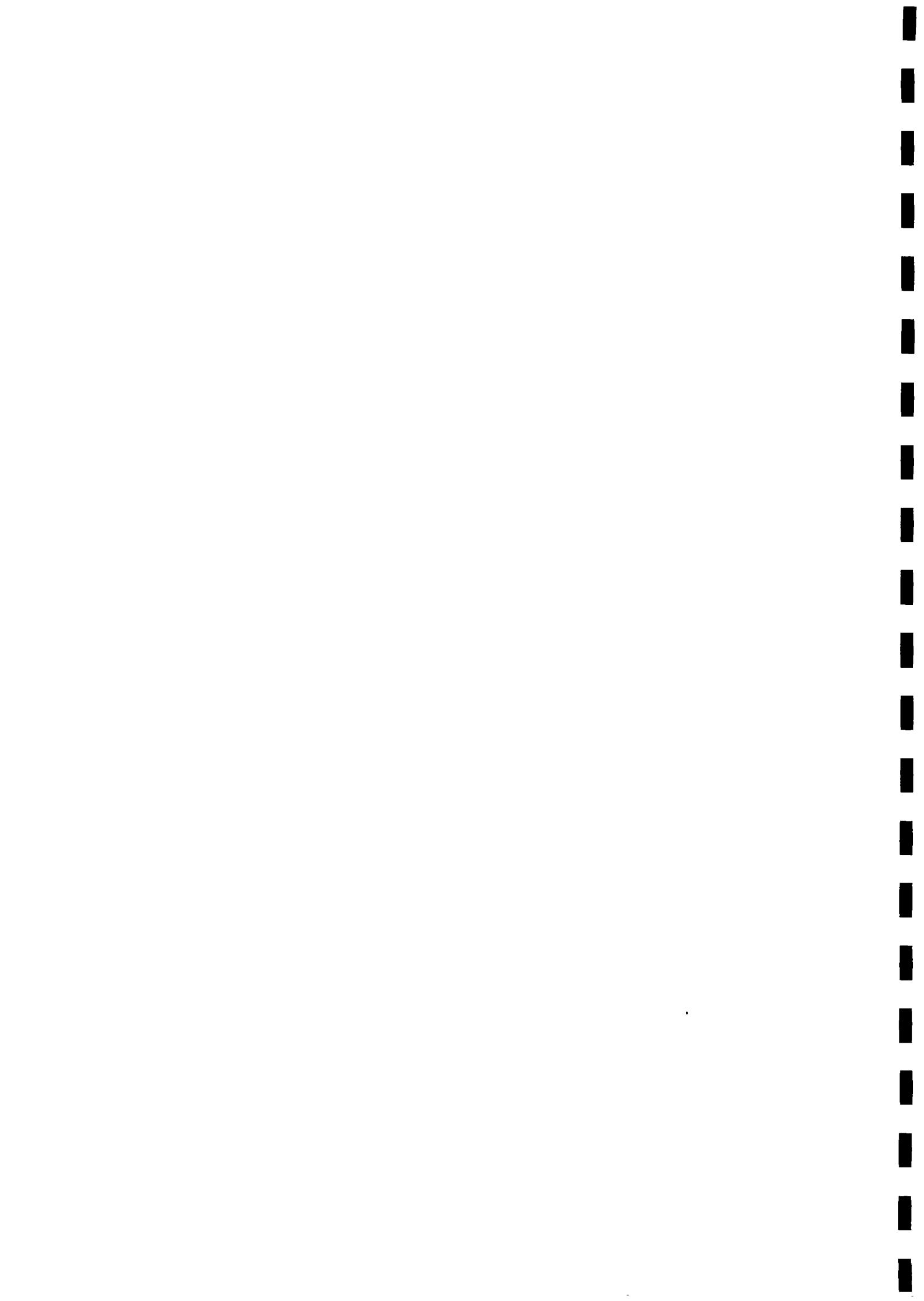
The need to assess the feasibility of rainwater harvesting as an water supply option specially for low income households located at places where no other viable option is available, has always existed. It is an appropriate time to do this study as a number of water supply schemes under CWSSP with no traditional options, continue to increase.

Given the time frame of just three months for the preparation of this report including trial construction at places upto 200 km away from the Head Office and the limited office facilities, some issues may not be dealt with in sufficient depth. Future studies may be able to correct any such deficiencies.

Numerous persons were involved with the study and their friendly response and cooperation significantly contributed to the formulation of this report. They include the TSC Manager Mr. Han Heijnen and the staff of CWSSP at Head Office, Regional Offices in Matara, Badulla and Ratnapura and the NERD Centre, Ja-Ela.

The co-operation of UNICEF, ITDG, SARVODAYA, the Faculty of Engineering Peradeniya, Residents of Rahaspokuna, Mr. Pigera of Bandarawela, Residents of Iriyagama and the Principal of Paradise School Ratnapura need special mention. The consultant is deeply indebted to all of them.

A special thank you to Ms. Samanthika de Silva for computer analyzing the data and typing the report.



3. Executive Summary

Introduction

An Action Research Study on Rain Water Harvesting was commissioned in January 1995 by CWSSP as part of its Research and Documentation Program.

Rainwater Harvesting appears to be the only option remaining for a number of water supply schemes, under CWSSP with no traditional options. This applies to all three districts where CWSSP is working : Matara, Badulla & Ratnapura.

The objective of the study was to design and construct low cost rain water harvesting storage tanks and to gather existing experience in Sri Lanka on rainwater harvesting, in order to investigate the possibility to conduct Pilot Projects to develop recommendations and guidelines for the in-ception of the rain water harvesting option in the CWSSP.

The study comprised of four main steps :

1. Design and construction of trial tanks.
 2. Visits to existing rainwater harvesting places in Sri Lanka.
 3. Field visits to selected pilot project villages.
 4. The collection and analysis of rainfall data.

Status of Rain Water Harvesting in Sri Lanka

Presently there is no planned rainwater harvesting program in Sri Lanka.

Local investigation reveals :

- that rainwater harvesting for domestic consumption is currently in practice in Sri Lanka.
 - that a section of potential consumers are looking for appropriate technology to harvest and store rain water.
 - that a section of potential consumers are not sure about rainwater harvesting. They are concerned about the quality and reliability of rain water.

Rain Water Harvesting as an Option

Technical potential for rain water harvesting exists every where in the island where a suitable catchment is available.

Economic feasibility varies from place to place. It is a reasonable option where,

- Water bills are high



- Traditional technical options are not economically feasible.
- Operation and maintenance of traditional methods are a major concern.

In the CWSSP rainwater harvesting is specially relevant in some 30% of the total projected project coverage where tube wells and pump systems are, envisaged, or in areas high up in the hills where there are no springs.

Various Technical Options Tested

- CWSSP criteria on rainwater collecting tanks system requires that a five cubic meter tank be built to cost below Rs. 5,400/- excluding unskilled labour.

Three types of storage tanks were studied:

<u>Type</u>	<u>Capacity</u>
Brick Dome	5M ³
Ferro-Cement	5M ³
Cement Jar	1M ³

These were designed and constructed. Construction indicates that :

- The brick dome tank can be constructed to meet this criteria.
- The ferro cement tank constructed, using the cost lowering method, was successful in bringing the standard cost of a 5m³ ferro cement tank down by a impressive 50%. It is anticipated that with a few more trials the cost could be brought down further to meet CWSSP criteria, by reducing skill labour time.



COMPARISON OF DIFFERENT TANKS

Type of Tank	Total Cost/ M ³ (1995) Rs.	Advantages	Disadvantages	Rural Level Construction
Brick Dome	1318	<ul style="list-style-type: none"> - Can be built to any capacity from 2 - 10M³ - Can easily be maintained & repaired at rural level. - Dome roof prevents contamination - Water wasted is minimum due to extraction of water by pump 	<ul style="list-style-type: none"> - Tank is under ground level - Need a pump to extract water - Difficult to empty for cleaning. - Risk of falling in by children, animals, etc. 	<ul style="list-style-type: none"> - With a short training rural masons can build the tanks with locally available material.
Ferro-Cement (Pumpkin Shape)	1468	<ul style="list-style-type: none"> - Can be built upto 5M³ capacity. - Easy to maintain at rural level. - Water is well protected against outside contamination. - Convenient to take water from a gravity fed tap or siphon pipe - Safe for children and animals 	<ul style="list-style-type: none"> - Difficult to built larger than 5M³ - The full tank is visible - Water might get wasted from the tap. 	<ul style="list-style-type: none"> - With the use of a simple low cost mould possible to build at rural level with available materials.
Cement Jar	1874	<ul style="list-style-type: none"> - Easy to maintain & repair at rural level. - Water is well protected against outside contamination. - Safe for children & animals. 	<ul style="list-style-type: none"> - Difficult to built larger than 2M³ capacity. - Need number of jars for a house. - Takes too much ground space to keep. 	<ul style="list-style-type: none"> - Possible to build at rural level, with available material.

Pilot Project

Three places from the three districts were identified to do pilot projects. They are :

Dematawelhinna

- Badulla District

Medawatugoda Upper Sec.

Omalpe

- Ratnapura District

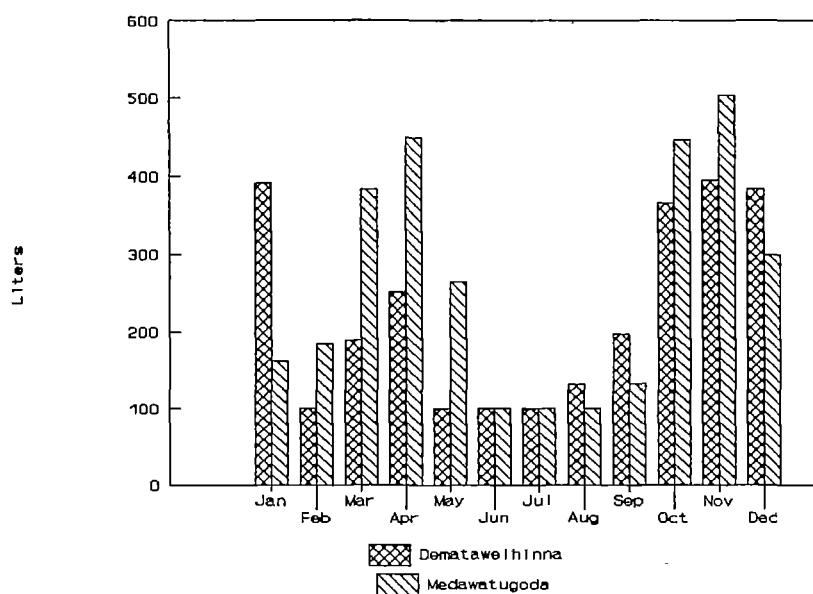
Dorsar Kanda

- Matara District



- At Dematawelhinna and Madawatugoda rainwater harvesting is technically and economically feasible to improve the present status of water supply. However supply per day will be less than 20LPCD from smaller catchment roofs during the dry spell in a ten year dry year. Graphs X and N depicts these scenarios. Bar graphs 3-1 & 3-2 gives the daily supply scenarios, possible from a well managed system consisting of a $60M^2$ (R.C.-0.8) catchment & $5M^3$ storage tank for Dematawelhinna & Madawatugoda respectively in a normal year.

Bar Graph 3.1 & 3.2



- At Dorsarkanda available roofs are mostly covered with thatch and are not suitable for rainwater harvesting. To do rainwater harvesting here suitable catchment must be constructed.

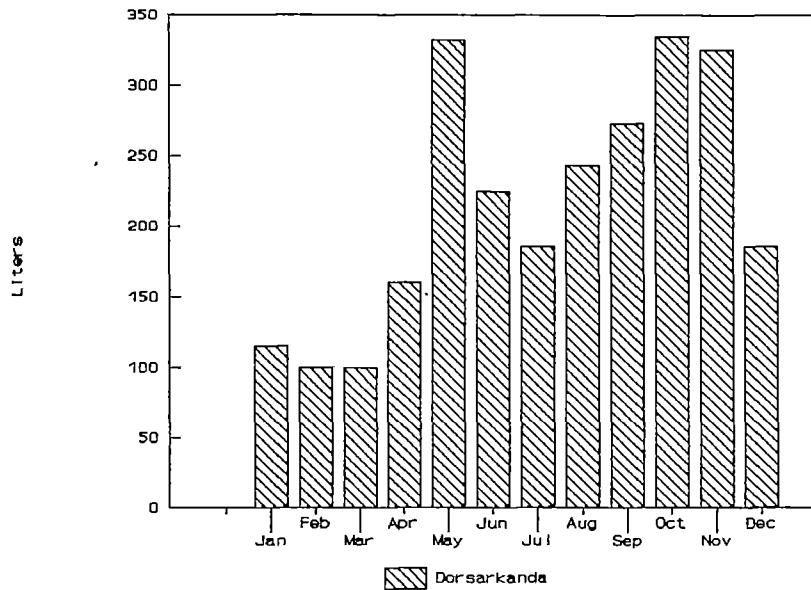
Most householders have taken house-building loans recently and have started to build better houses with permanent roofs, suitable as catchments.

Once suitable catchment is available rainwater harvesting becomes technically and economically feasible to improve the present status of water supply Graph Y gives the dry season supply to the catchment area scenario in a ten year dry year.

Bar graph 3-3 gives the daily supply scenario, possible from a well managed system consisting of a $60M^2$ catchment & $5M^3$ storage tank for Dorsarkanda in a normal year.



Bar Graph 3 3

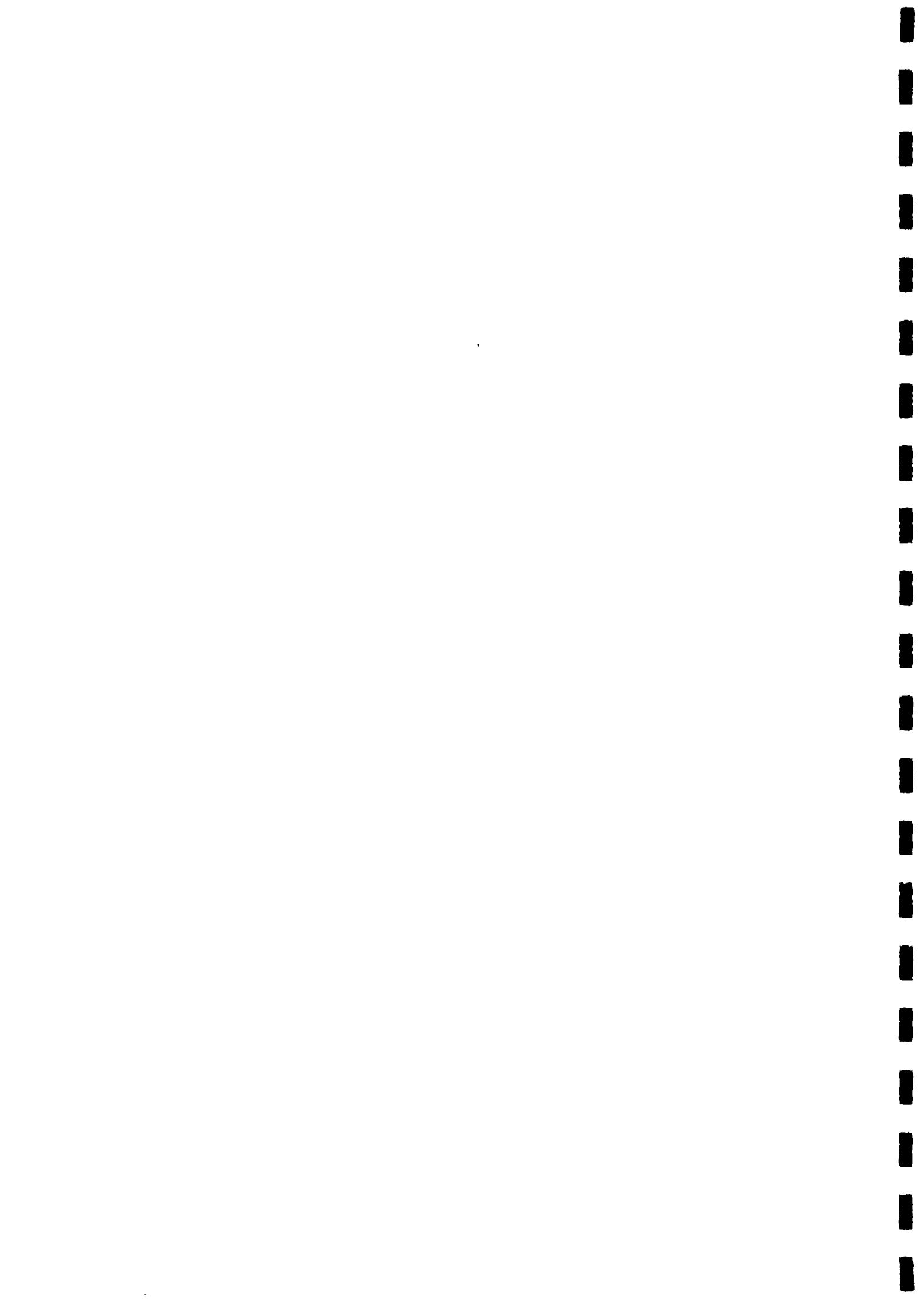


Conclusion and Recommendations

1. There is adequate social acceptance of rainwater harvesting as a source of water in areas, where there is no adequate or sustainable fresh-water source within reasonable distance. However a vast majority of the potential beneficiaries do not understand the full benefits of rainwater harvesting.

It is recommended to conduct an awareness campaign under the CWSSP targeted to potential consumers.

2. The study recommends the design and construction of the three pilot project already identified at Badulla, Ratnapura and Matara. By monitoring these projects after construction, to evaluate the technical economic and social aspects experience can be gained which in turn can be used to train the TO of Partner Organization in design and construction of rainwater harvesting systems.
3. The study recommends continued construction of ferro-cement tanks and Cement Jars with suggested improvements to bring down the cost to fall within the CWSSP cost criteria. These can be done at Regional Level.



4. From literature referred, the study concludes that the rainwater collected off

G.I. Sheet
Clay Tile &
Asbestos

made catchment is suitable for drinking and other domestic purposes. However, the first flush of water after the dry season should be discarded. To avoid any environmental problems, tank should be made mosquito proof.



4. Introduction

The time has come where serious consideration should be given to rainwater harvesting. In the dry zone as well as in the wet zones of Sri Lanka many areas that are potentially suitable for rainwater harvesting remain undeveloped. Rural poor inhabitants of these areas continue to use highly polluted water or suffer from lack of any water, for most basic needs, resulting in high incidence of water related diseases.

At the recommendation of the National Steering Committee, an Action Study on Rain Water Harvesting in Sri Lanka was started by the CWSSP at the end of Jan' 95. It is an appropriate time to do this study as the number of water-supply schemes under CWSSP with no traditional options, continues to increase.

The study involved an investigation phase, focused on obtaining and studying past and current published literature on the subject both local and foreign, and visits to sites where rainwater harvesting is currently practiced in Sri Lanka. Investigations were followed by a note for discussion, giving the preliminary options on rainwater harvesting by the Consultant.

Technical personnel of the CWSSP contributed at the discussion. As a result CWSSP accepted as a policy to :

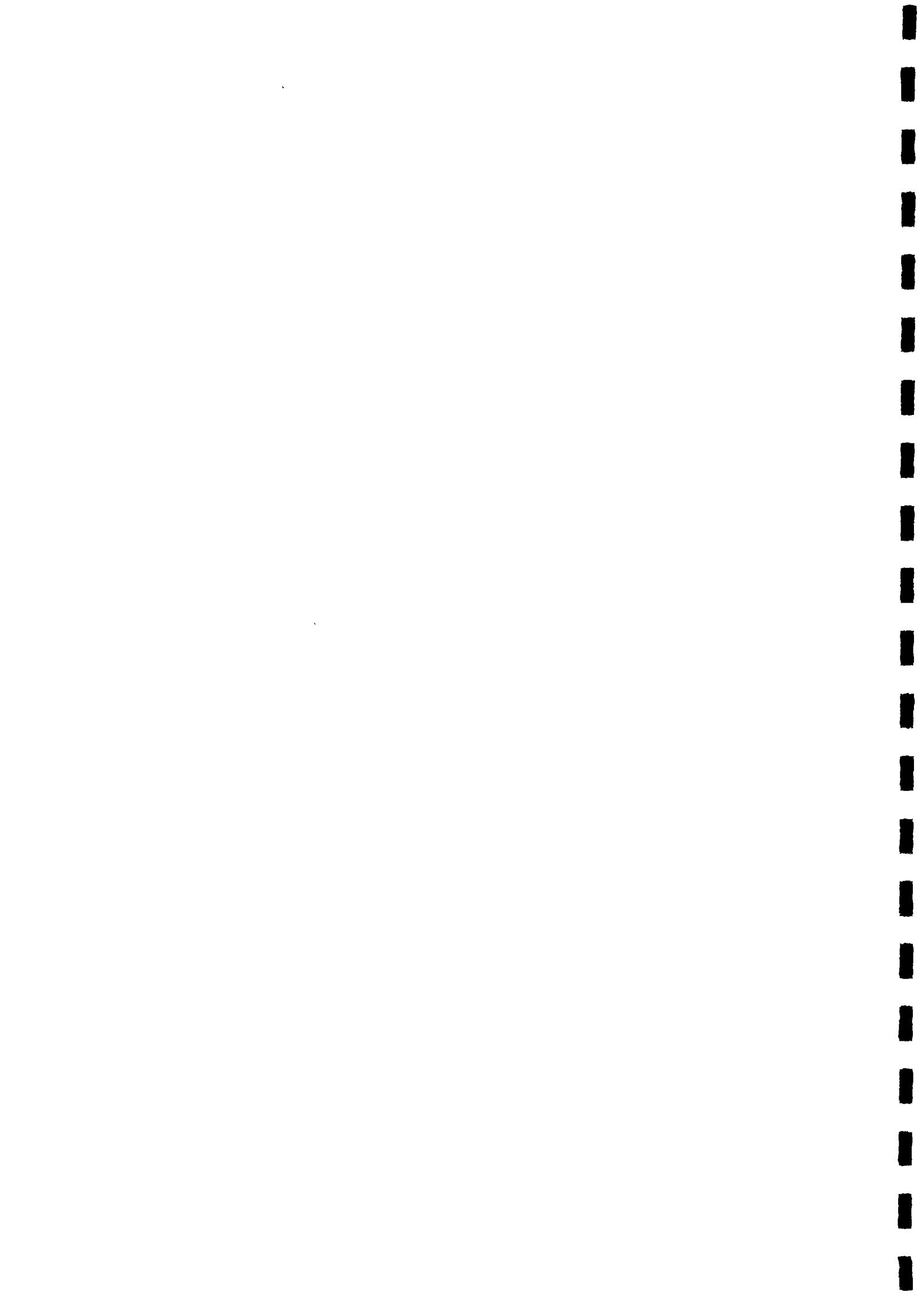
1. promote **rainwater as a domestic supply** where other acceptable sources are not feasible due to technical, maintenance or economic reasons.
2. to ensure that rainwater would prove an acceptable alternative, CWSSP adopted the strategy to improve the existing situation to a reasonable level. i.e. to supply a minimum of **20 lpcd during the dry season.**
3. develop affordable **Rainwater storage tanks**

These strategic considerations and the objectives as stated in the Terms of Reference for the consultant guided the study. (See Annex 1A)

4.1 Purpose

The action research aimed to

1. design and construct a 5 cubic meter storage tank system to cost less than Rs. 5400/- excluding unskilled labour cost.
2. make appropriate recommendations for the incorporation of rainwater harvesting option in the CWSSP.
3. prepare training material so as to transfer skills to CWSSP technical staff.



4.2 Study Area

The study area covers the CWSSP Project area which comprises the Districts of Badulla, Ratnapura and Matara. However, the recommendations could be adapted to any part of Sri Lanka.

4.3 Methodology

The research study comprised of the following steps.

4.3.1 Desk studies

- Preparation of a work plan for the study
- A review of published literature on the subject covering local and foreign sources.
- An analysis of rainfall data.
- Design of tank including preparation of drawings and bill of quantities.
- Study of literature on rain water quality.

4.3.2 Collection of data

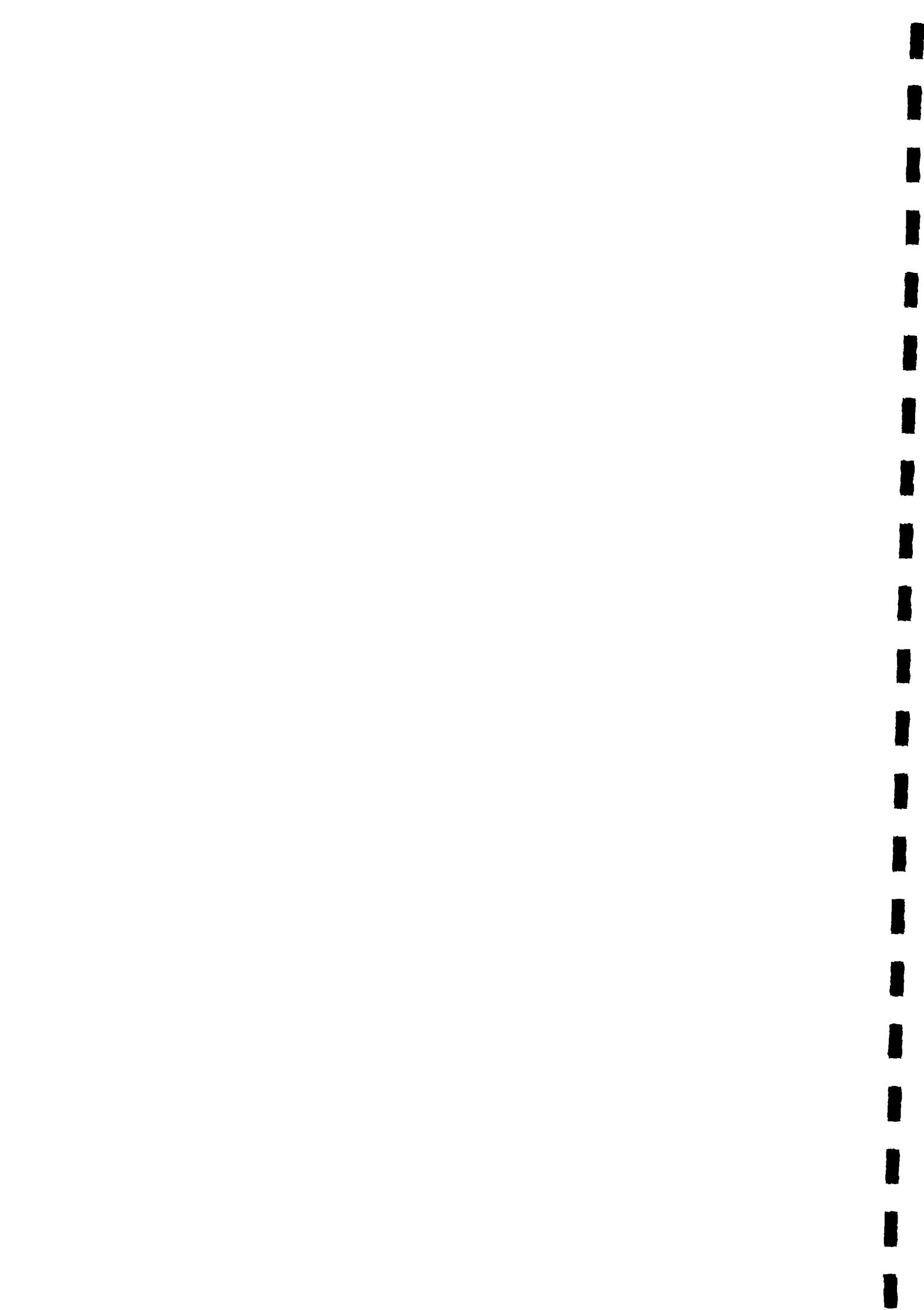
- Collection of data on rainfall from the Meteorological Department Colombo.

4.3.3 Field Visit

- Survey the existing rainwater harvesting experiences.
- Assess the level of interest/demand for rainwater harvesting from potential consumers within CWSSP area.

4.3.4 Construction

- Construction of a 5M³ Brick dome tank at Badulla
- Construction of a 5M³ Ferrocement trial tank at Ratnapura
- Construction of a 1M³ Cement Jar at NERD Centre Ja-Ela.



5. Status of Rain Water Harvesting in Sri Lanka

In Sri Lanka one can trace the evidence of rainwater harvesting back to the fifth century.

For instance, the network of storage reservoirs, swimming pools artificial streams and baffling fountains of the 5th Century rock fort of Sigiriya relied totally on rainwater harvesting. Agriculture also relied mainly on irrigation through cleverly designed, surface storage tanks (wewas).

In recent years many of this rain water collection skills have become obsolete. People now often rely on reticulated, central systems for drinking water supply and irrigation. So, presently Sri Lanka cannot claim a well planned rainwater harvesting program.

Local Investigations reveal however that

- rainwater harvesting for domestic consumption is currently in practice in Sri Lanka.
- a section of potential consumers are looking for appropriate technology to harvest and store rain water.
- a section of potential consumers are not sure about rainwater harvesting.

Details of a Few Selected Visits

5.1 Iriyagama

The residents of Iriyagama situated close to the Kandy Road at Peradeniya used mainly rain water before the town water supply system was put into operation. One house with a roof area of about 200 sq. meters has three 7000 liter tanks, made of masonry. This system built about sixty years ago is still usable. The residents had adequate water for all their domestic uses when the system was in use. The Bible School at Iriyagama too used rain water as the only source while running a 35 student hostel. Hosteliers were not allowed to bathe with this water.

At present the town relies almost totally on the town's pipe water supply as their main source of water. This is unfortunate. Rainwater harvesting systems if re-used can be a useful additional source of water. However, as long as the town supply continue to supply government subsidized cheap water the interest of the resident to re-use the rainwater harvesting systems will be low.



5.2 Bandarawela

Mr. Pigera of Bandarawela, a retired police officer, built an underground cistern to store rainwater in 1982. This rectangular cistern is 3 meter deep and holds about 18000 liters. The catchment roof, is approximately 180 M². The tank is made by simply plastering the sides of the pit with cement mortar, and all the work was done by the unskilled members of the family. This cistern has served up to four families in the past. This is the best water supply solution for people in the hills, says Mr. Pigera who got the idea from a friend in South India. In dry parts of South India where it rains only a few months per year harvesting rainwater has a long history, according to Mr. Pigera.



Mr. Pigera & the water system. (Hapugoda)

5.3 Galle

At the peak of the Buona Vista Hill, Galle a rainwater harvesting system is under construction. On completion rain water from part of the very large roof will fill into a 18000 liters. re-inforced concrete covered tank. The over flow from this tank is directed to a 90,000 liters open tank, through underground locally fabricated 30 cm diameter concrete pipes. The estimated cost for this system is about five hundred thousand rupees.

The Peak of Buona Vista Hill, has long suffered from lack of water. The rain water harvesting system design was proposed after an effort to supply water with tube wells and other means failed, said Mr. Lakshman Welikala, the Civil Engineer responsible for this design. The design was presented at the Tokyo International Rainwater Utilization conference in 1994.



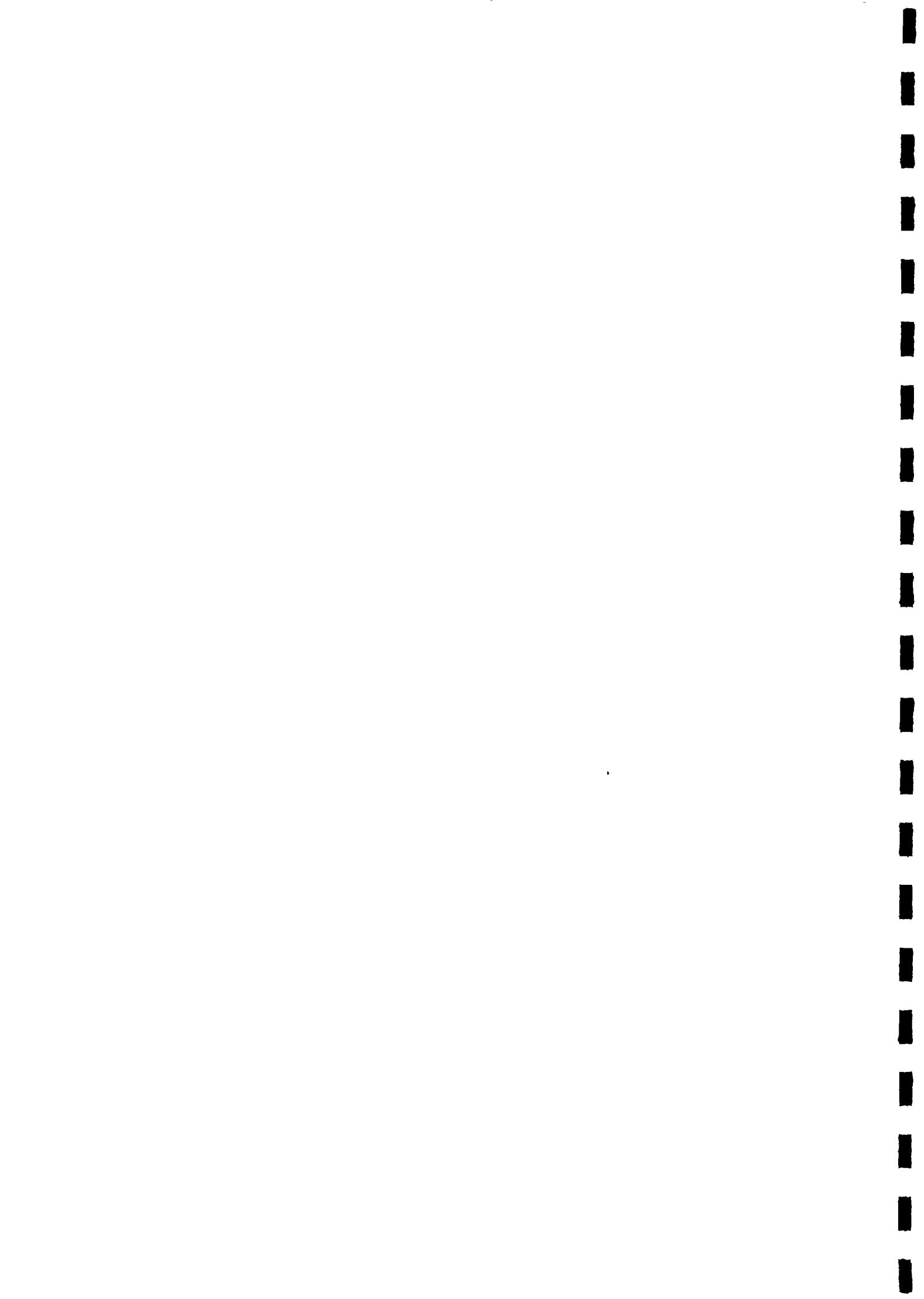
5.4 Kundasale

Low income families at Ahaspokuna Village in Kundasale, have on their own built 1400 - 1800 liter tanks out of home burnt mud bricks. Out of the seven houses visited six of them had some form of permanent roofs. The gutters were standard pvc gutters. They have improvised a cheap polythene pipe to lead the water from the gutter into the tank. The roof area in most houses was over 40 m², and some tanks were said, never to go dry. A women in one of the houses was keen to add that they are very careful with water, as they pay up to Rs. 350 per 5000 liter bowser. At one house, a low level second tank built adjoining the main tank, collected some of the waste water for bathing, washing, etc. This is depicted in the front cover graphic. This water is re-used in the water-seal toilets. A recent aid project helped the inhabitants to build these toilets. The village households have collected and used rainwater for the last five years. Most tanks leak after about five years, however these can be repaired easily by replastering the inside.

None of the tanks had covers resulting in mosquito nuisance. One owner had some fish in the water, said to prevent mosquito breeding. The general view is that rain water is acceptable as a water source. However the cost of building tanks to store it is too costly. One family said they were willing to spend up to Rs. 10000/- in installments to build storage tanks, if they can store enough water for their domestic use.



Typical System at Kundasale (Hapugoda)



5.5 Peradeniya

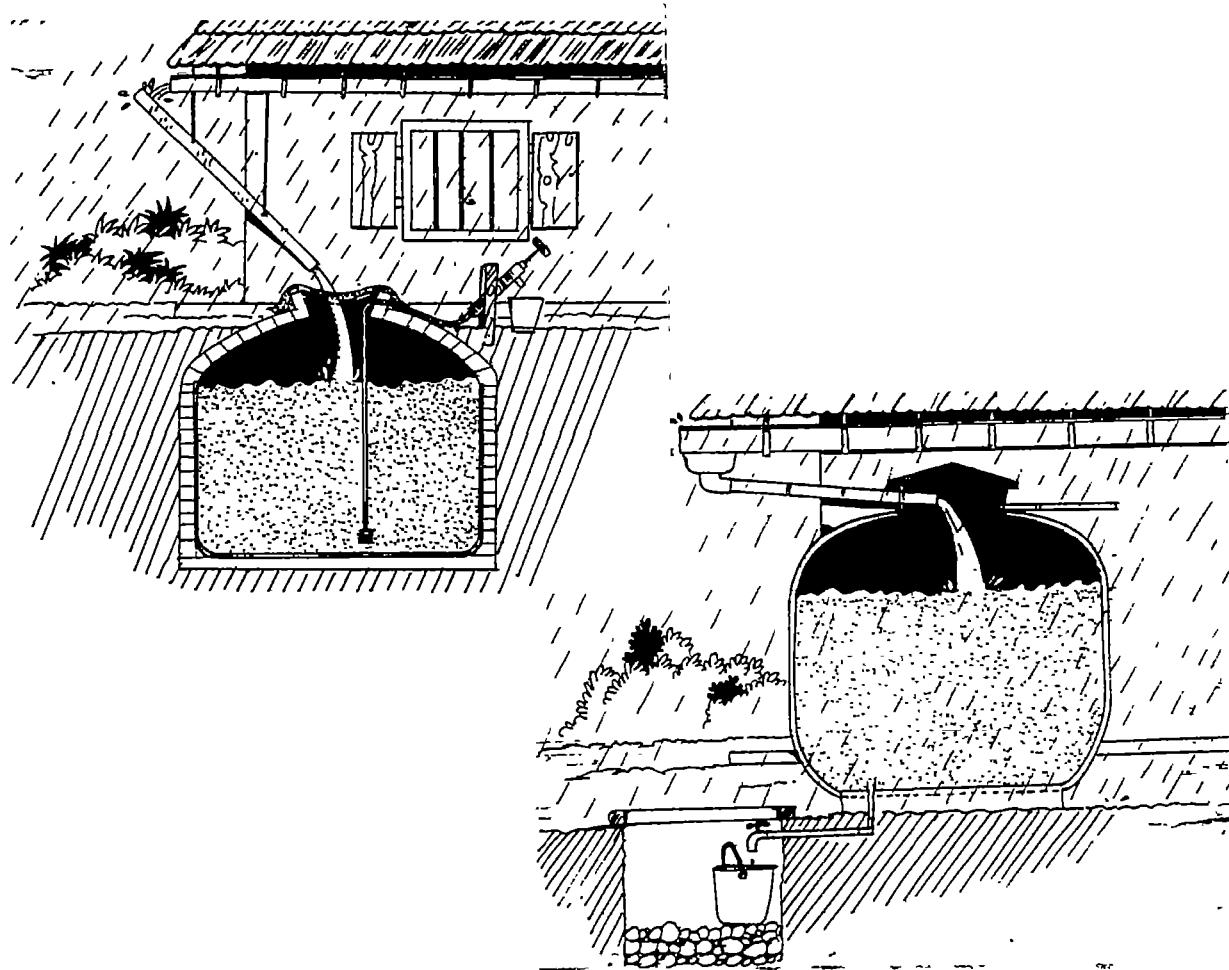
The residence of the Dean of the Faculty of Engineering, University of Peradeniya has an 2.40 meter high 30 cubic meter ferro-cement tank to store rainwater from an approximately 200 square meter area of his house roof. The water is pumped into a two cubic meter overhead tank and used for all domestic purposes including washing clothes by machine. Eight adults live here. An elaborate two-pump system to pump water from a well, located about one hundred meters lower in elevation, backs up the rainwater harvesting system. However this is rarely used. The tank costs about Rs. 10000 in 1992. The Professor is very pleased and proud of the system.



(Hapugoda)



6. Rain Water Harvesting as an Option.



6.1. Advantages and Disadvantages of Rain-Water Harvesting Systems.

Advantages and disadvantages of rainwater harvesting vary depending mainly on the rainfall pattern, catchment area, storage capacity and user demand, of a situation. General advantages and disadvantages are given below.

Advantages

- the quality of rainwater can be kept high with simple precautions.
- systems can be independent
- local materials and skills can be used for the construction of the systems.
- maintenance can be done by the user.
- water is available at the dwelling, this saves time in collecting water.



- during rainy periods a high level of domestic service can be expected as there is adequate water collected.

disadvantages

- High initial capital cost.
- available water is limited by rainfall and catchment area.
- water has a flat taste due to lack of minerals.
- lack of minerals in the water may cause nutrition deficiencies.
- the user must learn to ration the use of water during the dry season.

6.2. Feasibility

At the Project Development Phase, once there is doubt that traditional water-supply systems are not feasible due, to technical, economic or social reasons, consideration of the feasibility of rainwater harvesting can be initiated.

In the CWSSP the choice of technology must suit remote rural communities. Construction must be possible by locally available materials and skills. In a number of hilly areas available water supply options are tube wells or high head pump systems. Both can be poor choices. To construct tube wells external expensive technical inputs are needed. Sometimes lack of proper roads make it very difficult for rigs to get to the right place. Pump systems need fuel or electricity on a continuous basis. Their maintenance need funds and skilled personal.

In the existing pump schemes under CWSSP, it is seen that paying for water on a regular basis is difficult for the beneficiaries who in many cases do not have a regular income.

Communal pump pipe schemes and tube well systems create social problems due to their communal nature. In most villages there are political, social and economic differences that trickle down into the management of communal water systems. Water right issues, such as the owner of the land where the springs are, located may protest, here too rainwater harvesting can be the choice to prevent further delays.



6.2.1 Rain fall

Sri Lanka is divided into two major zones, wet and dry. The dry zone occupies the majority of the land area. (65% of total land area). The dry zone gets the rain fall from North-East monsoon from November through April and the wet zone gets the rain from May through October mainly. (see figure 1).

Reliable rainfall data is required when determining the supply from the system. Rainfall data for about the last 10 year period is preferable. This information can be obtained from the Colombo Meteorological Office.

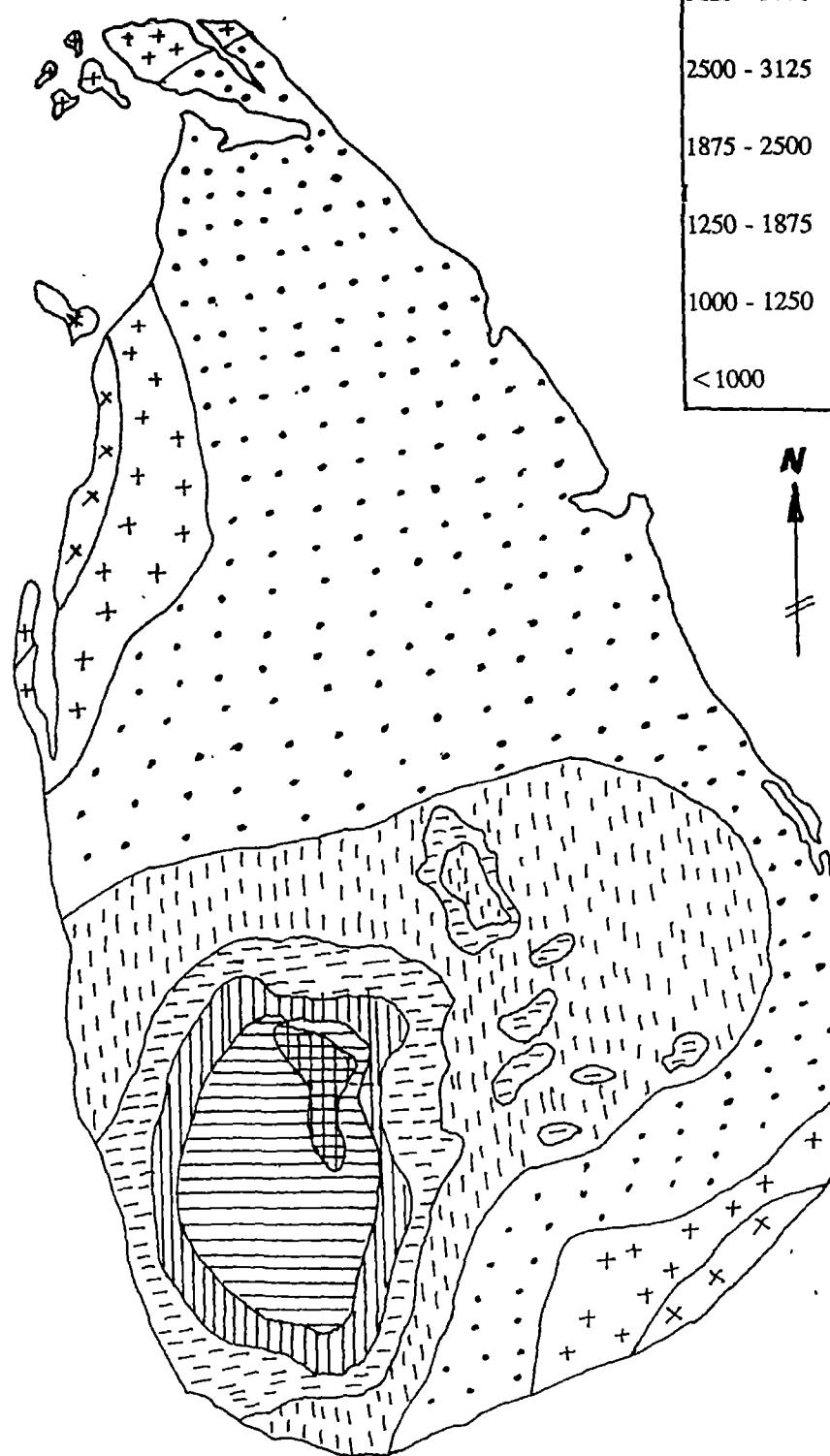
If rain-fall data for a particular area is not available by identifying the area in the 1" contour maps at the Meteorological Office, monthly rainfall data can be obtained from the climatically closest station to this area.

For design purposes it is important to obtain monthly rainfall data. The Met: office sells one year monthly rain fall data at Rs. 15/- (1995). A computer print out on daily rain fall data too is available for sale.

A monthly rainfall data for selected stations relevant to the study is given in **Annex 2**. Figure I gives mean annual rainfall for the entire country.



Figure I



Mean Annual Rainfall (mm)



6.2.2 Water Demand

In a household water is used for drinking, cooking, cleaning, and washing. In rural areas under the CWSSP each person may use between 45 to 120 liters per day, if there is no restriction.

The supply from a rainwater harvesting system takes place in a variable manner depending on the rainfall pattern of a place. In the wet season in a normal year (about 6 months of the year) it can supply upto six times the dry season supply. In this way where a dry season demand is 20 liters per person per day, during half the year the demand can go up to 120 liters per person per day.

The next step involves estimating the total annual demand and comparing it with the supply possible from the relevant rainwater catchment area. If the supply exceeds the demand rainwater harvesting is technically feasible.

Table 6 - 1 sites examples with different rainfall average and roof catchment areas.

Table 6.1

Annual Average Rainfall mm	Roof Area M ²	Run off Coefficient	Annual Average Supply M ³	Annual Minimum Demand M ³	Feasibility
1300	40	0.8	41.6	36.5	Feasible
1300	20	0.8	20.8	36.5	Demand too high
1750	20	0.8	28	36.5	Demand too high
1750	30	0.8	42	36.5	Feasible
3500	14	0.8	39.2	36.5	Feasible

If the supply is less than demand, then a possible solution includes increasing the catchment area, or reducing the demand for rainwater by limiting it uses to say, drinking and cooking.

6.2.3 Water Supply

Graphs U,V,W,X,Y,Z (Annex 10) give possible driest (in a ten year period) season supplies in liters per day from a 5 m³ storage for catchment areas upto 200 sqr. mtrs. for selected six meteorological station regions in Badulla, Matara and Ratnapura districts.



Table 6.2 is prepared using the above graphs. The catchment area is selected as 60M^2 .

Table 6 - 2

District	Roof Area M^2	Storage M^3	Dry season supply in liters from one roof per day.	
			In a area with high average annual/rainfall	In a area with low average annual rainfall
Matara	60	5	150 (Aninkanda)	65 (Kekenadora)
Ratnapura	60	5	125 (Ratnapura)	48 (Ambilipitiya)
Badulla	60	5	77 (Haputale)	62 (Badulla)

Minimum water-supply volumes are for the driest months of the driest year, in a ten year period. Water-supply can go up to six times these amounts during the remaining months depending on how wet it is.

Table 6 - 3 gives the possible daily supplies, in different months, from a well managed system with a 60M^2 catchment and 5M^3 tank, at Ambilipitiya in the Ratnapura district, in a normal year.

In all other regions in the three districts, it is possible to get a better level of service than at Ambilipitiya from a well managed rain water harvesting system as rainfall at Ambilipitiya is among the lowest in the three districts.

Table 6 - 3

Ambilipitiya in a Normal Year [System 60M^2 catchment 5M^3 Storage]

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Monthly mean R.F.	75.9	66.9	120	153	112	44	55	41	71.8	201	243	160
Monthly Supply M^3 [Catchment 60M^2 R.C. 0.8]	3.6	3.2	5.8	7.3	5.4	2.1	2.6	2	3.4	9.7	11.7	7.7
Taken from the months supply M^3	3	3	5.8	7.3	3	2.1	2.6	2	3	9.7	11.7	7.7
Taken from other monthly supply M^3	0	0	0	0	-2.3	+.9	+.4	+.1	0	0	0	0
Possible Supply in a day in Liters	100	100	190	240	100	100	100	100	100	315	384	250

Conclusion: In a normal year, if the tank is half full at the end of May, this catchment can supply 100 liters per day throughout the dry season months upto September. This is a very reasonable level of service for a area as dry as Ambilipitiya.



6.3. Economics

Initial per capita capital cost of a rainwater harvesting system is high, in relation to other types of water supply systems.

A typical rainwater harvesting systems consist of

1. Suitable roof catchment
2. Gutter & down pipe system
3. A storage tank of adequate size.
4. Device to extract water from the tank.

Normally, the catchment will be an existing roof and gutters & down pipes. These are considered part of the building.

The major cost being in the construction of tanks, the economic analysis given below refer to the cost of tank construction.

6.3.1 Cost Scenario

Graphs O,P,Q,R,S,T (Annex - 9) give the required tank storage volumes for roof areas upto 200 square meters in 6 selected Meteorological Station regions in the three district of Badulla, Ratnapura and Matara.

Graphs O,P,Q,R,S,T takes into account monthly rainfall variation of a ten year period. Tank storage volume is the requirement for the ten year dry year.

Graphs A,B,D,E,F,G (Annex - 8) prepared by mass curve analysis (numerical method) were used to prepare the graphs O,P,Q,R,S,T.

Table 6.4

District	Roof Area M ²	Minimum Supply from a roof per day lit (M ³ /YR)	Storage required in Cubic Meters	
			Station with high Avg Annual R.F.	Station with Low Avg. Annual Rainfall
Matara	60	100 (36.5)	(Aninkanda) 0.6	(Kekeñadora) 9.5
Ratnapura	60	100 (36.5)	(Ratnapura) 2.5	(Ambilipitiya) 17.5
Badulla	60	100 (36.5)	(Haputale) 6.75	(Badulla) 12.5

Runoff coefficient = 0.8

If five persons live in a house with a suitable roof catchment area of 60M² and each person requires supply of 20 lit per day, the annual required supply is 36.5 cubic meters.

Where the roof area is taken as 60M² Table 6.4 gives required storage values within each district.



e.g. At Matara district required volume is approximately from 0.6 to 11 cubic meters depending on the rainfall of the area. At Rs. 1.25 per lit for constructing a storage tanks, costs per house of 60M² catchment roof varies between 750 to Rs. 13,750.

Comment: Storage values given in Table 6.4 are for the 10 year driest year. In a normal year the level of service improves considerably, as can be seen from Table 6.3.

Table 6.5

Tank	Capacity M ³	Total Cost	Pump	Cost per Lit Storage Rs.
Brick Dome	5	5592	450	1.21
Brick Dome	8	8129	450	1.08
Brick Dome	10	9175	450	0.97
Ferro-Cement	5	7166	NIL	1.43
Jar	1.1		NIL	ref. annex 13

Total cost exclude transport cost.

Annex 14 gives material and cost breakdown of the brick dome tanks.

Table 6.5 gives cost per liter of storage for four types of tanks. A brick dome tank is built below ground. Therefore the cost of, extraction pump is included.

Table 6.6

Total Tank Cost (Example)

DISTRICT	Roof Area M ²	Possible min Supply per day from a roof (house) Liters in a ten year dry year	Total Cost per Tank System	
			Area with high Avg. Rain Fall Rs.	Area with Low Avg. Rain Fall Rs.
Matara	60	100	750	11,875
Ratnapura	60	100	3125	21,875
Badulla	60	100	8438	15,625



Table 6.7

CWSSP Contribution as 80% of Total Cost

DISTRICT	Roof Area M ²	Possible min Supply per day from a roof (house) Liters in a ten year dry year	CWSSP Cost per Tank System	
			Area with high Avg. Rain Fall Rs.	Area with Low Avg. Rain Fall Rs.
Matara	60	100	600	9,500
Ratnapura	60	100	2500	17,500
Badulla	60	100	6750	12,500

Tables 6 - 6 & 6 - 7 gives general trend of the costs of rainwater harvesting in the relevant three districts, where the minimum supply for a house per day is 100 liters in a ten year dry year.

To bring the CWSSP contribution down to Rs. 5390/-, options are,

1. to increase the catchment area.
2. to lower to minimum service level, for the ten year dry year.
3. to select a relevant low cost tank option.

Various scenarios, to be considered in Badulla are as follows.

Table 6 - 8 gives the cost scenario when minimum supply per day in a ten year dry year from a roof is 50 liters.

Table 6.8

Catchment area M ²	40	60	80
Annual Supply (R.C = 0.8) M ³	56	84	112
Annual Demand M ³	18.3	18.3	18.3
Demand as % of Supply	33	22	16
Required Storage as % of Supply. (From Rain Region graph A Annex 8)	9	4	1.5
Required Storage M ³	5	3.4	1.7
Total Cost of Storage Rs.	6250	4250	2125
CWSSP Cost Rs.	5000	3400	1700



Table 6 - 9 gives the cost scenario when minimum supply per day in a ten year dry year from a roof is 75 liters.

Table 6.9

Catchment area M ²	40	60	80	100
Annual Supply (R.C = 0.8) M ³	56	84	112	140
Annual Demand M ³	27.4	27.4	27.4	27.4
Demand as % of Supply	49	33	25	20
Required Storage as % of Supply. (From Rain Region graph A Annex 8)	18	9	5	2.5
Required Storage M ³	10	7.6	5.6	3.5
Total Cost of Storage Rs.	12,500	9,500	7,000	4,375
CWSSP Cost Rs.	10,000	7,600	5,600	3,500

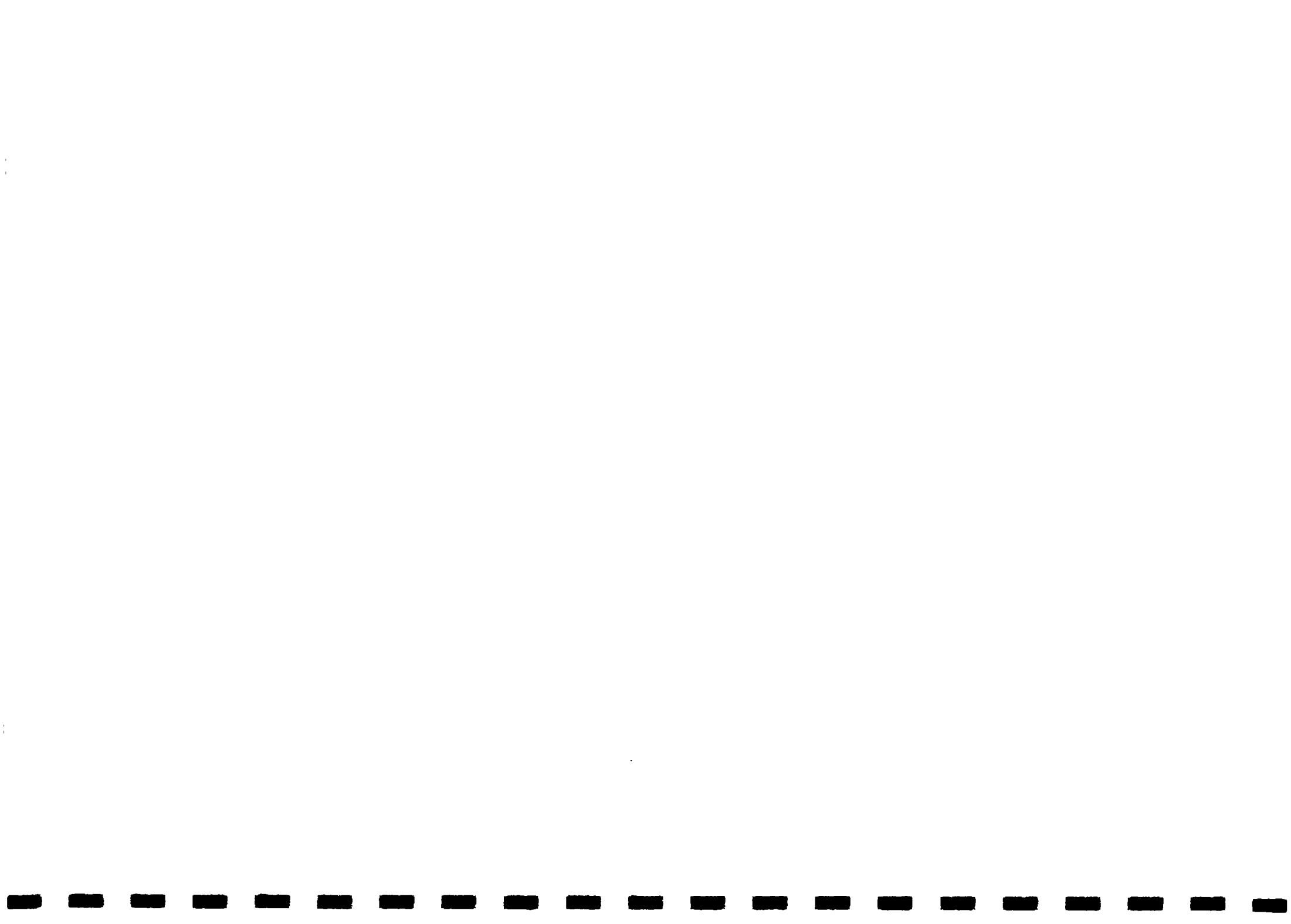
- Note:
1. In a normal year minimum supply per day is more than double.
 2. Six months of the year, when it is wet supply per day from a roof can go up six times the supply volume, of the dry months, in the same system.

Possible daily supply in liters from a well managed Rain Water Harvesting System in a normal year in the Badulla Rain Region, consisting of different size catchments and a 5M³ storage tank, is given in Table 6 - 10.

Table 6 - 10

Catchment Area M ²	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
20	70	70	70	70	70	70	70	70	70	70	70	70
30a	100	100	100	100	100	100	80	65	110	184	200	125
40	252	100	100	100	100	100	100	100	148	250	260	250
60	383	110	187	252	100	100	100	131	228	365	409	377

Note: a With a 5.5M³ Tank possible to manage a minimum supply of 100 LPD.



6.4. Social

Once it has been tentatively established that it is technically and economically feasible to construct a rain water harvesting system, the next step involves social and community assessment. This stage is critical to the success of the scheme.

Consideration must be given to traditional practices within the community. The role of women and children is carrying water, existing catchment possibilities, palatability of rain water, communal vs individual systems, and maintenance expenditure management.

At the end the community members should willingly choose the option of rainwater harvesting.

6.5. Design

The design stage of the project involves in sizing the storage tank. Two acceptable methods are discussed below.

6.5.1 Dry season demand versus supply method

To determine the required tank volume multiply the days of the longest dry period by the amount of water required per day.

e.g at Badulla.

To supply 100 lit per day per house to accommodate a 50 day dry period, the required storage volume is:

$$100 \times 50 = 5000 \text{ M}^3$$

This method gives only a rough estimate of the storage required. It does not take into account the variation in the annual rainfall pattern.



Table 6 - 11 gives water supply scenario from a 5M³ tank.

FIXED - Storage Capacity 5000 Liters

Table 6 - 11

Length of Drought Days	Family of 6 available Water per Person per Day	Family of 5 Available Water per Person per Day
14	60	70
21	40	48
28	30	36
35	24	29
42	20	24
49	17	20
56	15	18
63	13	16
70	12	14
77	11	13
84	10	12
91	9	11

Note : The possible service level in 70 to 90 day dry spell is considered adequate for most basic needs such as drinking and cooking.

6.5.2 Mass curve analysis method

A more accurate method of sizing a tank, involves an analysis of monthly rainfall data using the mass curve technique. Best is to use approximately the latest 10 years of data. As an example, the data for the Badulla area is analysed below.

Badulla Monthly Rainfall data (mm) is in **Table 6 - 12**.

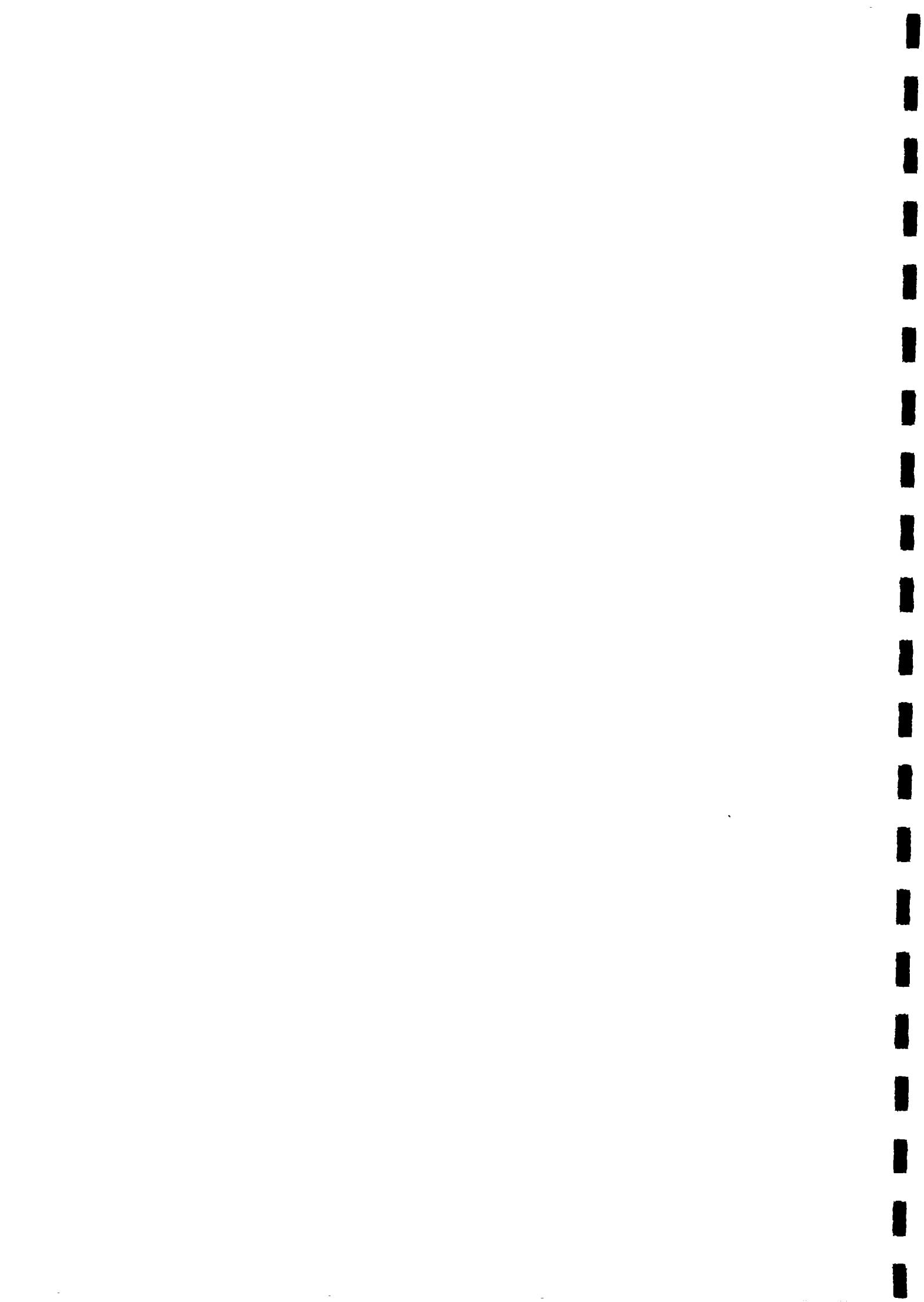


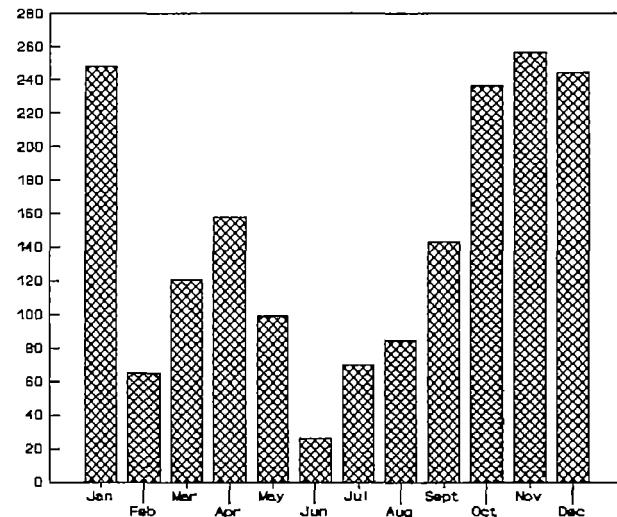
TABLE 6 - 7

BADULLA RAINFALL DATA

in mm

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sept	Oct	Nov	Dec	Total
1985	171.2	76.1	185.4	75.6	82.2	16.9	52.0	133.6	90.8	233.3	188.9	245.1	1551.10
1986	721.5	136.8	281.0	250.1	120.4	2.0	71.3	98.0	65.8	376.2	131.4	207.8	2462.30
1987	206.5	42.7	85.7	218.7	171.6	3.6	10.2	62.9	175.0	273.8	165.2	88.4	1504.30
1988	48.4	59.0	198.7	249.0	35.6	30.0	51.9	246.1	136.8	147.1	350.9	241.5	1795.00
1989	201.0	14.9	80.2	114.1	51.3	39.0	216.7	76.5	249.6	295.7	267.6	106.4	1713.00
1990	386.0	118.8	156.0	149.0	101.3	8.4	105.3	43.0	172.5	179.1	151.7	332.3	1903.40
1991	347.9	39.1	101.1	219.0	90.3	48.0	25.4	31.0	147.4	155.9	153.1	300.8	1659.00
1992	85.3	0.0	0.0	46.6	85.2	0.3	48.0	32.6	63.2	112.1	584.1	245.0	1302.40
1993	63.9	36.4	76.6	97.7	236.3	86.6	101.7	85.2	134.2	270.0	241.1	329.8	1759.50
1994	247.6	129.6	42.3	159.1	17.2	26.5	17.2	37.2	197.4	320.0	328.4	343.5	1866.00
Average	247.9	65.3	120.7	157.9	99.1	26.1	70.0	84.6	143.3	236.3	256.2	244.1	1751.6
Standard Deviation	190.6	45.9	79.4	70.0	61.7	25.4	57.7	62.3	56.0	81.1	131.1	85.3	292.6

Rain Fall Analysis - Badulla





6.5.2.1 Design (example Badulla)

1. Roof size 60M²

Run off coefficient 0.8

2. Average yearly supply = Area x runoff coeff. x average annual rainfall

= 60 X 0.8 X 1.75

Average annual rainfall = 1750 mm (1985 to 1994)

3. Table of Mass Curve Analysis

4. Decide monthly demand (supply) = 1500 liters

5. From the mass curve analysis (**Table 6 - 13**)

the storage requirement

is determined as = 464548.8 - 461548.8 = 3000 liters

(Total amount stored in the 85th Month minus 87th Month)

Comment: In the above case it is possible to give an extra level of service with a 5000 liter storage tank, which can be constructed within CWSSP criteria in Badulla.



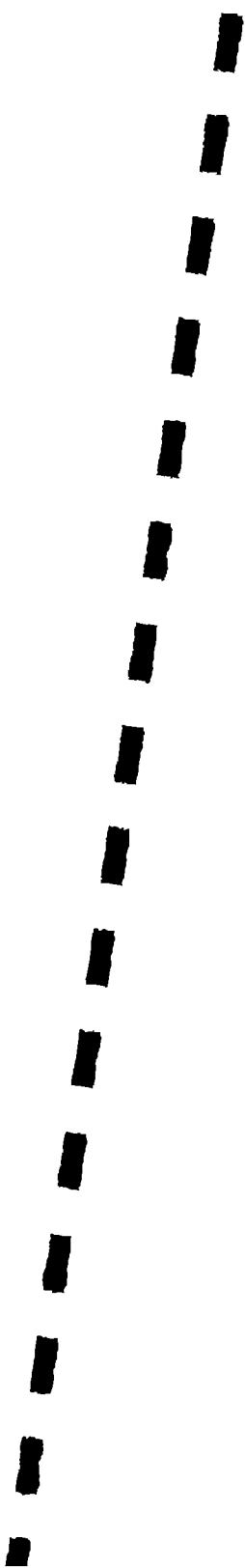
Table 6 – 13**RAINFALL MASS CURVE ANALYSIS – MONTHLY****RAINFALL MASS CURVE ANALYSIS – MONTHLY**

(Numerical Method)

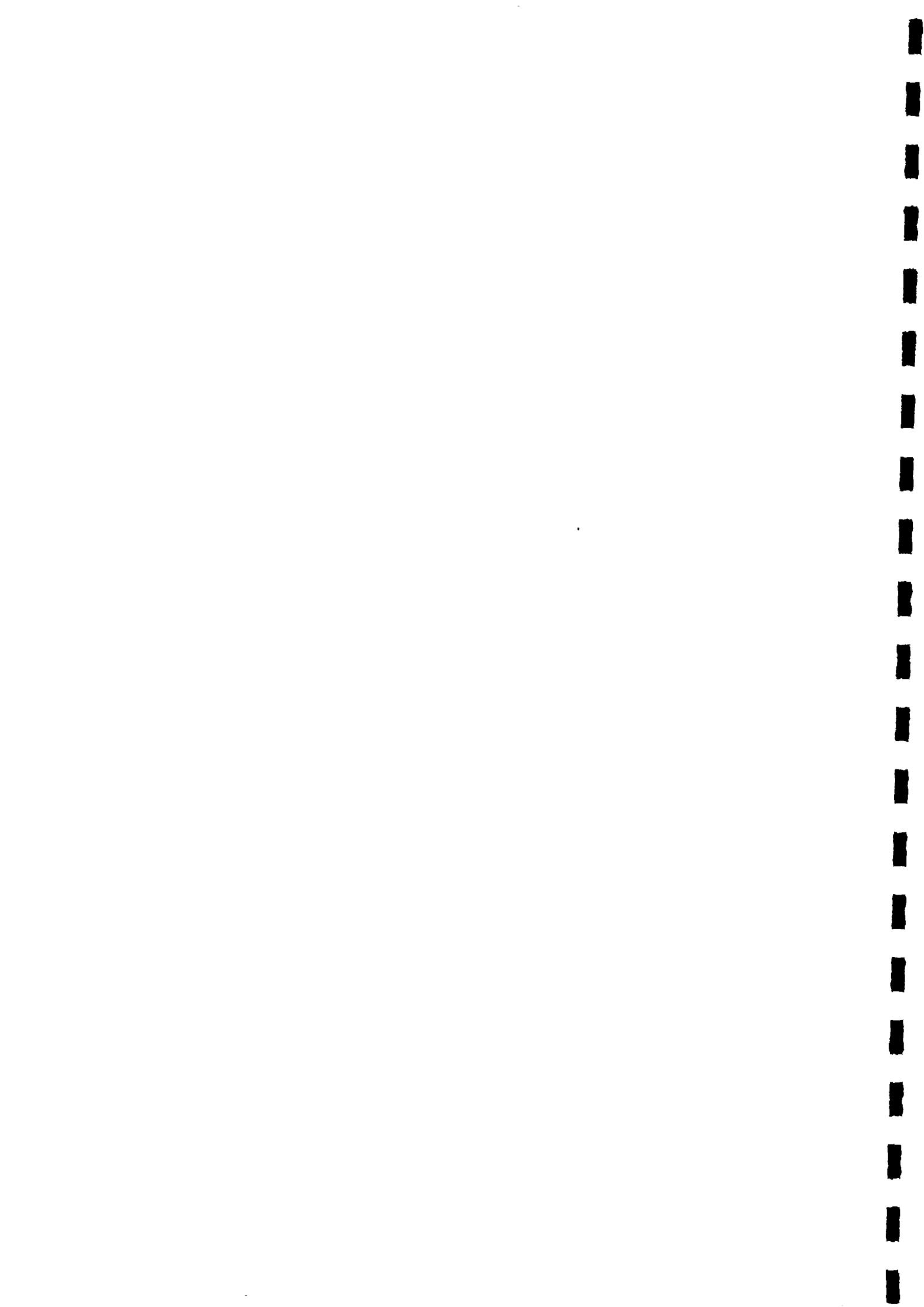
BADULLA 1985 TO 1994ROOF AREA = 60 M²

RUN OFF COEFFICIENT = 0.8

Month	Monthly Rainfall	Monthly Supply Liters	Cumulative Supply Liters	Monthly Demand Liters	Amount Stored Liters	Total Amount Stored Liters	Required Tank Volume Liters	
1	0.0	0.0	0.0	0	0.0	0.0		48
2	0.0	0.0	0.0	0	0.0	0.0		48
3	0.0	0.0	0.0	0	0.0	0.0		48
4	75.6	3628.8	3628.8	1500	2128.8	2128.8		48
5	82.2	3945.6	7574.4	1500	2445.6	4574.4		48
6	16.9	811.2	8385.6	1500	-688.8	3885.6		48
7	52.0	2496.0	10881.6	1500	996.0	4881.6		48
8	133.6	6412.8	17294.4	1500	4912.8	9794.4		48
9	90.8	4358.4	21652.8	1500	2858.4	12652.8		48
10	233.3	11198.4	32851.2	1500	9698.4	22351.2		48
11	188.9	9067.2	41918.4	1500	7567.2	29918.4		48
12	245.1	11764.8	53683.2	1500	10264.8	40183.2		48
13	721.5	34632.0	88315.2	1500	33132.0	73315.2		48
14	136.8	6566.4	94881.6	1500	5066.4	78381.6		48
15	281.0	13488.0	108369.6	1500	11988.0	90369.6		48
16	250.1	12004.8	120374.4	1500	10504.8	100874.4		48
17	120.4	5779.2	126153.6	1500	4279.2	105153.6		48
18	2.0	96.0	126249.6	1500	-1404.0	103749.6		48
19	71.3	3422.4	129672.0	1500	1922.4	105672.0		48
20	98.0	4704.0	134376.0	1500	3204.0	108876.0		48
21	65.8	3158.4	137534.4	1500	1658.4	110534.4		48



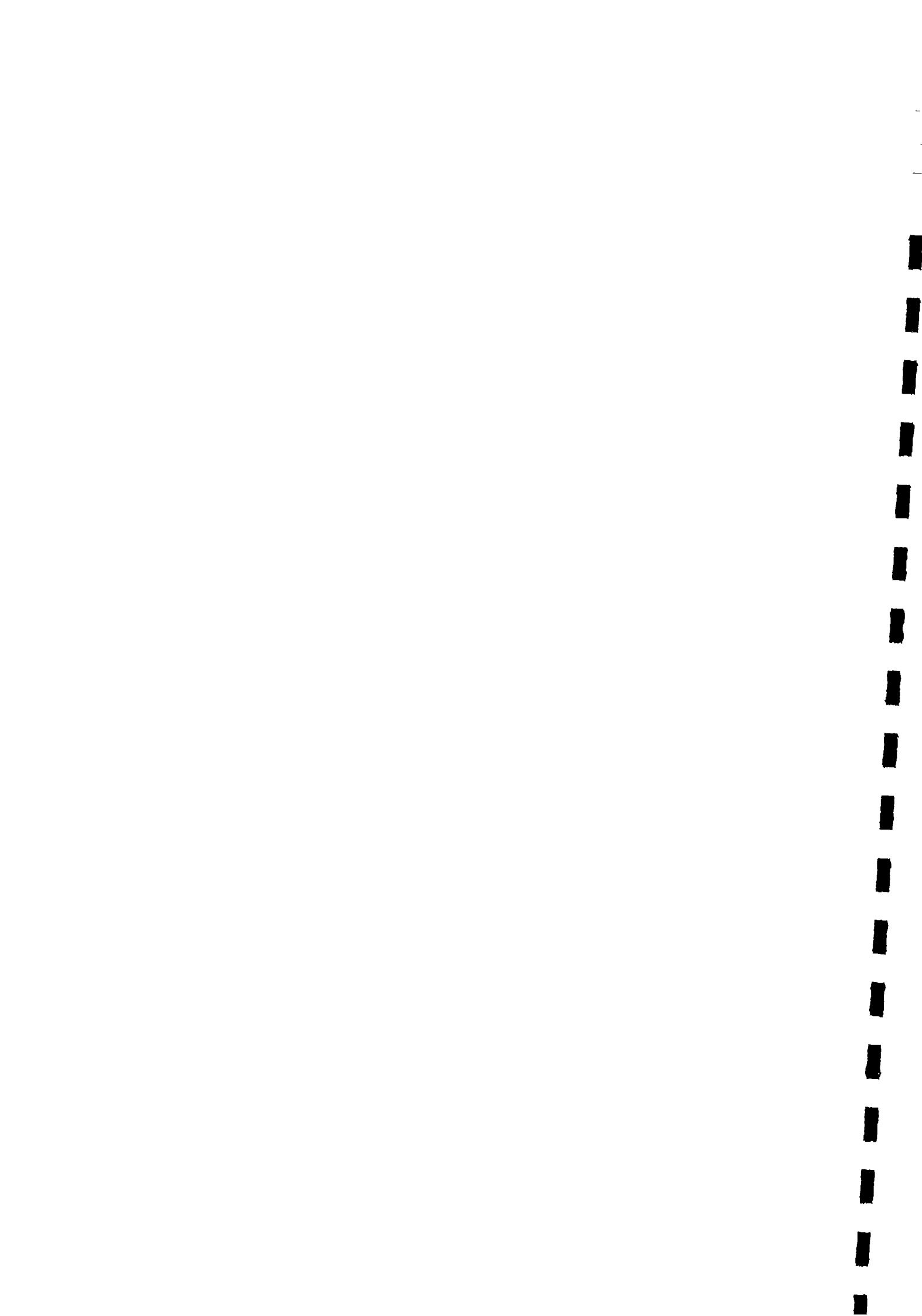
Month	Monthly Rainfall	Monthly Supply Liters	Cumulative Supply Liters	Monthly Demand Liters	Amount Stored	Total Amount Stored	Required Tank Volumn	
22	376.2	18057.6	155592.0	1500	16557.6	127092.0	48	
23	131.4	6307.2	161899.2	1500	4807.2	131899.2	48	
24	207.8	9974.4	171873.6	1500	8474.4	140373.6	48	
25	206.5	9912.0	181785.6	1500	8412.0	148785.6	48	
26	42.7	2049.6	183835.2	1500	549.6	149335.2	48	
27	85.7	4113.6	187948.8	1500	2613.6	151948.8	48	
28	218.7	10497.6	198446.4	1500	8997.6	160946.4	48	
29	171.6	8236.8	206683.2	1500	6736.8	167683.2	48	
30	3.6	172.8	206856.0	1500	-1327.2	166356.0	48	
31	10.2	489.6	207345.6	1500	-1010.4	165345.6	48	
32	62.9	3019.2	210364.8	1500	1519.2	166864.8	48	
33	175.0	8400.0	218764.8	1500	6900.0	173764.8	48	
34	273.8	13142.4	231907.2	1500	11642.4	185407.2	48	
35	165.2	7929.6	239836.8	1500	6429.6	191836.8	48	
36	88.4	4243.2	244080.0	1500	2743.2	194580.0	48	
37	48.4	2323.2	246403.2	1500	823.2	195403.2	48	
38	59.0	2832.0	249235.2	1500	1332.0	196735.2	48	
39	198.7	9537.6	258772.8	1500	8037.6	204772.8	48	
40	249.0	11952.0	270724.8	1500	10452.0	215224.8	48	
41	35.6	1708.8	272433.6	1500	208.8	215433.6	48	
42	30.0	1440.0	273873.6	1500	-60.0	215373.6	48	
43	51.9	2491.2	276364.8	1500	991.2	216364.8	48	
44	246.1	11812.8	288177.6	1500	10312.8	226677.6	48	
45	136.8	6566.4	294744.0	1500	5066.4	231744.0	48	
46	147.1	7060.8	301804.8	1500	5560.8	237304.8	48	
47	350.9	16843.2	318648.0	1500	15343.2	252648.0	48	
48	241.5	11592.0	330240.0	1500	10092.0	262740.0	48	



Month	Monthly Rainfall	Monthly Supply Liters	Cumulative Supply Liters	Monthly Demand Liters	Amount Stored Liters	Total Amount Stored Liters	Required Tank Volumn Liters	
49	201.0	9648.0	339888.0	1500	8148.0	270888.0		48
50	14.9	715.2	340603.2	1500	-784.8	270103.2		48
51	80.2	3849.6	344452.8	1500	2349.6	272452.8		48
52	114.1	5476.8	349929.6	1500	3976.8	276429.6		48
53	51.3	2462.4	352392.0	1500	962.4	277392.0		48
54	39.0	1872.0	354264.0	1500	372.0	277764.0		48
55	216.7	10401.6	364665.6	1500	8901.6	286665.6		48
56	76.5	3672.0	368337.6	1500	2172.0	288837.6		48
57	249.5	11976.0	380313.6	1500	10476.0	299313.6		48
58	295.7	14193.6	394507.2	1500	12693.6	312007.2		48
59	267.6	12844.8	407352.0	1500	11344.8	323352.0		48
60	106.4	5107.2	412459.2	1500	3607.2	326959.2		48
61	386.0	18528.0	430987.2	1500	17028.0	343987.2		48
62	118.8	5702.4	436689.6	1500	4202.4	348189.6		48
63	156.0	7488.0	444177.6	1500	5988.0	354177.6		48
64	149.0	7152.0	451329.6	1500	5652.0	359829.6		48
65	101.3	4862.4	456192.0	1500	3362.4	363192.0		48
66	8.4	403.2	456595.2	1500	-1096.8	362095.2		48
67	105.3	5054.4	461649.6	1500	3554.4	365649.6		48
4	43.0	2064.0	463713.6	1500	564.0	366213.6		48
69	172.5	8280.0	471993.6	1500	6780.0	372993.6		48
70	179.1	8596.8	480590.4	1500	7096.8	380090.4		48
71	151.7	7281.6	487872.0	1500	5781.6	385872.0		48
72	332.3	15950.4	503822.4	1500	14450.4	400322.4		48
73	347.9	16699.2	520521.6	1500	15199.2	415521.6		48
74	39.1	1876.8	522398.4	1500	376.8	415898.4		48
75	101.1	4852.8	527251.2	1500	3352.8	419251.2		48



Month	Monthly Rainfall	Monthly Supply Liters	Cumulative Supply Liters	Monthly Demand Liters	Amount Stored Liters	Total Amount Stored Liters	Required Tank Volumn Liters	
76	219	10512.0	537763.2	1500	9012.0	428263.2		48
77	90.3	4334.4	542097.6	1500	2834.4	431097.6		48
78	48.0	2304.0	544401.6	1500	804.0	431901.6		48
79	25.4	1219.2	545620.8	1500	-280.8	431620.8		48
80	31.0	1488.0	547108.8	1500	-12.0	431608.8		48
81	147.4	7075.2	554184.0	1500	5575.2	437184.0		48
82	155.9	7483.2	561667.2	1500	5983.2	443167.2		48
83	153.1	7348.8	569016.0	1500	5848.8	449016.0		48
84	300.8	14438.4	583454.4	1500	12938.4	461954.4		48
85	85.3	4094.4	587548.8	1500	2594.4	464548.8		48
86	0.0	0.0	587548.8	1500	-1500.0	463048.8		48
87	0.0	0.0	587548.8	1500	-1500.0	461548.8		48
88	46.6	2236.8	589785.6	1500	736.8	462285.6		48
89	85.2	4089.6	593875.2	1500	2589.6	464875.2		48
90	0.3	14.4	593889.6	1500	-1485.6	463389.6		48
91	48.0	2304.0	596193.6	1500	804.0	464193.6		48
92	32.6	1564.8	597758.4	1500	64.8	464258.4		48
93	63.2	3033.6	600792.0	1500	1533.6	465792.0		48
94	112.1	5380.8	606172.8	1500	3880.8	469672.8		48
95	584.1	28036.8	634209.6	1500	26536.8	496209.6		48
96	245.0	11760.0	645969.6	1500	10260.0	506469.6		48
97	63.9	3067.2	649036.8	1500	1567.2	508036.8		48
98	36.4	1747.2	650784.0	1500	247.2	508284.0		48
99	76.6	3676.8	654460.8	1500	2176.8	510460.8		48
100	97.7	4689.6	659150.4	1500	3189.6	513650.4		48
101	236.3	11342.4	670492.8	1500	9842.4	523492.8		48
102	86.6	4156.8	674649.6	1500	2656.8	526149.6		48



Month	Monthly	Monthly	Cumulative	Monthly	Amount	Total	Required	
	Rainfall	Supply	Supply	Demand	Stored	Amount	Tank	
		Liters	Liters	Liters	Liters	Stored	Volumn	
103	101.7	4881.6	679531.2	1500	3381.6	529531.2		48
104	85.2	4089.6	683620.8	1500	2589.6	532120.8		48
105	134.2	6441.6	690062.4	1500	4941.6	537062.4		48
106	270.0	12960.0	703022.4	1500	11460.0	548522.4		48
107	241.1	11572.8	714595.2	1500	10072.8	558595.2		48
108	329.8	15830.4	730425.6	1500	14330.4	572925.6		48
109	247.6	11884.8	742310.4	1500	10384.8	583310.4		48
110	129.6	6220.8	748531.2	1500	4720.8	588031.2		48
111	42.3	2030.4	750561.6	1500	530.4	588561.6		48
112	159.1	7636.8	758198.4	1500	6136.8	594698.4		48
113	17.2	825.6	759024.0	1500	-674.4	594024.0		48
114	26.5	1272.0	760296.0	1500	-228.0	593796.0		48
115	17.2	825.6	761121.6	1500	-674.4	593121.6		48
116	37.2	1785.6	762907.2	1500	285.6	593407.2		48
117	197.4	9475.2	772382.4	1500	7975.2	601382.4		48
118	320.0	15360.0	787742.4	1500	13860.0	615242.4		48
119	328.4	15763.2	803505.6	1500	14263.2	629505.6		48
120	343.5	16488.0	819993.6	1500	14988.0	644493.6		48



Though accurate it is too complicated a method to determine the storage capacity when a project involves close to a hundred houses of different roof catchment sizes.

Here it is useful to prepare graphs, applicable to any roof sizes and demand related to a set of rainfall data, relevant to an area or region.

These graphs are named as Rain Region Graphs in this report. Details of these Rain Region graphs are given in the section 6.5.2.2.

6.5.2.2. Rain Region Graph

For the Badulla region rainfall data, the rain region graph is given in graph A of Annex 8.

Rain Region Graphs for

Haputale]	Badulla District
Ratnapura	}	
Ambilipitiya	}	Ratnapura District
Kolonna	}	
Kekenadora]	
Aninkanda]	Matara District

are given in Annex 8. These represent high & low average rainfall regions in the three districts.

This is a useful graph though it was derived from a particular roof. It works for all demands for any roof area and with any run off co-efficient. This graph can be used in the field to analyse individual systems located in one area. The graph is prepared by repeating mass curve analysis for a set of data using different demands. These graphs can be plotted easily by regional technical staff.

Assumptions used in the above analysis.

- Demand is the same for every month.
- Demand is constant from year to year.
- Rainfall pattern in the future will be similar to pattern of rainfall data used.
- Evaporation from tanks is included in the run off co-efficient.

6.6. Construction

Construction of a Rainwater Harvesting system include the catchment, the gutter system, storage and a water extraction device.



6.6.1 Roof catchment

The roof should be made of suitable materials such as galvanized iron (G.I.) sheet. Thatched roofs are not suitable as decaying vegetative materials would add taste and colour to the water. However this water can be used for livestock irrigation and to flush toilet. There should be no trees over shadowing the roof as falling leaves also would act similarly. If GI roofs are painted the paint should be non toxic. Generally there is a fear of using asbestos roofs as rainwater catchment. Some authorities maintain that this fear is not justified as the fibre causes cancer only when inhaled (**Annex 12**). Tiled roofs have the drawback, that they are difficult to clean, and are susceptible to algae growth. The best option seem to be GI sheets painted with non toxic paint.

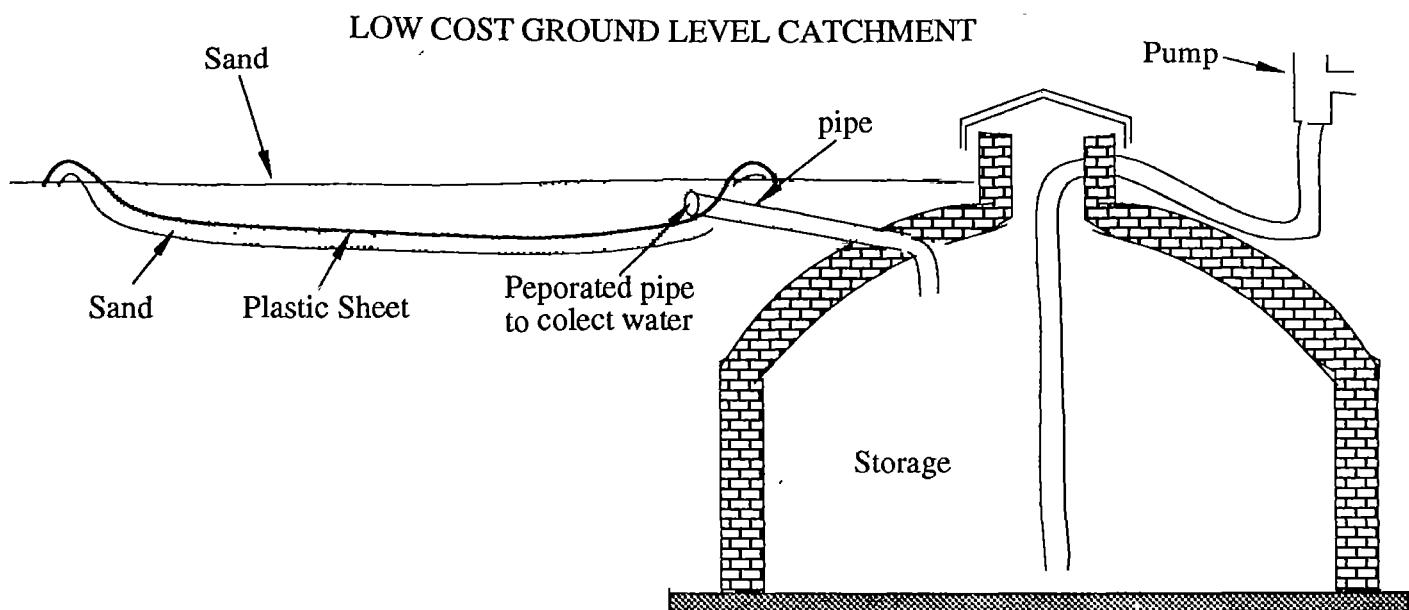
Most roofs in rural Sri Lanka are made of or fast becoming made of GI sheet or tiles.

6.6.2 Surface catchment

Where there is no suitable roof catchment rainwater can be harvested by construction of an impervious surface on the ground itself.

Chicken wire re-inforced concrete floor costs about Rs. 250/m²

A cheaper catchment surface can be made by laying a piece of plastic sheeting in a shallow excavated and levelled area as given in the drawing. The estimated cost to be around Rs. 50/m² for a 60/m² area.





6.6.3 Gutter System

Effective guttering is an important part of the roof catchment systems. GI and UPVC can be used for gutters and down pipes. Sizing will depend on the roof area.

A facility to catch the first flush or bypass for flushing the roof is essential. For small systems this can be done by simply fixing a small length of flexible hose at the end of the down pipe. When the roof is being flushed the flexible hoses should be taken out of the storage tank inlet, and directed to a drain. Once the roof is clean this could be inserted back into the storage tank.

Just before the rainy season the roof is usually cleaned by sweeping off the impurities collected on it such as dust, leaves, bird dropping etc. The first rainfall is then used to flush the roof by keeping the bypass open.

Table 6 ~ 14

Standard PVC Gutters and Down Pipes for a 60m² roof. (length of gutters - 15 meters)

Item	Unit	Qty	Unit Cost	Cost
Gutters	meters	15	87	1305
Clips	No	25	13	325
Center Running Head	No	02	80	160
Down Pipe	meters	7.5	60	450
TOTAL				2240

Cost (May 95) Rs.

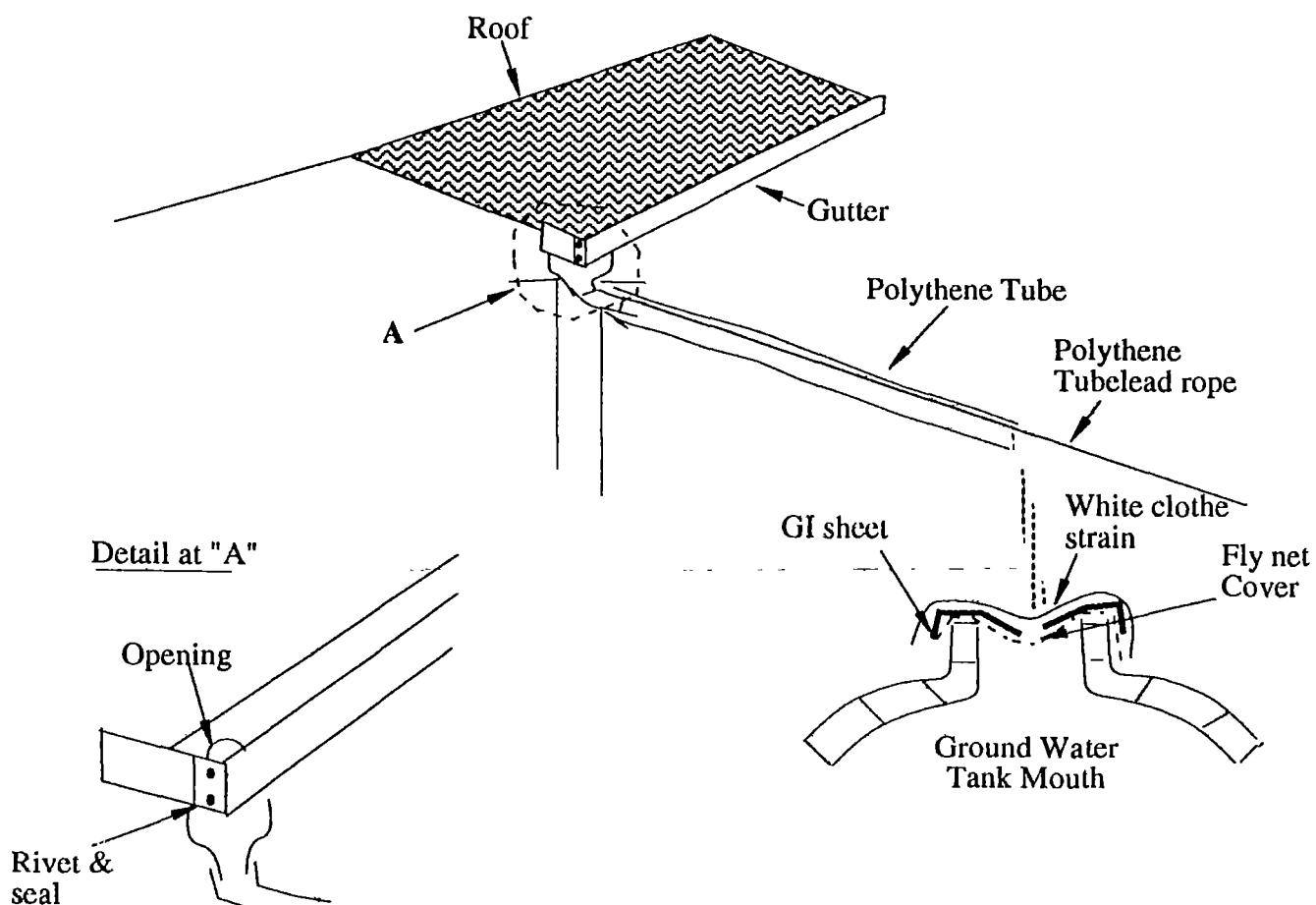


Table 6 - 15

Low cost GI sheet gutters and polythene tube down pipe for a 60m² roof.
 (Length of gutters - 15 meters)

Item	Unit	Qty	Unit Cost	Cost
GI sheet	M ²	6	100	600
Nylon Rope	M	12	7	84
Polythene Tube	M	6	6.50	39
Other				100
TOTAL				823

Cost (May 95) Rs.



6.6.4 The Storage Tank

A satisfactory storage tank is the most important part of a Rainwater Harvesting System. Its construction must be simple to manage at rural level, and result in a durable tank.

Three trial tanks were constructed to test various tank options. Details are given in chapter 7.



Table 6 - 16
Comparison of Different Tanks

Type of Tank	Total Cost M ³ (1995)	Can be Built above Ground	Resistance to UV Light	Minor Repairs at Rural Level	Remarks
Fibre Glass	5500	Yes	Poor	Difficult	
HDPE	5500	Yes	Good	Difficult	
Ferrocement	1468	Yes	Good	Easy	Cost can be brought down
Brick dome	1318	No	Good	Easy	Can be built above ground with re-enforcement.
Jar	1874	Yes	Good	Easy	Cost can be brought down

6.6.5 Water Extraction Device

When storage tanks are build above ground water can be extracted by fixing a tap at the bottom of the tank or by siphoning the water with a tube with a tap attached at the point of collection.

When storage is underground a low-cost home-made PVC pump can be used to extract the water.

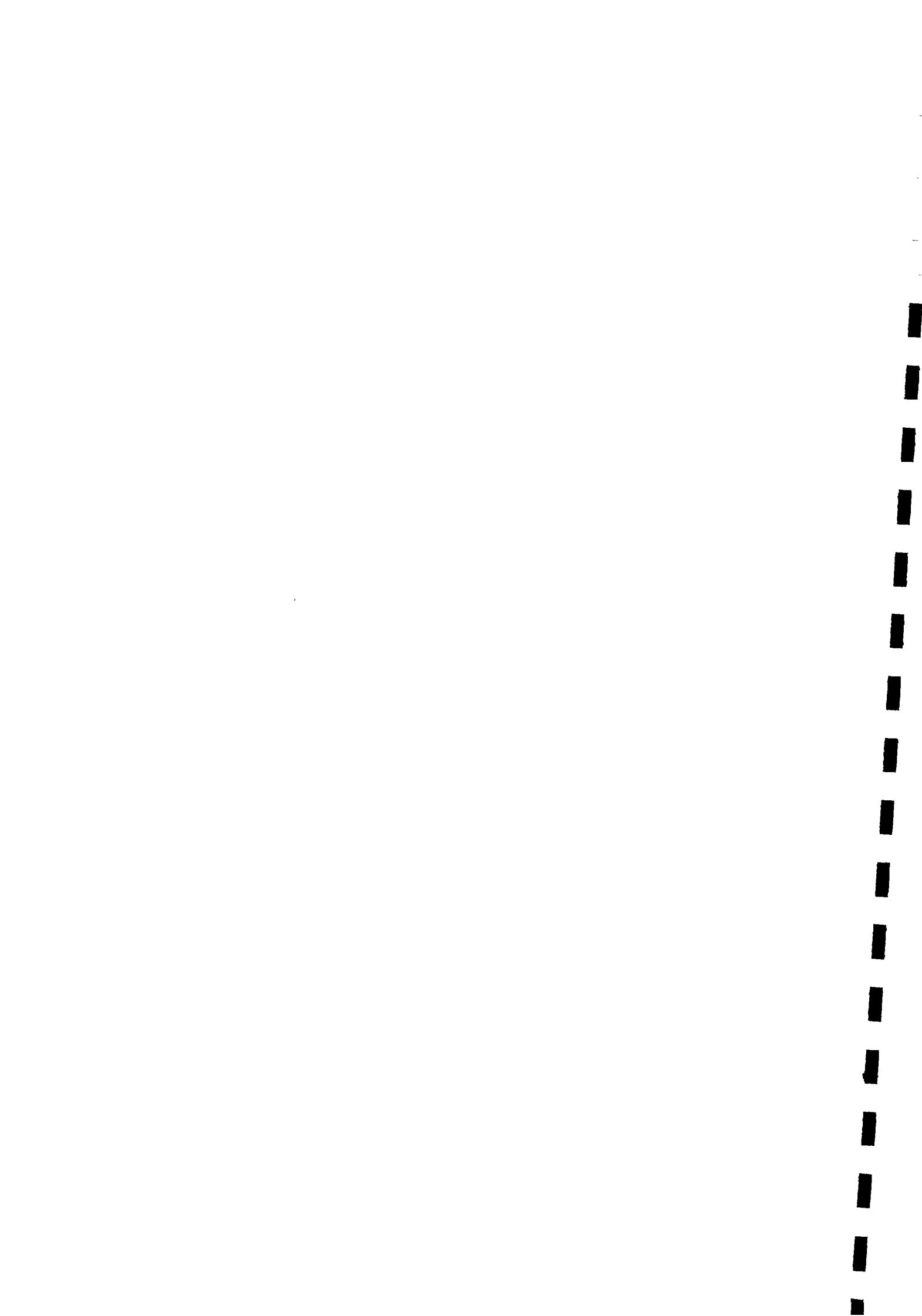


Table 6 - 17 gives the material and cost breakdown.

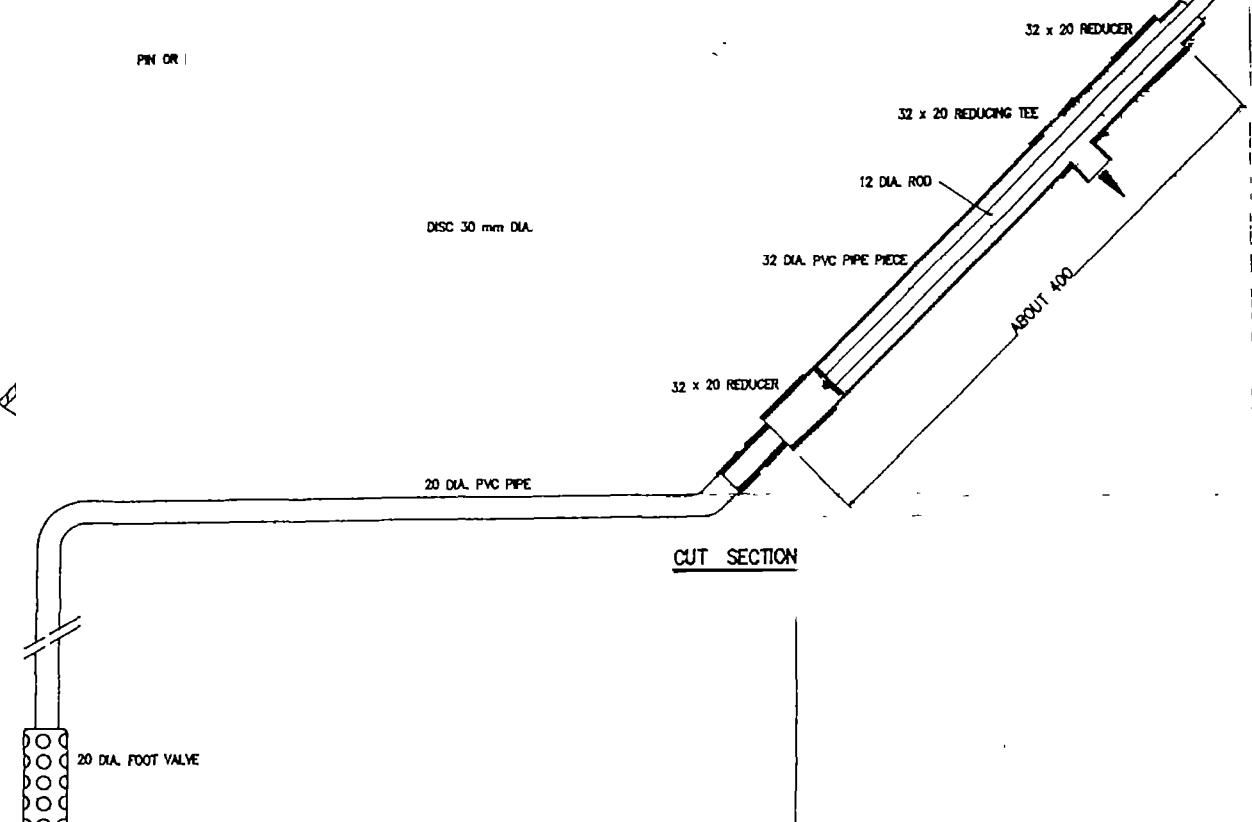
Table 6 - 17

**Rain Water Harvesting
Low Head Home Made PVC Hand Pump**

Item	Unit	Qty	Unit Cost	Cost
3/4" Foot Valve	No	01	150	150
3/4" Valve Socket	No	01	10	10
3/4" Bend	No	02	10	20
1 1/4x3/4 Reducing Socket	No	01	22	22
1 1/4" Pipe	Mtr	0.5	65.6	32.8
3/4" Pipe	Mtr	4	30	120
Plunger	No.	1	30	30
TOTAL				424.8
		Say		450/-

Costs (May 95) Rs.

PLUNGER DETAIL





7. Technical Options Tested

Three types of storage containers were constructed as trials. The objective being to build tanks with 5M³ storage capacity at a cost below Rs. 5400/-, excluding unskilled labour.

7.1 Ferro-Cement Tank

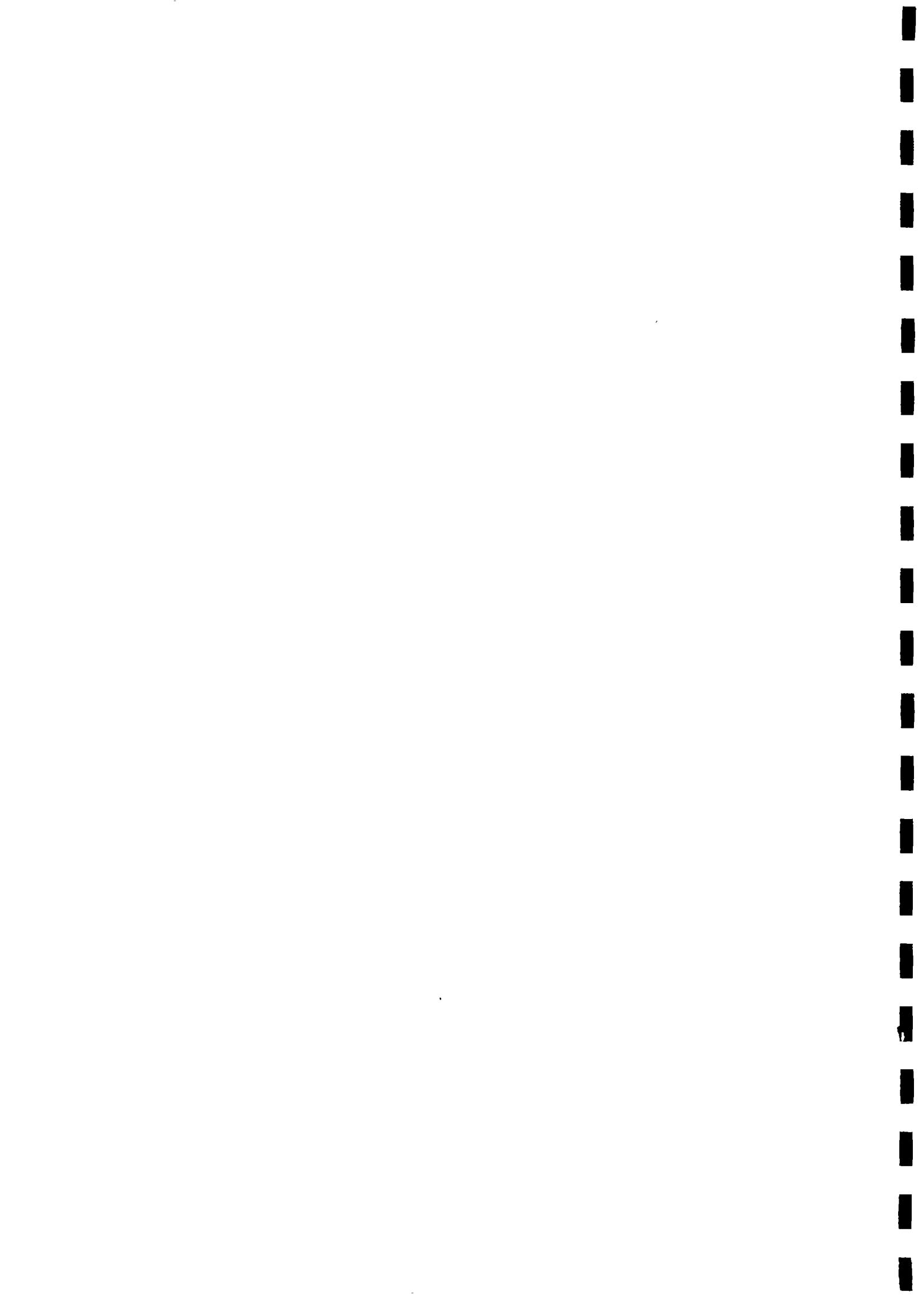
The ferro-cement tank (built above ground) is based on an idea by Neil Herath - Rural Water Supply Engineer (CWSSP). It is a pumpkin shaped 5M³ ferro cement tank was successfully constructed by R.M.N.D. Illukumbura Senior Technical officer Ratnapura CWSSP.

A skeleton mould, made out of shaped 1" 'L'irons, is fixed around a circular foundation with horizontal rings made of 6mm mild steel bars at different heights to stabilise and to give the pumpkin shape. Two layers of 1/2" chicken-mesh are used as re-inforcement.

Material and cost break-down is given in Annex - 4.

Tank drawing is given in Annex - 3.

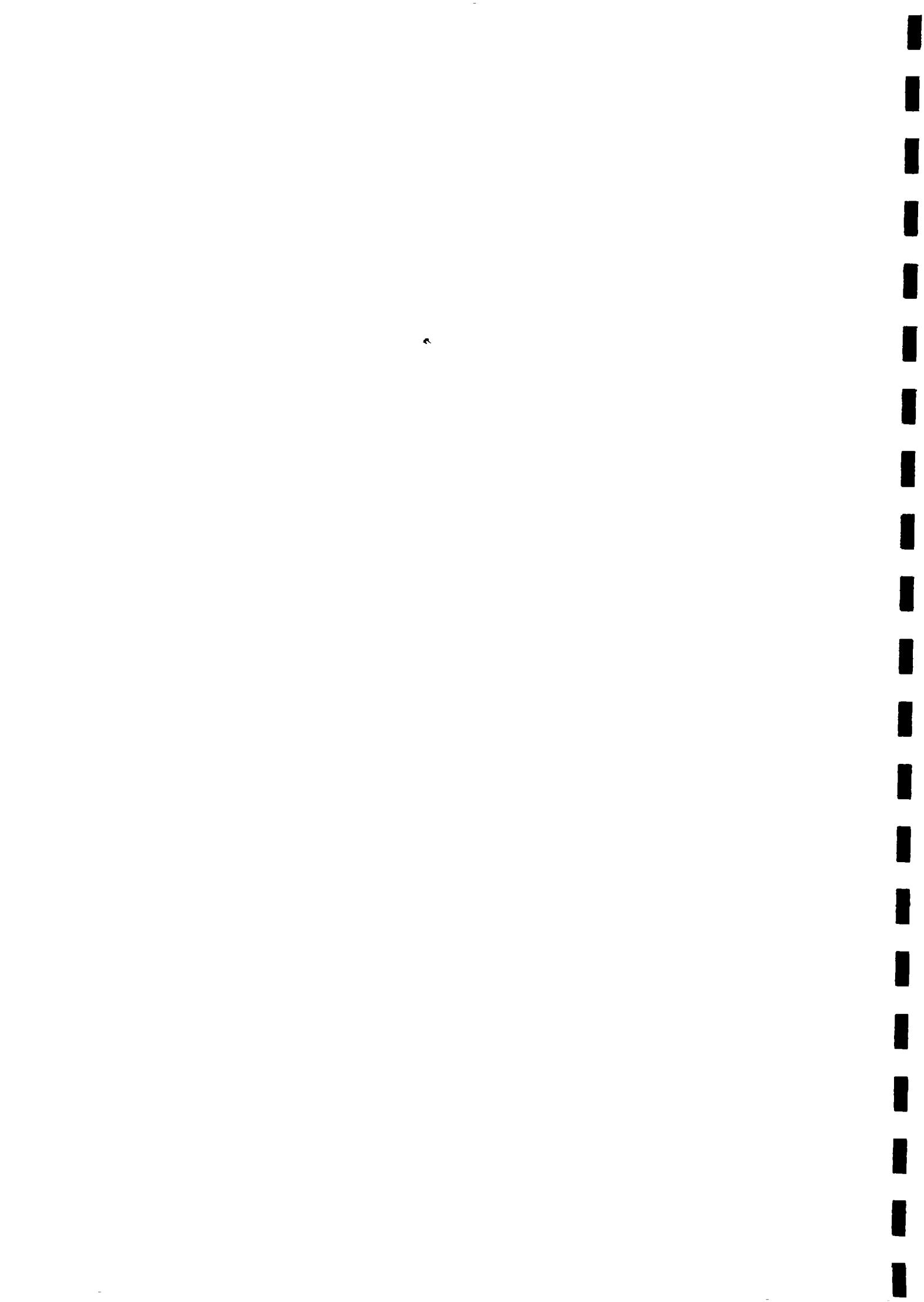




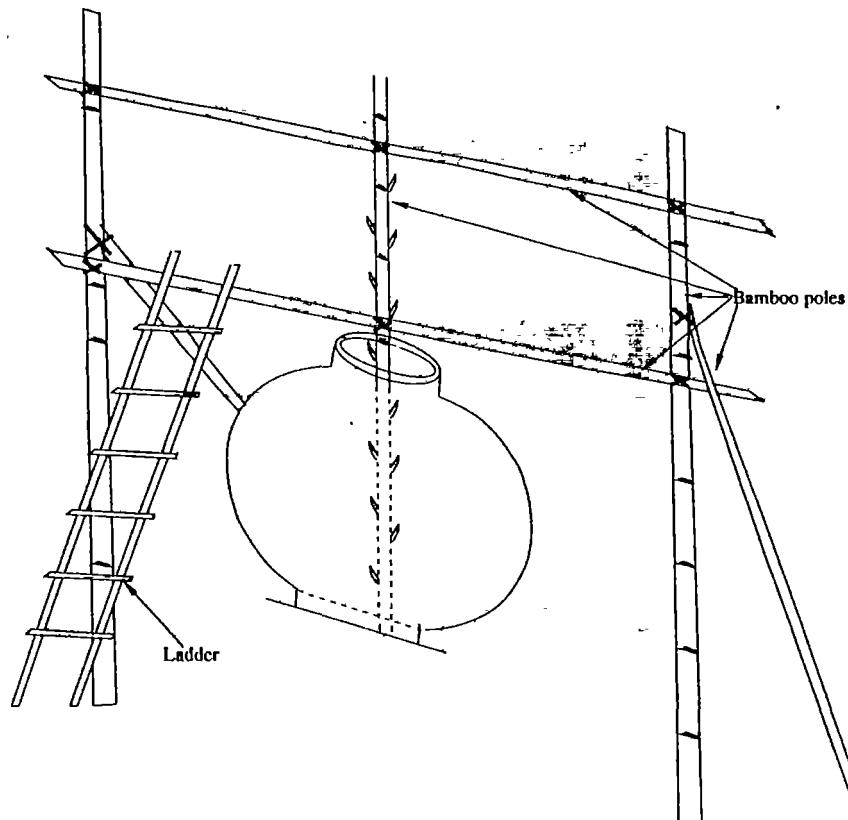


Actual material plus skilled labour plus mould cost of the tank is Rs. 5441. Under normal circumstances the cost of the ferro-cement pumpkin shaped tank is above the project criteria.

However by over-coming various constraints and delays that occurred during the construction phase, it should be possible to bring down the cost to meet financial project criteria. The construction method had many novel features, and with experience, the construction time will be reduced saving on skill and labour costs.



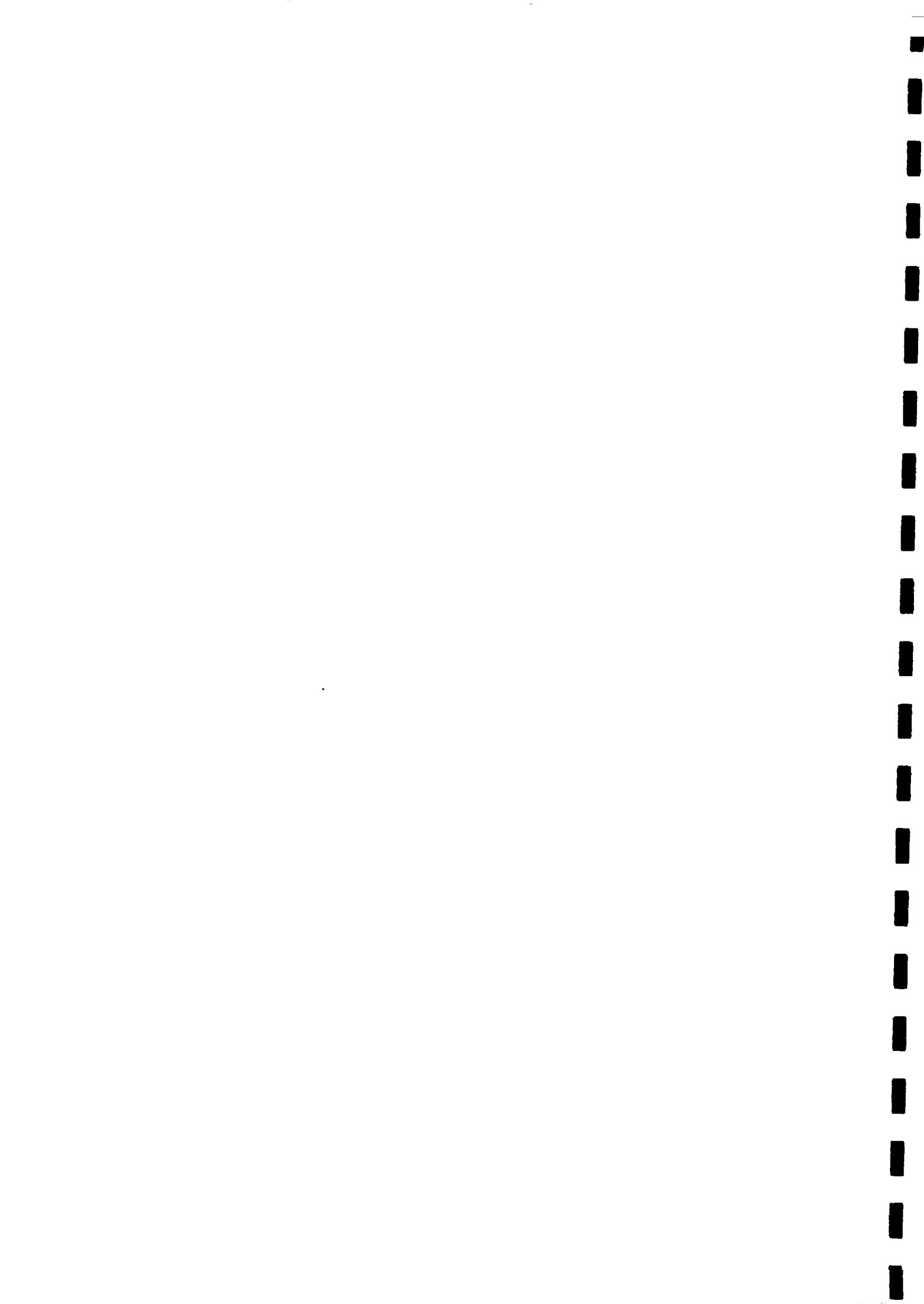
Construction Phase scaffolding arrangement is given below :



Illukumbura suggests

- To reduce the time of skilled labour and cement waste.
- 1. The skeleton mould to have at least 8 verticals and 6mmΦ re-bar (removable) horizontal rings, every 10 cm vertically.
- 2. To plaster the exterior of the walls first and to remove the mould from inside the tank to do the inside plaster, and complete the tank.

This trial tank was built at Paradise School premises in Kuruwita Ratnapura. The co-operation and help of the school principal Mrs P.I. Wimalasiri must be mentioned here with gratitude.

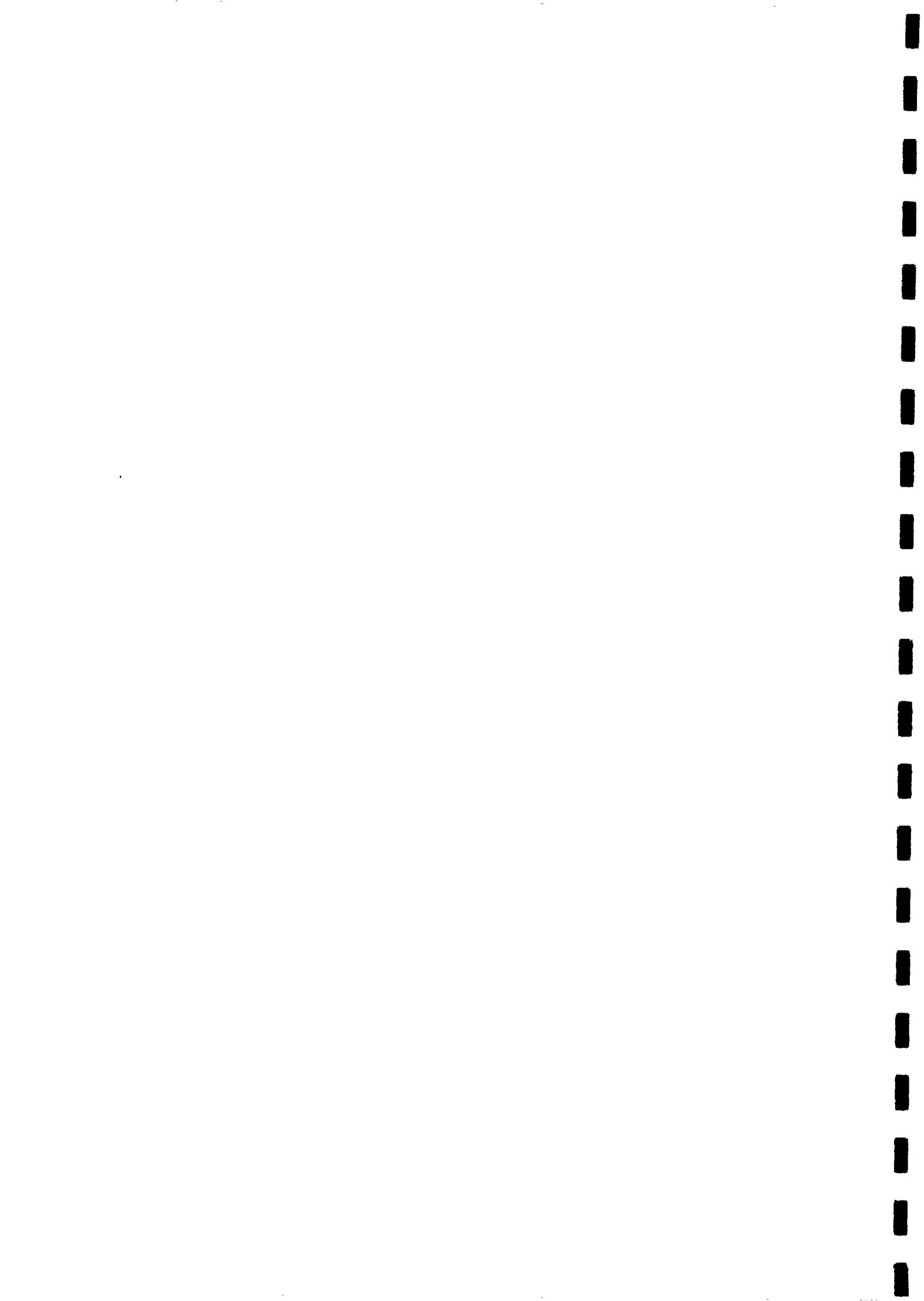


7.2 Brick-dome tank (built under ground)

The brick masonry tank was built at a potential rainwater harvesting site at Badulla. With actual material plus skilled labour the cost of the tank is Rs. 4298. In addition the transport of materials cost Rs. 1000/. Under normal circumstances the brick rainwater storage tank will be acceptable within the project criteria and will be affordable to the householder in terms of labour and cash.

The roof of the tank is made of 1/4 brick thick in the shape of a dome without the use of a mould. The tank can be completed by a crew of one skilled worker and three helpers in three days, excluding excavation.







An engineer and a skilled worker from the NERD Centre Ja-Ela, conducted a training course in the construction of the tank, for the technical staff and village masons involved in the project in the Badulla District. The tank is currently being inco-operated into a rainwater harvesting system.

The trial tank construction at Badulla, included the following input from the Regional Office.

- Selection of a site at a project village.
- Supply & transport of materials to site.
- Provision of transport for trainees and trainers, from the Regional Office to the site for 3 days.

The Regional Director and District Engineer gave their fullest support in arranging these inputs. Special mention must be made of young resource engineer Wijaya Widhyaratne and CRO Sunil Ratnasiri for their positive attitude, which enabled the work to get organized with short notice, to be completed on time.

Material and cost break-down in **Annex 6**.

Tank drawing in **Annex - 5**.



7.3. Cement Jars

Cement Jars of 1 to 2 M³ capacity are popular rainwater storage containers used in Thailand. Investigations reveal that these Jars are not made in Sri Lanka. Available data on cement jars were collected.

Trial Jar of one above 1M³ capacity was constructed at National Engineering Research and Development Centre Ja-Ela.

One layer of 1/2" chicken mesh fixed on to a skeleton made of 6mm re-bar placed 9" apart both ways (horizontally and vertically) and plastered with 1:3 cement sand mortar to a 1" thick wall. The inside is made water-proof by painting with cement slurry.

Cover is made separately with 1/2: "chicken mesh" re-inforced cement mortar and fixed on to the lower section, which has the shape of a bucket.

Drawing is given in Annex - 11.

Cost break down is given in Annex 13.

7.4 Clay pot or Jars

Clay pot of upto 200 liter capacity are made at Molagoda on the Kandy, Colombo Road.

Market price of a 200 liter Clay Jar or Pot is Rs. 1500/. Cost per liter Rs. 7.50.

Conclusion - Cost per liter is too high compared to the cost of all other types of storage tanks.



8. Pilot Project

Three villages in the three districts, where standard options, are not feasible due to technical economic and social reasons, were identified and visited.

They are:

8.1. Madawatugoda Upper Section, in Omalpe Ratnapura District.

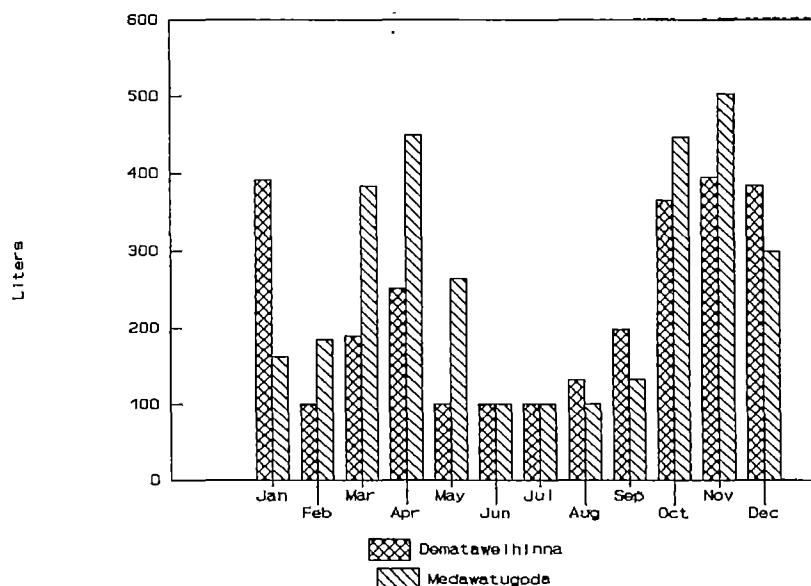
Here about 40 tile-roofed small households live on the slope of a high hill. Few springs are available below house levels, but they are used to irrigate the paddy lands below, and the farmers do not allow them to be used for piped domestic supply.

Two visits were made to Madawatugoda during the period of study. The climatically closest meteorological station to Madawatugoda is at Kollone, with an average annual rainfall of 1.7 meters. (1955-1965).

Available tile & GI sheet roofs can be used as catchment areas. Roof areas are generally above 40M².

Graph N gives minimum dry season supplies from varying roof-catchment in a day in a ten year dry year. Required storage is given as 5M³ which could be constructed within project criteria. As catchment roof areas differ from house to house with a 5M³ storage tank the service level too changes. However the dry season service level will be a substantial improvement from the present status of water-supply of the majority of the households.

Bar Graph 3.1 & 3.2



Here rainwater harvesting is technically and economically feasible to improve the present status in water supply. Bar graph above gives the supply possible from typical system in a normal year. System include 60m² catchment & 5m³ tank.



The option can be put forward to the beneficiaries, and if they choose it as the preferable option, the design work can start.

8.2. Dematawelhinna Village in the Badulla District.

Dematawelhinna village is situated about 6 miles from the Regional Office, Badulla on top of the slope of a hill, 205 families live here. Houses are built of mud bricks. Most houses have GI corrugated-sheet roofs. Roof areas vary between 30 to 100 m². In the dry season women collect water in pots from the water holes located at the bottom of the hill.

Rainwater harvesting is a new concept to the village. Presently about 10 to 20 pots of water is required per day per house. When explained the building of tanks big enough to store the number of pots of rain water required per day-times the number of dry period days, it is easily understood by the householders.

With the advice of the DD/T the first brick-dome trial tank was constructed at a household in this village. Since then the understanding & enthusiasm on rainwater harvesting has increased according to Resource Engineer Mr. Widyaratne. Number of householders have made requests for rainwater storage tanks.

Other options, such as gravity pipe systems, dug wells are not feasible at Dematawelhinna, according to CRO and villages.

A pump-water scheme is possible. For this water must be bought from the Water Board and pumped up a nearly 100m and stored for distribution. The Regional Office estimate is Rs. 140/- month per house maintenance. This is not affordable to the villagers, according to the Chairman of the CBO for running cost and most villagers have no regular income.

At a meeting held at the village presided by Regional Director CWSSP Badulla, an awareness presentation on rainwater harvesting was conducted. Since over one hundred applications requesting rainwater harvesting systems were received by the CWSSP Regional Office Badulla. Design and Construction of this project is expected to begin in August '95.

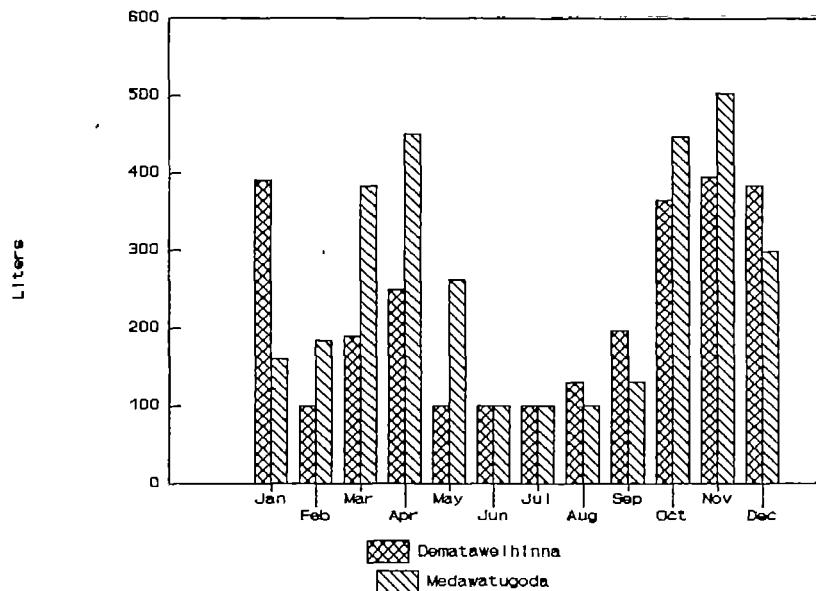
The climatically closest meteorological station to Dematawelhinna is at Badulla, with an average annual rainfall of 1.75 meters (85-94). Graph X (Annex - 10) a gives possible dry season supply in liters from a roof catchment in a day from a 5M³ storage tank system in a ten year dry year.

Available roofs are mostly GI and vary in area. These can be used as roof-catchment.

With a 5M³ tank which can be constructed within CWSSP criteria, it is possible to improve the present water-supply status to different levels depending on the size of the catchment roofs. Supply from a typical system in a normal year is depicted in the bar graph below.



Bar Graph 3.1 & 3.2



Therefore rainwater harvesting is technically and economically feasible to improve the present status of water supply.

8.3. Dorsar Kanda Village Matara

A visit was made to the village with CRO/T and the Community Facilitator.

The village is situated on a hill about 6 Km from the Matara Regional Office. Half of the families live close to the bottom of the hill where shallow wells are possible.

The highest point is about 40 m above ground-water level. A few houses have permanent roofing made of tiles. Most houses have thatched roofs.

Most householders have taken house building loans recently and have started to build better houses with permanent roofs. Electricity is available at the bottom of the hill. A dirt road is available upto the top of the hill.

A few members of the CBO were contacted including the President, and the priest of the village. It is their aspiration to get both water and electricity to their houses, which they see available at low-income houses close by.

However, they are not ready to pay more than their counterpart in the town for pipe water. This issue needs more investigation and analysis.

The original design included a pump pipe scheme.



The current rainwater-harvesting practice is only to collect small quantities of water from tree trunks.



Climatically closest meteorological station to Dorsarkanda village is at Kekenadora, with an average annual rainfall of 1.23 meters. (80-89). Graph Y gives possible dry season supply in liters from roofs of varying sizes in a day, using a 5 M³ storage tank system in a ten year dry year.

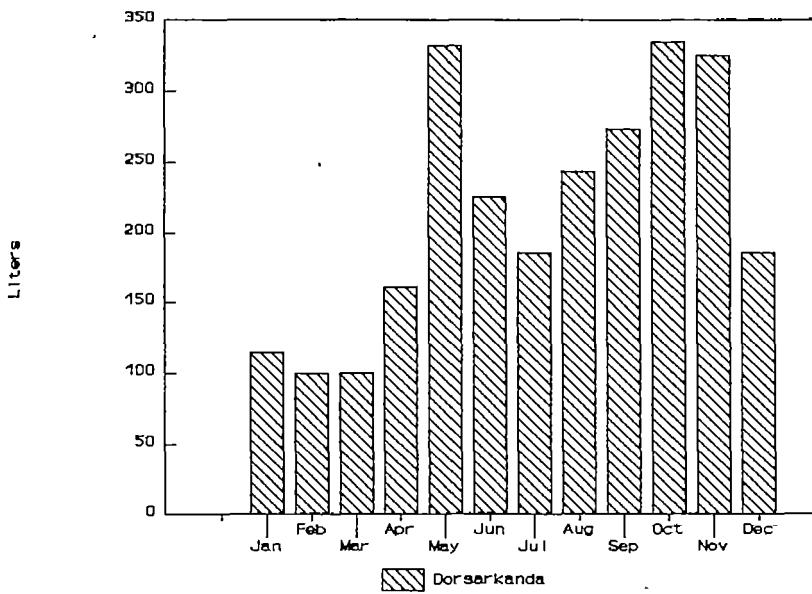
Available roofs are mostly thatch and are not suitable for rainwater harvesting. To do rainwater harvesting, first a suitable catchment must be constructed.

Once suitable catchment is available, rainwater harvesting becomes technically and economically feasible to improve the present status of water supply.



Supply from a typical system in a normal year is depicted in the bar graph below. System consists of 60m^2 catchment & 5m^3 tank.

Bar Graph 3.3





9. Conclusion and Recommendation

9.1. Technical

The rainwater Harvesting Action research concludes that rainwater harvesting is technically feasible in the three districts of Badulla, Ratnapura and Matara.

Rainfall is adequate and most buildings have suitable roof-catchment.

The research recommends the design and construction of the three pilot projects already identified, at Badulla, Ratnapura and Matara. Monitor these projects after construction and review the technical, economic and social aspects and the policy on rainwater-harvesting accordingly.

9.2. Economic

The study concludes that it is possible to build a 5000 liter storage tank with brick (underground) or ferro-cement (over ground) to cost less than Rs. 5400 excluding unskilled labour. However, the level of service from a 5M³ storage tank will vary according to the rainfall pattern of the location and the size of the catchment area used.

The research recommends the continued construction of ferro-cement type trial tanks in order to bring the cost down further and improve the design.

9.3. Social

A vast majority of potential beneficiaries specially the lower income groups do not understand the full benefit of rainwater-harvesting. Reliability of rain as a source and the quality of rainwater are their main concerns.

It is recommended to conduct an awareness campaign under the CWSSP, targeted to potential consumers on rainwater harvesting.

The potential beneficiaries include houses located at higher elevation and away from the existing sources, where specially women have to walk long distances to fetch water.



9.4. Design

The study recommends the preparation and use of Rain Region Graphs to design the size of tanks, for a set of rainfall data. The required tank sizes can be determined for different catchment areas and demands, by the use of 'Rain Region' graphs. Rain Region graphs should be prepared at Head Office or Regional Office levels of CWSSP with available monthly rainfall data for each region where the rainfall pattern is similar.

Higher storage is expensive to build. The alternative is to reduce the demand in a ten year dry year. For drinking and cooking 6 lit per capita per day can be considered as standard. Where roof-catchment is limited, the next option is to build low-cost ground level catchment with underground storage tank.

9.5. Construction

The construction of Pilot Projects should be supervised direct from the Regional Offices with maximum community involvement.

Training on low-cost tank construction should be given to relevant masons and supervisors prior to actual construction. These training costs must be budgeted for in addition to the pilot projects.

With relevant experience gained from the pilot project the next step should be to train Technical Officers of the Partner Organizations in designing and the construction of the rainwater-harvesting systems.

9.6. Quality

The quality of rainwater depends on how clean the atmosphere is. The cleanliness of the material of the catchment surface, gutters and down pipes, the storage tank and the water extraction device, determines the quality more significantly.

The atmosphere is considered to be clean in the rural and small town areas where the CWSSP is being implemented.

The best surface for a catchment is the G.I. or Aluminium sheet roofs, Tiles, asbestos and plastic are only satisfactory.

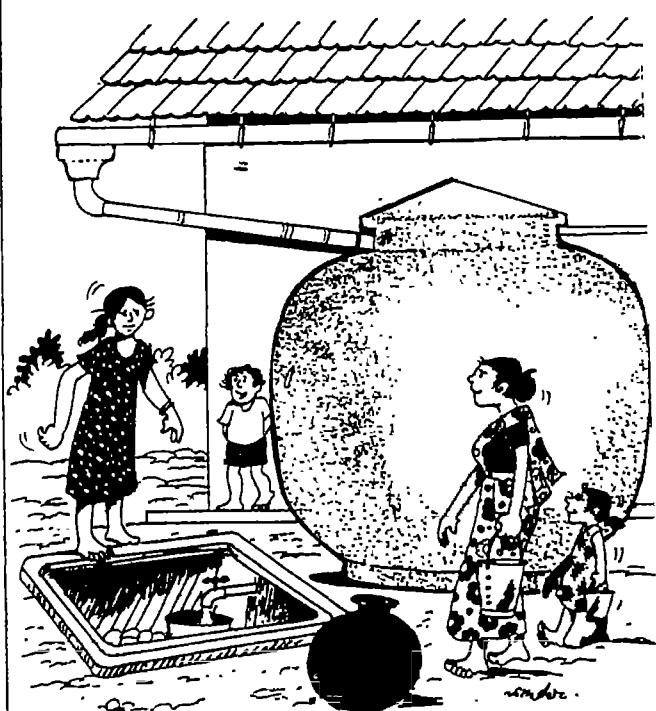
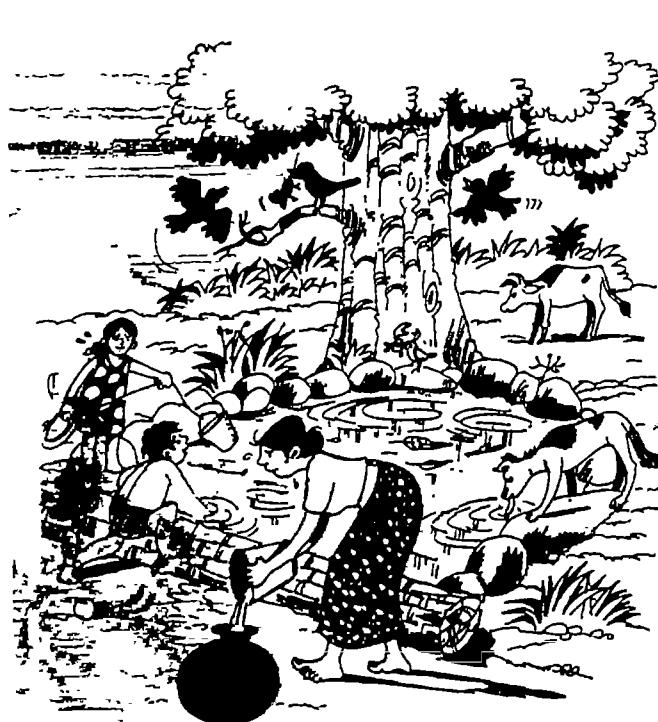


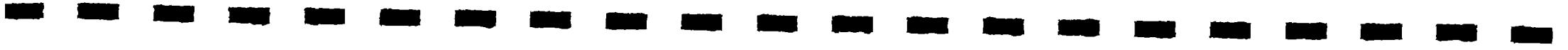
The gutters and down pipes made of GI or PVC or polythene are considered satisfactory.

Storage tanks should be covered and made mosquito proof. Where there is any chance of pollution, the pot method of chlorination can be used to keep the water clean.

Water should be extracted from the tank by means of a pump or siphon pipe or gravity tap and not by bucket to prevent human contamination.

Rain water harvesting has the distinct advantage of being a separate system for each household. This prevents any outside contamination of the tanks.





RAINWATER HARVESTING - ACTION RESEARCH**Task No.**

1. Design a functional water storage system capable of holding 5,000 litres and costing not more than Rs.5,400 (excluding unskilled labour costs).
2. Construct sufficient number of prototypes of the above to ensure that after appropriate artisan training they can be constructed without major difficulty in a village situation using typically available local labour and materials.
- ✓ 3. Conduct a brief survey of the experience to date with rainwater harvesting in Sri Lanka and record any significant lessons of either technical or social significance.
4. Visit and investigate the two villages (Badulla & Matara) where options other than rainwater do not appear to be available. Assess the level of interest/demand of the villagers and, if favourable, seek their agreement to participate in a pilot project.
5. With the assistance of CWSPU District staff, conduct a pilot project in the two villages in a manner such as will generate maximum community involvement and contribution.
6. Review likely demand and physical potential for ground-level rainwater harvesting and, if appropriate, make recommendations for further development.
7. Based on the pilot experience and other relevant Sri Lankan experience, make appropriate recommendations for the incorporation of rainwater harvesting options in the CWSSP
8. Prepare summary training material so as to transfer necessary skills to CWSPU technical staff.

TIME ALLOCATED

A. TECHNICAL

B. COMMUNITY

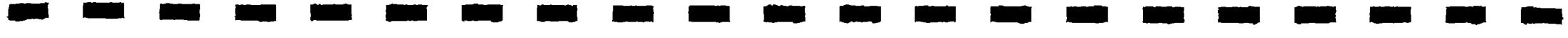
REMUNERATION RATE

CWSPU standard rates to be paid.



Main Reports and Publications Consulted

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Annex 2



RAINFALL ANALYSIS

STATION : UPPER OHIYA ESTATE

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	274.8	114.7	77.2	124.6	112.2	17.7	218.1	29.7	76.2	335.6	601.2	99.3	2679.2
1961	256.5	240.2	164.4	277.8	220.2	32.5	38.1	54.1	88.3	279.6	291.0	244.8	2207.5
1962	153.1	96.2	221.7	297.4	228.0	55.6	75.1	116.5	104.1	381.5	321.5	279.4	2330.1
1963	349.5	253.2	356.8	447.2	204.7	56.1	50.0	22.3	137.1	434.0	508.0	287.0	3105.9
1964	209.8	200.9	202.4	494.0	148.6	77.9	125.7	100.8	152.9	148.5	55.6	162.6	2079.5
1965	79.5	101.6	286.5	753.3	218.6	5.5	5.5	136.1	68.5	369.5	305.3	298.7	2628.6
1966	182.3	57.4	268.6	403.6	48.0	31.2	20.3	64.0	213.8	261.1	133.3	212.0	2192.6
1967	233.6	177.0	221.4	153.1	85.0	34.7	6.0	101.6	21.0	268.9	419.3	151.3	1901.9
1968	149.6	46.2	254.7	216.9	130.5	50.8	38.6	26.6	31.2	523.4	346.9	340.1	2155.6
1969	265.1	102.6	17.2	310.3	17.7	27.4	65.7	241.0	63.8	593.3	276.6	174.7	2475.4
1970	186.6	260.4	313.9	449.0	176.7	46.4	33.7	31.2	94.9	248.8	62.2	345.9	2255.7
1971	320.5	174.4	168.4	402.3	40.1	60.7	101.8	170.4	284.9	183.6	161.8	146.0	2534.9
1972	98.8	0.0	140.7	249.4	220.9	42.6	57.4	19.0	164.8	463.2	728.9	160.3	2366.0
1973	48.0	117.6	136.1	264.9	116.3	67.0	113.5	62.9	50.8	408.1	327.4	594.3	2306.9
1974	61.2	200.9	74.6	303.0	220.9	15.2	40.2	50.8	182.8	133.8	381.0	264.1	1956.5
1975	194.5	109.2	144.7	436.8	215.9	45.7	66.0	121.9	160.0	80.8	495.3	205.7	2246.5
1976	299.4	69.3	221.9	426.2	218.6	139.4	29.2	152.1	75.8	281.1	729.4	371.8	3013.8
1977	8.8	215.6	232.1	831.1	378.2	43.6	126.4	104.3	173.9	654.0	633.9	279.9	3361.8
1978	77.9	189.9	286.0	236.4	281.4	23.6	153.6	69.8	111.6	432.3	319.5	378.4	2560.3
1979	50.8	188.9	46.2	361.7	106.4	39.1	63.2	40.3	339.8	412.4	623.0	180.8	2442.3
1980	36.0	84.0	146.0	410.2	292.1	60.9	8.8	71.8	133.8	303.5	497.0	261.1	2305.2
1981	175.1	36.3	183.9	183.2	196.9	42.7	207.8	69.4	159.9	256.8	316.8	113.9	1942.7
1982	26.5	177.5	313.8	194.1	318.0	93.4	12.9	82.6	85.8	267.7	126.8	274.3	2273.1
1983	56.8	20.4	82.6	48.7	201.3	24.8	45.0	480.0	63.8	308.8	390.7	723.2	2447.9
1984	393.2	570.8	581.9	593.0	209.2	70.8	116.7	152.1	273.4	303.8	439.1	276.1	3980.1
1985	162.2	286.7	351.4	321.3	199.0	179.9	57.8	91.1	64.8	171.9	407.6	433.6	2727.2
1986	798.0	141.2	293.3	830.6	292.7	29.6	32.6	91.1	66.8	241.5	142.0	112.3	3397.7
1987	157.9	46.8	366.0	346.3	287.8	43.9	4.3	67.4	815.9	1599.1	690.6	138.6	4264.6
1988	77.1	387.4	211.9	722.1	103.0	27.5	49.3	216.6	120.3	66.1	321.0	398.0	2698.9
1989	195.8	49.0	116.9	299.5	351.0	100.2	160.7	163.5	341.1	188.9	403.5	119.4	2519.5
AVERAGE	186.7	177.5	216.9	379.3	194.7	52.9	71.1	106.7	148.7	352.3	403.5	289.2	2579.3
STAND.DEV.	151.4	134.8	115.0	174.3	89.1	36.1	57.3	88.6	106.9	270.1	173.1	142.5	554.3
MAXIMUM	798.0	570.8	581.9	630.6	378.2	179.9	218.1	480.0	515.9	1599.1	729.4	723.2	4264.6
MINIMUM	8.8	0.0	17.2	48.7	17.7	5.5	4.3	19.0	21.0	50.8	55.6	99.3	1901.9

YEAR	TOTAL	RANK	PROBABILITY	10 Year Moving Average
				Year Avg.
1967	1901.9	1	0.03226	60 - 69
1981	1942.7	2	0.06452	61 - 70
1974	1956.5	3	0.09677	62 - 71
1964	2079.5	4	0.12903	63 - 72
1968	2155.5	5	0.16129	64 - 73
1966	2192.6	6	0.19355	65 - 74
1961	2207.5	7	0.22581	66 - 75
1975	2246.5	8	0.25806	67 - 76
1970	2255.7	9	0.29032	68 - 77
1982	2273.1	10	0.32258	69 - 78
1980	2305.2	11	0.35484	70 - 79
1973	2306.9	12	0.38710	71 - 80
1962	2330.1	13	0.41935	72 - 81
1972	2366.0	14	0.45161	73 - 82
1979	2442.3	15	0.48387	74 - 83
1983	2447.9	16	0.51613	75 - 84
1969	2475.4	17	0.54839	76 - 85
1989	2519.5	18	0.58065	77 - 86
1971	2534.9	19	0.61290	78 - 87
1978	2560.3	20	0.64516	79 - 88
1965	2628.6	21	0.67742	80 - 89
1960	2679.2	22	0.70968	
1988	2698.9	23	0.74194	
1985	2727.2	24	0.77419	
1976	3013.8	25	0.80645	
1963	3105.9	26	0.83871	
1977	3381.8	27	0.87097	
1986	3397.7	28	0.90323	
1984	3980.1	29	0.93548	
1987	4264.6	30	0.96774	

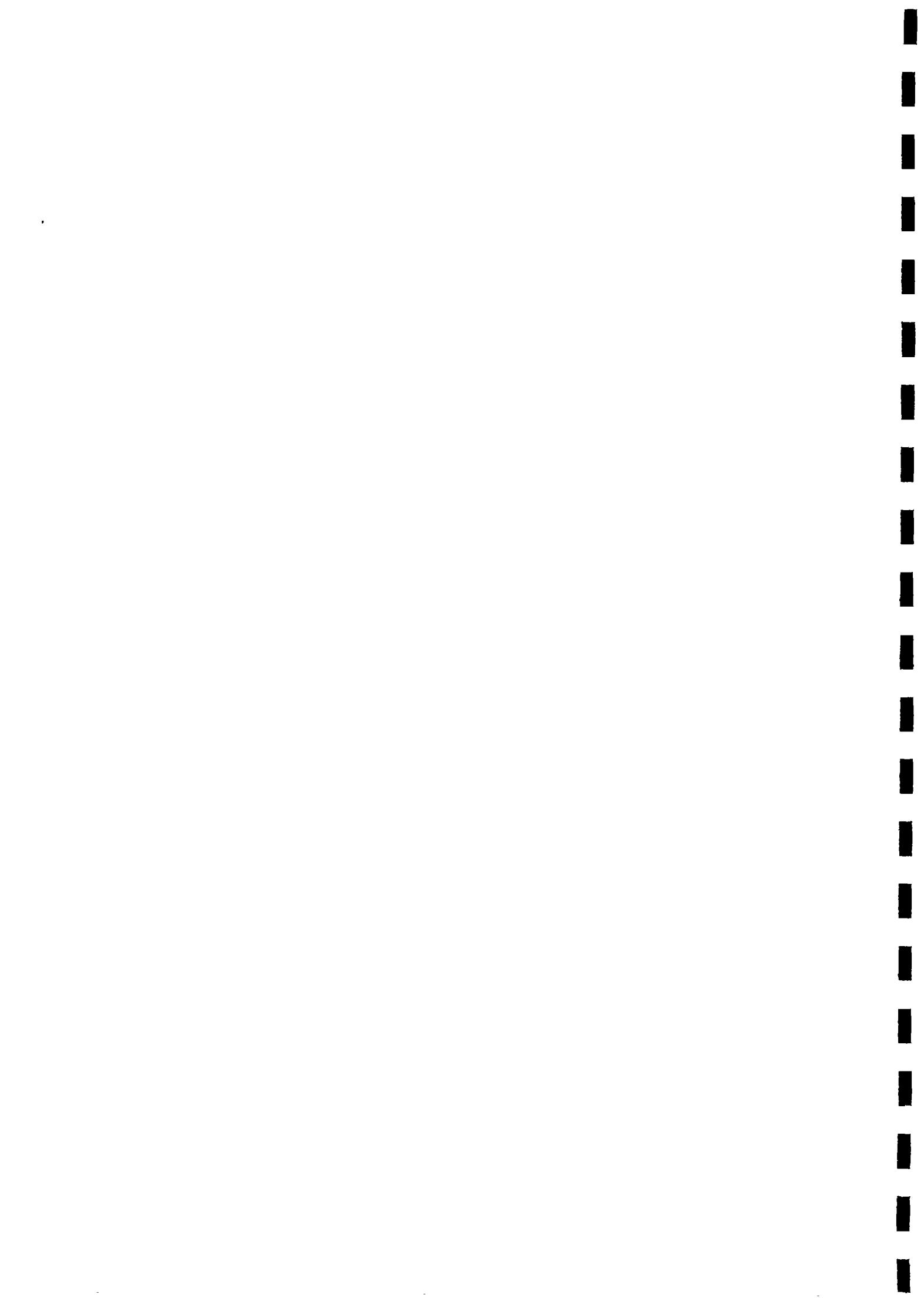


RAINFALL ANALYSIS

STATION 1: WELIMADA GROUP

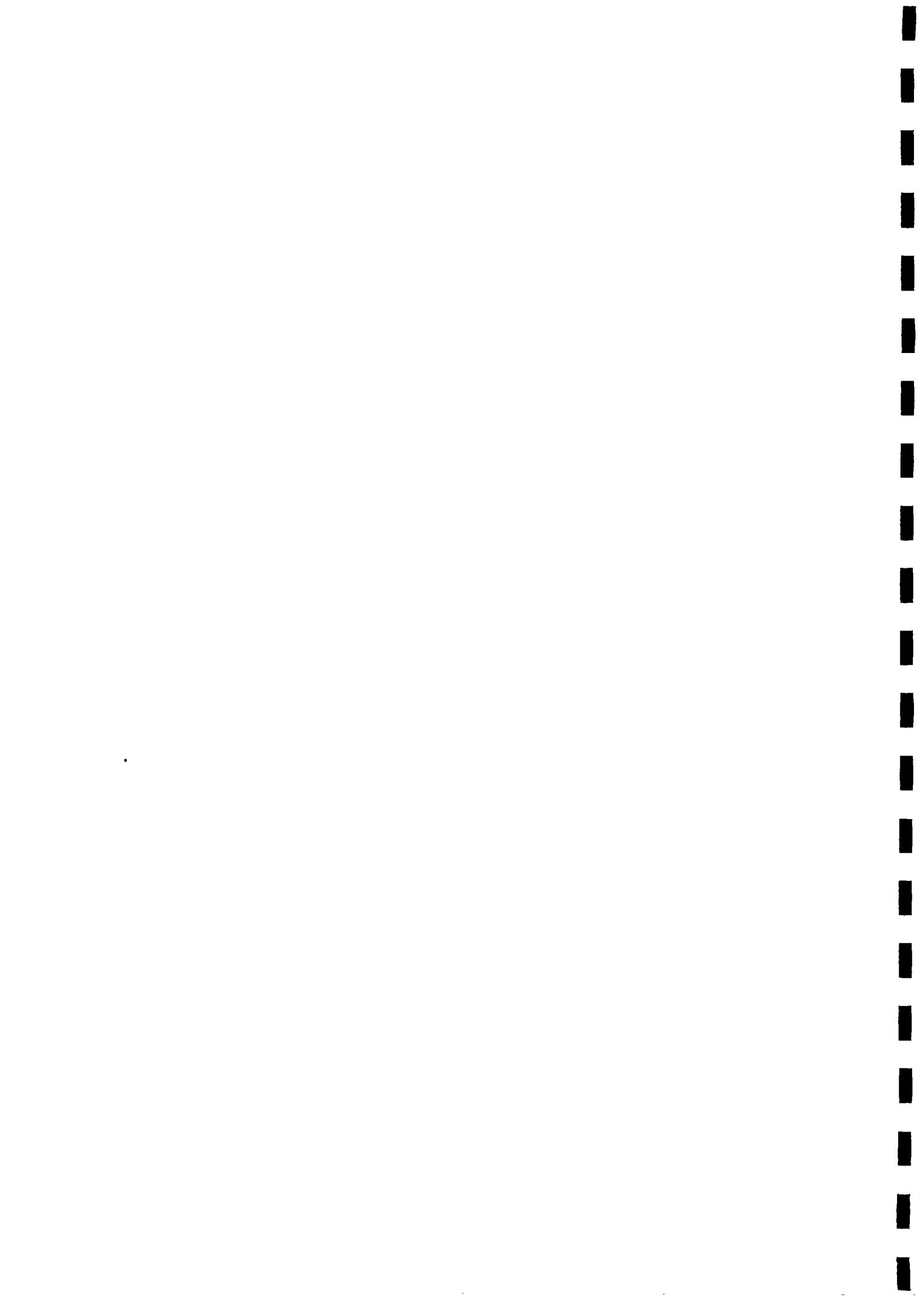
YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	180.6	331.9	15.4	237.1	56.6	23.8	139.9	32.2	42.1	204.7	277.3	45.9	1580.0
1961	176.5	133.8	140.9	184.9	67.3	5.8	21.3	17.2	107.9	186.1	193.5	160.0	1435.7
1962	135.1	35.3	82.6	67.6	163.5	6.1	5.3	77.2	29.2	139.7	96.5	146.5	1006.6
1963	172.9	97.5	115.8	131.3	69.6	66.5	53.3	57.4	62.2	131.5	151.6	139.4	1289.0
1964	98.0	160.0	126.7	35.9	70.1	41.9	137.4	19.6	40.1	99.3	100.5	134.3	1083.4
1965	52.0	139.9	48.5	326.1	147.5	6.8	26.6	113.5	40.2	145.7	200.9	202.6	1488.3
1966	106.1	20.8	120.1	232.6	61.4	34.7	22.6	165.3	166.6	188.4	137.6	119.0	1369.2
1967	131.0	140.4	93.7	156.2	46.7	67.3	36.0	28.4	57.1	260.0	341.1	140.9	1498.6
1968	64.0	1.5	80.2	76.4	30.7	45.3	45.2	93.9	214.6	152.9	202.6	1001.6	1001.6
1969	163.0	23.8	101.0	211.0	116.8	5.5	31.1	133.0	100.8	192.5	71.6	374.6	1525.0
1970	107.6	216.6	115.5	145.7	51.0	12.9	8.3	63.2	78.4	110.7	256.5	329.4	1495.6
1971	136.3	85.5	49.5	166.8	29.2	7.6	41.4	126.6	139.1	141.4	116.3	320.0	1359.3
1972	63.3	0.0	66.5	263.1	92.9	30.7	50.0	122.4	101.6	105.3	232.9	205.9	1543.9
1973	14.9	24.3	56.3	108.2	61.2	21.3	48.0	30.4	78.9	161.6	150.3	317.7	1093.1
1974	0.0	61.7	46.7	172.6	167.6	23.8	70.1	55.6	110.7	33.0	105.9	307.6	1116.9
1975	128.2	34.0	166.6	179.5	92.2	42.6	98.5	63.0	166.6	61.6	109.2	239.5	1581.7
1976	159.7	10.6	41.9	198.3	24.3	86.1	41.9	60.7	78.4	60.1	201.9	140.9	1101.6
1977	2.5	32.7	96.7	186.6	109.2	0.0	59.9	68.1	106.1	256.5	206.5	132.0	1279.6
1978	57.6	13.2	88.3	23.8	152.1	0.0	22.6	18.7	49.5	282.9	194.5	182.3	1085.6
1979	56.6	50.0	8.0	122.6	61.4	47.0	26.1	59.1	146.8	346.4	307.3	140.2	1371.7
1980	27.4	0.0	80.5	199.8	172.4	1.2	0.0	11.4	100.8	177.2	161.2	98.6	1031.3
1981	62.7	33.6	76.7	67.9	56.4	17.5	26.7	30.7	70.4	144.3	246.7	106.9	941.6
1982	3.0	0.0	130.8	81.8	127.3	18.0	3.0	19.8	99.6	129.8	243.3	206.1	1062.7
1983	43.2	14.0	23.1	15.7	95.8	37.1	36.3	33.6	176.6	139.0	390.2	981.3	981.3
1984	160.5	210.9	128.3	284.7	98.8	0.0	103.6	74.7	150.9	61.3	184.9	89.4	1565.9
1985	64.3	89.7	123.9	37.2	37.6	116.4	31.2	60.3	60.7	112.8	115.1	161.0	982.6
1986	50.4	77.2	90.2	134.1	134.3	31.0	82.6	27.4	47.0	205.6	94.7	1504.1	1504.1
1987	90.9	17.0	71.4	176.0	111.2	26.7	4.8	85.6	94.0	276.0	138.2	88.1	1179.9
1988	20.6	67.4	87.9	252.5	46.0	20.8	114.6	101.6	90.7	31.7	48.2	142.2	1041.2
1989	123.7	10.4	16.8	32.5	105.9	52.6	129.5	10.9	108.2	146.3	145.0	930.1	930.1
AVERAGE	104.1	71.5	83.6	119.6	92.5	26.7	48.4	58.2	89.3	170.6	170.2	178.6	MM
STAND. DEV.	92.3	78.6	41.3	81.2	42.1	21.5	41.8	41.8	37.7	86.2	70.6	88.2	MM
MAXIMUM	501.4	331.9	186.6	326.1	172.4	86.1	139.9	165.3	166.6	405.3	341.1	374.6	MM
MINIMUM	0.0	0.0	0.0	6.0	15.7	0.0	0.0	10.9	29.2	31.7	45.2	45.9	MM
TOTAL	1588.0	1989	930.1	1	0.03226	60	60	60	60	1328.6	1319.4	1311.7	1365.5
	1435.7	181	911.6	2	0.06452	61	61	61	61	1319.4	1311.7	1311.7	1365.5
	1006.6	1983	961.3	3	0.09677	62	62	62	62	1319.4	1311.7	1311.7	1365.5
	1289.0	1985	962.5	4	0.12903	63	63	63	63	1319.4	1311.7	1311.7	1365.5
	1083.4	1968	1001.8	5	0.16123	64	64	64	64	1319.4	1311.7	1311.7	1365.5
	1488.3	1962	1006.6	6	0.19355	65	65	65	65	1319.4	1311.7	1311.7	1365.5
	1369.2	1980	1031.3	7	0.22581	66	66	66	66	1319.4	1311.7	1311.7	1365.5
	1498.8	1988	1041.2	8	0.25806	67	67	67	67	1319.4	1311.7	1311.7	1365.5
	1001.6	1982	1062.7	9	0.29032	68	68	68	68	1319.4	1311.7	1311.7	1365.5
	1525.0	1964	1083.4	10	0.32258	69	69	69	69	1319.4	1311.7	1311.7	1365.5
	1495.8	1978	1085.5	11	0.35484	70	70	70	70	1319.4	1311.7	1311.7	1365.5
	1359.3	1973	1093.1	12	0.38710	71	71	71	71	1319.4	1311.7	1311.7	1365.5
	1543.9	1974	101.6	13	0.41935	72	72	72	72	1319.4	1311.7	1311.7	1365.5
	1093.1	1971	116.9	14	0.45161	73	73	73	73	1319.4	1311.7	1311.7	1365.5
	1116.9	1982	1179.9	15	0.49387	74	74	74	74	1319.4	1311.7	1311.7	1365.5
	1361.7	1977	1279.8	16	0.51613	75	75	75	75	1319.4	1311.7	1311.7	1365.5
	1101.6	1963	1289.0	17	0.54639	76	76	76	76	1319.4	1311.7	1311.7	1365.5
	1052.7	1971	1359.3	18	0.58065	77	77	77	77	1319.4	1311.7	1311.7	1365.5
	1085.5	1966	1369.2	19	0.61290	78	78	78	78	1319.4	1311.7	1311.7	1365.5
	1565.9	1967	1498.8	20	0.64516	79	79	79	79	1319.4	1311.7	1311.7	1365.5
	952.5	1986	1504.1	21	0.67742	80	80	80	80	1319.4	1311.7	1311.7	1365.5
	1179.9	1972	1525.0	22	0.70968	81	81	81	81	1319.4	1311.7	1311.7	1365.5
	1041.2	1984	1543.9	23	0.74194	82	82	82	82	1319.4	1311.7	1311.7	1365.5
	1984.1	1970	1495.8	24	0.77419	83	83	83	83	1319.4	1311.7	1311.7	1365.5
	1565.9	1971	1371.7	25	0.80645	84	84	84	84	1319.4	1311.7	1311.7	1365.5
	1504.1	1975	1301.7	26	0.83871	85	85	85	85	1319.4	1311.7	1311.7	1365.5
	1179.9	1969	1525.0	27	0.87097	86	86	86	86	1319.4	1311.7	1311.7	1365.5
	1041.2	1972	1543.9	28	0.90323	87	87	87	87	1319.4	1311.7	1311.7	1365.5
	1984.1	1974	1565.9	29	0.93518	88	88	88	88	1319.4	1311.7	1311.7	1365.5
	1980.1	1970	1588.0	30	0.96774	89	89	89	89	1319.4	1311.7	1311.7	1365.5

10-Year Moving Average



RAINFALL ANALYSIS

YEAR	STATION NAME: KIRKLEES											TOTAL
	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	
1950	465.5	619.2	35.8	297.6	124.9	9.1	158.7	35.8	73.6	290.5	325.5	212.8
1951	343.4	349.5	161.5	261.3	217.1	59.1	46.4	61.2	93.9	170.6	414.5	387.6
1952	312.1	136.3	116.0	197.1	96.7	49.6	14.0	10.1	250.1	208.2	421.3	2031.5
1953	559.5	277.3	110.9	251.2	230.1	26.4	100.3	64.5	213.6	264.6	376.6	662.6
1954	399.2	309.3	149.0	142.4	38.6	37.0	196.3	33.0	107.4	176.5	206.7	337.0
1955	212.3	262.9	115.6	358.6	355.0	20.0	19.9	200.4	157.4	239.6	452.1	369.5
1956	370.0	163.3	253.2	198.6	47.2	27.1	39.3	198.3	165.8	320.8	293.1	368.5
1957	440.4	334.0	226.5	261.6	49.7	124.9	40.8	67.8	80.7	309.9	555.6	373.1
1958	392.6	17.0	199.3	183.6	54.1	25.6	11.9	7.3	124.9	233.4	334.0	369.0
1959	412.2	127.7	28.4	394.2	113.2	9.8	18.5	17.0	129.2	277.8	418.3	743.9
1960	405.3	326.3	206.7	261.1	140.9	13.7	35.0	89.1	59.6	114.0	532.3	733.6
1961	571.5	226.6	89.6	237.6	19.0	34.9	284.2	175.3	212.5	142.9	702.3	289.7
1962	319.7	7.3	97.5	227.8	137.4	141.2	65.5	182.6	633.7	556.2	517.3	2901.3
1963	128.5	131.8	109.4	176.5	102.8	25.4	147.5	40.6	286.6	247.3	311.1	2168.3
1964	9.6	168.4	160.5	259.9	79.2	51.6	64.7	132.8	45.4	167.9	709.4	1952.7
1965	326.8	119.3	224.7	275.6	70.1	16.3	166.2	137.4	145.6	58.9	220.2	686.6
1966	384.3	82.0	44.7	289.0	70.1	21.8	19.5	111.5	73.6	99.0	332.4	2456.5
1967	277.1	66.8	85.3	228.6	155.1	17.2	72.8	93.2	91.4	361.5	431.6	1606.9
1968	299.4	151.9	201.1	314.7	246.8	21.0	38.1	14.7	19.7	160.5	360.1	385.3
1969	186.1	52.8	141.9	117.9	102.8	15.1	83.0	65.8	280.4	535.9	400.6	958.7
1970	148.0	8.8	93.4	173.7	135.1	4.0	176.0	195.6	183.5	206.2	272.6	117.6
1971	106.5	21.8	114.0	16.1	127.0	31.0	259.5	65.3	142.0	243.6	340.5	268.1
1972	12.0	30.8	145.9	139.9	24.3	24.3	46.5	16.2	71.4	340.5	340.5	1737.4
1973	231.1	36.6	4.6	21.5	193.0	10.5	10.5	18.5	314.9	406.1	343.0	450.5
1974	365.3	356.3	243.4	208.4	68.2	5.0	22.3	53.9	62.9	101.5	327.4	2262.7
1975	172.4	156.4	166.9	109.7	128.8	21.4	44.5	130.4	197.2	221.4	246.7	1614.6
1976	1193.4	192.0	161.4	357.6	163.7	4.0	76.5	89.9	315.6	228.6	372.6	1862.2
1977	369.4	93.7	108.9	207.6	190.1	10.5	5.8	120.6	86.7	182.6	338.7	3212.0
1978	144.0	61.9	276.5	344.3	159.7	49.4	53.5	177.4	105.2	114.7	439.8	2167.2
1979	339.8	12.1	50.2	63.9	133.0	47.3	237.2	91.6	178.8	280.7	337.9	2084.8
AVERAGE	322.6	158.1	211.5	124.6	31.4	75.0	96.8	112.3	266.8	338.3	453.9	2328.6
STAND. DEV.	218.9	140.7	71.1	95.5	73.9	32.2	69.6	67.7	55.5	136.4	123.1	182.3
MINIMUM	1193.4	19.2	276.6	394.1	352.0	141.0	259.5	284.2	280.4	633.7	656.8	782.6
MAXIMUM	9.8	4.6	10.6	16.1	10.6	4.0	5.6	7.3	10.1	45.4	80.0	117.6
1980	2077.5	9	0.29032	67	76	68	76	79	82	2429.0	2449.3	2419.3
1981	2084.0	10	0.32250	69	77	69	77	70	79	2360.5	2001.0	2001.0
1982	2100.5	11	0.35184	71	79	71	80	71	80	2391.5	2016.6	2016.6
1983	2132.1	12	0.38710	72	80	72	80	72	80	2373.6	2243.5	2243.5
1984	2165.7	13	0.41935	73	81	72	81	72	81	2512.7	2132.9	2132.9
1985	2169.9	14	0.45161	74	82	73	82	73	82	2429.0	2449.3	2419.3
1986	2260.5	15	0.49387	75	83	74	83	75	84	2360.5	2001.0	2001.0
1987	2262.7	16	0.51613	76	84	75	85	76	85	2391.5	2016.6	2016.6
1988	2313.1	17	0.54839	77	85	76	85	77	85	2373.6	2243.5	2243.5
1989	2313.2	18	0.58065	78	86	77	86	78	86	2538.9	2119.9	2119.9
1990	2419.3	19	0.61290	79	87	78	87	79	87	2429.0	2112.5	2112.5
1991	2456.5	20	0.641516	80	88	79	88	80	89	2360.5	2131.2	2131.2
1992	2490.7	21	0.67742	81	89	80	89	81	89	2391.5	2108.4	2108.4
1993	2565.1	22	0.70968	82	90	81	90	82	90	2373.6	2243.5	2243.5
1994	2649.1	23	0.74194	83	91	82	91	83	91	2538.9	2119.9	2119.9
1995	2718.5	24	0.77419	84	92	83	92	84	92	2429.0	2112.5	2112.5
1996	2849.7	25	0.80645	85	93	84	93	85	93	2360.5	2131.2	2131.2
1997	2901.3	26	0.83871	86	94	85	94	86	94	2391.5	2108.4	2108.4
1998	2917.8	27	0.87097	87	95	86	95	87	95	2373.6	2243.5	2243.5
1999	2945.3	28	0.90323	88	96	87	96	88	96	2538.9	2119.9	2119.9
2000	3137.6	29	0.93549	89	97	88	97	89	97	2429.0	2112.5	2112.5
2001	3212.0	30	0.96774	90	98	89	98	90	98	2360.5	2131.2	2131.2



RAINFALL ANALYSIS

STATION NAME: HORROROWEA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	Total
1960	568.9	843.0	22.6	259.3	143.7	0.0	151.3	25.4	13.7	247.3	362.4	173.4	2811.0
1961	511.3	195.0	144.2	343.1	51.6	6.3	14.2	5.3	52.5	197.8	603.7	560.8	2688.8
1962	384.8	174.2	177.8	244.3	171.1	4.3	10.9	339.0	46.4	163.3	275.3	339.0	2339.7
1963	455.4	319.7	13.5	158.7	61.2	0.0	42.2	164.1	238.5	194.7	641.3	2712.0	
1964	509.2	419.3	159.0	70.3	79.2	3.8	112.7	104.3	37.3	110.2	185.1	411.4	2201.8
1965	208.5	813.9	103.3	231.3	65.0	10.1	1.5	229.9	50.0	305.8	454.9	412.2	2835.3
1966	356.1	96.5	265.2	81.0	44.1	12.1	3.3	64.0	111.5	323.5	356.8	307.5	2035.6
1967	275.5	299.2	130.0	54.6	11.1	49.7	2.7	4.0	54.6	251.4	749.0	378.9	2268.7
1968	287.5	18.0	290.3	66.1	6.6	10.9	62.0	26.6	222.2	200.1	542.6	1862.2	
1969	262.7	189.2	395.8	253.2	13.9	13.2	4.5	162.1	120.6	365.5	119.3	704.5	2294.5
1970	354.5	532.1	105.1	143.0	65.0	4.3	2.5	21.0	64.2	40.1	286.2	290.8	1939.8
1971	357.6	231.5	115.6	152.6	71.4	13.2	46.3	62.0	63.3	207.7	339.6	401.2	2061.8
1972	263.1	231.5	72.6	152.6	71.4	16.5	38.1	62.0	63.3	207.7	121.7	507.4	2113.8
1973	134.1	448.6	76.1	58.9	38.6	58.4	59.9	10.6	95.2	189.3	530.3	621.5	
1974	189.4	37.8	176.8	109.4	6.0	38.6	26.9	46.2	52.3	85.8	522.2	1241.4	
1975	225.0	161.0	135.1	104.6	130.0	11.9	147.8	49.5	116.0	67.0	194.8	516.9	1839.3
1976	326.9	53.3	57.6	117.0	39.8	54.6	56.3	75.4	30.4	76.4	310.3	224.5	1420.4
1977	60.4	68.2	161.6	67.3	81.0	4.0	107.9	29.7	172.9	255.7	280.6	290.5	1609.9
1978	130.3	79.7	72.3	101.8	43.6	0.0	22.0	5.0	13.9	237.2	189.2	565.1	1463.1
1979	162.8	82.2	116.1	65.5	9.3	18.5	22.3	0.0	70.3	306.6	384.0	319.2	1561.8
1980	533.9	63.3	285.2	44.1	0.0	13.9	1.3	253.4	336.5	69.6	1336.0		
1981	135.1	231.5	107.2	0.0	19.0	2.6	17.0	171.2	339.6	317.0	1862.2		
1982	22.6	0.0	95.0	214.6	101.6	10.8	48.5	28.4	49.7	288.3	302.6	489.8	1832.1

YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE
1980	1133.6	1	0.0167	60 - 69
1974	1244.1	2	0.08333	61 - 70
1976	1424.4	3	0.12500	62 - 71
1978	1480.1	4	0.16667	63 - 72
1979	1560.6	5	0.20833	64 - 73
1980	1563.2	6	0.25000	65 - 74
1977	1600.8	7	0.29167	66 - 75
1981	1645.2	8	0.33333	67 - 76
1982	1652.1	9	0.37500	68 - 77
1975	1659.3	10	0.41667	69 - 78
1970	1930.8	11	0.45833	70 - 79
1968	2063.6	12	0.50000	71 - 80
1971	2061.8	13	0.54167	72 - 81
1972	2113.8	14	0.58333	73 - 82
1964	2201.8	15	0.62500	
1987	2260.7	16	0.66667	
1969	2294.5	17	0.70833	
1973	2324.8	18	0.75000	
1962	2333.7	19	0.79167	
1965	2356.3	20	0.83333	
1961	2686.8	21	0.87600	
1960	2712.0	22	0.91667	
1960	2811.0	23	0.95833	

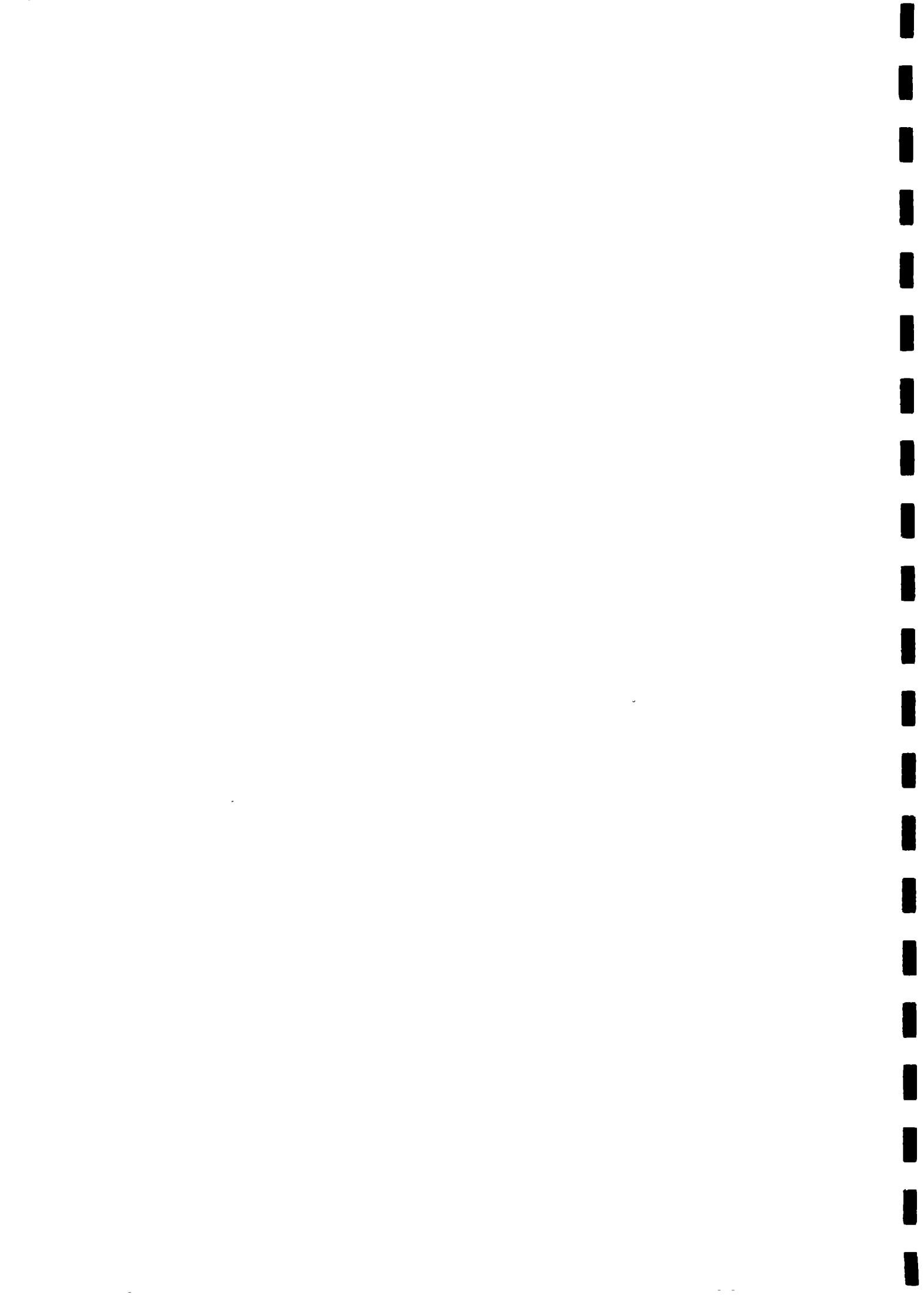


RAINFALL ANALYSIS

WEST - HAPURALE

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1961	251.5	162.6	246.1	299.5	278.9	33.0	52.1	56.0	46.8	105.1	328.2	159.1	2319.8
1962	91.9	70.2	260.9	445.4	215.1	52.4	44.9	97.4	62.2	335.3	332.6	287.0	2323.2
1963	256.2	174.6	351.1	632.2	354.5	90.1	37.9	22.0	230.8	491.6	539.5	261.1	3460.9
1964	118.5	146.5	344.3	468.4	655.3	26.2	97.2	107.7	101.7	70.5	67.2	1710.2	3462.9
1965	194.4	104.6	323.9	715.6	352.9	0.0	1.2	85.7	76.0	325.6	360.0	295.6	2662.9
1966	133.6	41.2	266.2	462.2	22.1	28.4	1.2	63.4	206.0	311.5	811.0	256.6	325.4
1967	151.4	116.0	177.7	205.5	39.9	45.5	11.8	105.5	47.9	397.7	377.9	172.4	1643.1
1968	168.2	24.1	186.1	365.4	108.9	77.7	54.6	22.6	40.9	501.6	167.4	194.5	1932.0
1969	126.1	262.2	171.9	372.5	187.4	30.1	12.7	169.6	71.5	56.5.9	195.3	464.1	2629.3
1970	135.1	274.6	400.9	538.7	148.6	47.0	26.1	57.0	75.7	203.4	436.4	265.9	2610.5
1971	230.4	276.3	408.5	198.3	39.3	77.5	17.1	282.9	215.4	135.8	314.6	2316.0	
1972	58.6	257.0	382.6	199.1	36.9	141.9	20.2	155.7	595.7	588.7	176.3	2611.8	
1973	13.9	65.5	154.1	312.9	74.3	31.8	15.7	26.1	61.8	296.8	230.9	295.1	1576.9
1974	0.0	103.0	81.6	244.1	182.3	50.3	76.3	36.0	316.1	192.2	419.7	324.4	2328.8
1975	198.0	2.7	151.2	224.9	288.9	12.2	10.6	197.5	301.2	335.9	240.3	1878.9	
1981	137.9	15.2	224.9	147.7	149.0	51.9	118.8	52.8	129.5	215.2	428.3	165.4	1756.6
1982	34.1	18.0	229.1	182.9	478.3	136.8	31.3	101.2	65.8	320.0	519.2	152.5	2272.2
1983	10.4	39.1	160.7	139.3	216.8	17.4	70.7	104.2	65.3	270.1	310.2	152.5	1976.7
1986	10.4	36.4	153.7	549.3	347.5	29.1	54.1	73.0	478.0	134.5	159.4	2102.6	
1987	170.4	54.0	262.6	333.1	273.8	8.0	9.0	102.9	73.0	478.0	134.5	159.4	2102.6
1988	30.5	240.0	270.0	558.0	124.5	31.0	69.0	110.5	164.5	274.0	274.0	273.7	
1989	102.5	51.0	81.0	250.5	272.0	55.0	212.0	103.5	176.0	264.0	450.0	149.0	
AVERAGE	102.4	104.2	225.5	377.4	196.8	42.2	54.7	74.4	133.6	358.9	334.6	224.0	2226.7
STD. DEV.	60.2	68.9	84.9	153.7	118.3	23.1	50.9	39.6	82.5	162.9	141.2	92.5	448.7
HIGH MUM	255.2	276.3	400.9	715.6	478.3	136.8	212.0	169.6	316.1	735.0	588.7	464.1	3460.9
MINIMUM	0.0	0.0	80.7	139.3	18.3	0.0	1.2	20.2	40.9	29.5	70.5	67.2	1476.7

YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE
YEAR	YEAR	AVG		
1963	1471.7	1	0.01348	61 - 70
1973	1571.9	2	0.08695	62 - 71
1984	1718.2	3	0.13043	63 - 72
1981	1753.6	4	0.17391	64 - 73
1967	1649.1	5	0.21739	65 - 74
1980	1878.9	6	0.26087	66 - 80
1983	1889.0	7	0.30435	67 - 81
1963	1932.0	8	0.34783	68 - 82
1985	2107.6	9	0.39330	69 - 83
1988	2228.5	10	0.43478	70 - 86
1982	2272.2	11	0.47826	71 - 87
1971	2318.0	12	0.52174	72 - 88
1961	2318.8	13	0.56522	73 - 89
1962	2322.2	14	0.60870	2023.8
1966	2325.4	15	0.65217	
1974	2328.9	16	0.69565	
1970	2410.5	17	0.73913	
1972	2611.9	18	0.79261	
1963	2628.3	19	0.82603	
1965	2662.9	20	0.86957	
1987	2733.7	21	0.91304	
1983	3460.9	22	0.95652	



RENNALL ANALYSIS

STATION : DIVARALABA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AGR	SEP	OCT	NOV	DEC	TOTR	L	
1960	211.4	265.7	26.4	227.3	162.4	69.1	150.3	13.0	35.7	210.8	344.4	44.8	1754.	3	
1961	135.9	167.5	155.9	167.3	203.8	11.9	26.8	19.1	111.5	253.3	191.5	190.4	1635.	3	
1962	117.8	176.7	164.9	173.2	157.2	72.7	59.3	103.2	107.1	291.5	169.7	167.0	1658.	4	
1963	161.2	115.0	63.4	159.7	80.6	31.3	55.6	28.0	161.6	303.8	277.2	258.5	1741.	4	
1964	144.1	131.3	116.4	118.6	82.2	23.0	154.8	54.4	112.1	228.9	176.6	104.7	1453.	0	
1965	46.8	99.8	50.0	270.8	106.4	3.9	50.2	170.2	59.0	292.8	279.6	207.0	1635.	5	
1966	100.4	122.6	149.3	163.8	23.9	3.1	199.2	211.3	240.2	177.1	157.8	1462.	1622.	2	
1967	128.2	142.7	52.0	128.9	96.6	31.3	56.4	48.6	250.5	269.1	113.8	1369.	555.	3	
1968	54.6	14.3	118.5	57.6	89.1	101.2	15.5	80.1	35.0	283.9	248.2	167.0	1265.	0	
1969	174.4	54.1	74.0	219.4	80.2	3.8	183.3	71.9	292.8	160.7	395.3	1731.	666.	3	
1970	116.0	279.7	174.0	342.7	142.9	23.3	14.1	19.7	81.7	165.6	322.9	2154.	555.	2	
1971	148.4	149.0	136.6	201.9	29.3	21.5	28.1	184.4	203.9	306.5	172.7	270.2	1854.	555.	2
1972	58.4	33.0	69.9	124.1	175.0	53.4	62.0	8.7	117.1	363.4	269.3	106.8	1543.	1	
1973	16.1	15.5	127.6	95.3	65.8	50.1	36.6	56.4	98.8	320.5	173.0	297.6	1364.	1	
1974	6.1	155.2	69.8	201.1	153.9	48.1	91.1	37.4	134.5	86.6	166.6	235.7	1423.	1	
1975	142.5	35.5	191.6	214.2	154.1	31.6	98.8	116.5	248.0	90.0	211.5	243.4	1780.	7	
1976	203.5	25.0	62.3	198.2	9.0	162.2	10.5	64.3	40.3	130.4	301.6	219.1	1425.	4	
1977	19.7	81.5	82.7	141.9	150.7	39.0	98.3	69.6	230.4	520.0	272.2	155.2	1843.	1	
1978	74.9	123.2	141.6	118.1	152.6	2.3	63.0	4.9	74.4	258.4	241.7	207.6	1462.	1	
1979	27.6	115.6	24.1	172.9	70.2	91.2	21.8	12.4	258.4	404.6	388.2	86.5	1673.	5	
1980	23.2	56.0	254.9	62.9	1.3	20.0	22.0	122.2	303.8	305.6	129.4	1285.	6		
1981	43.9	60.0	73.5	156.1	95.3	2.3	243.9	124.4	124.4	181.9	200.1	101.2	1362.	0	
1982	3.5	2.7	202.8	121.8	214.3	42.4	29.6	55.1	104.6	270.3	226.3	161.2	1431.	6	
1983	18.3	37.1	14.9	63.7	176.0	14.7	37.9	59.3	18.4	290.3	237.2	271.1	1239.	1	
1984	227.7	296.7	219.4	239.1	112.5	21.7	116.7	172.7	165.7	114.6	216.6	131.3	1977.	1	
1985	67.4	76.5	55.4	85.7	35.7	162.2	243.9	64.9	199.2	258.4	520.6	466.9	395.3	2151.	
AVERAGE	95.4	97.2	108.7	162.5	113.8	39.6	53.4	74.1	116.5	259.5	240.4	194.7	1570.	7	
STD. DEV.	227.7	279.7	219.4	342.7	214.3	14.9	9.0	0.1	4.9	18.4	86.6	146.4	254.0	1365.	
MAXIMUM	2.4	0.0	14.9	73.2	72.4	36.0	112.5	151.9	95.2	126.1	146.4	254.0	1365.	1	
MINIMUM	2.4	0.0	14.9	73.2	72.4	36.0	112.5	151.9	95.2	126.1	146.4	254.0	1365.	1	

10 YEAR MOVING AVERAGE

YEAR	TOTAL	RANK	PROBABILITY
1983	1239.9	1	0.03571
1968	1265.0	2	0.07143
1980	1263.6	3	0.10714
1981	1362.0	4	0.14286
1973	1364.5	5	0.17657
1985	1365.4	6	0.21429
1967	1368.5	7	0.25000
1976	1426.4	8	0.28571
1974	1428.1	9	0.32143
1982	1434.6	10	0.35714
1964	1453.0	11	0.39286
1966	1462.2	12	0.42857
1978	1462.4	13	0.46429
1978	1510.6	14	0.50000
1972	1543.1	15	0.53571
1961	1635.9	16	0.57143
1965	1636.5	17	0.60714
1977	1643.9	21	0.65714
1962	1655.4	18	0.69286
1979	1673.5	19	0.69286
1969	1731.6	20	0.71429
1963	1741.1	21	0.75000
1960	1754.3	22	0.78571
1975	1760.7	23	0.82143
1977	1843.9	24	0.85714
1971	1854.5	25	0.89286
1984	1877.0	26	0.92657
1970	2154.5	27	0.96429



MATERIAL ANALYSIS

STATION : CANAVARELLA GROUP

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1971	164.4	200.8	83.4	169.4	70.4	8.7	129.0	263.4	261.2	214.1	243.4	487.2	2714.2
1972	85.1	29.8	67.1	257.9	14.9	131.9	131.9	333.8	195.9	720.4	306.6	325.2	2418.0
1973	53.4	66.6	189.5	296.2	15.6	47.3	133.9	149.7	156.8	385.9	259.1	520.2	2323.2
1974	10.7	262.9	40.2	351.3	149.7	66.9	105.0	27.7	31.5	213.2	196.9	378.0	2134.0
1975	173.0	85.4	253.7	391.7	36.6	21.4	201.0	327.7	204.8	159.6	311.2	309.8	2539.9
1976	310.9	28.0	234.0	544.9	77.8	134.9	65.6	89.7	160.1	510.4	332.3	2679.3	2715.5
1977	7.2	70.4	98.9	353.4	315.3	99.6	177.1	110.3	340.7	504.0	517.4	186.2	2760.5
1978	30.0	96.3	265.2	227.1	217.3	25.4	131.1	28.8	103.2	416.4	341.7	474.5	2349.0
1979	53.9	58.5	47.0	384.1	30.7	79.0	53.1	62.0	335.3	656.1	887.3	270.3	2977.9
1980	40.4	0.0	69.1	634.5	67.4	19.6	81.6	311.5	260.9	571.0	136.0	2542.1	2539.6
1981	70.1	111.8	131.3	478.8	176.8	60.2	24.8	109.0	238.0	402.8	522.5	306.8	2651.6
1982	0.0	0.0	216.7	238.0	306.8	47.8	13.5	8.8	114.4	645.4	378.9	212.5	2085.8
1983	36.7	50.6	1.0	51.0	149.6	16.1	23.2	107.6	182.5	299.0	253.1	377.3	1568.6
1984	287.5	331.3	300.0	273.6	220.6	11.4	23.8	48.5	256.9	210.7	335.2	102.4	2591.9
1985	131.2	141.9	221.8	256.8	39.5	29.2	64.0	99.0	170.6	330.9	192.4	252.6	1973.6
AVERAGE	97.0	108.3	148.6	347.4	174.6	55.3	18.3	106.3	214.8	367.2	388.5	311.2	2432.2
STAND-DEV.	94.7	101.0	94.0	140.3	104.1	39.3	61.2	69.4	78.0	169.3	179.0	119.7	361.2
MAXIMUM	310.9	331.3	300.0	634.5	87.4	134.9	24.8	327.7	340.7	720.4	887.3	520.2	2977.9
MINIMUM	0.0	0.0	1.0	51.0	15.6	6.7	13.5	8.8	89.7	159.6	192.4	102.4	1668.6

YEAR	TOTAL	RANK	PROBABILITY	10 Year Moving Avg
				Year
1983	1583.5	1	0.05450	71 - 81
1985	1793.8	2	0.12400	72 - 82
1982	2105.8	3	0.10150	73 - 83
1974	2114.0	4	0.25100	74 - 84
1973	2125.2	5	0.31150	75 - 85
1978	2143.0	6	0.37400	
1972	2149.0	7	0.43750	
1975	2639.9	8	0.50600	
1980	2142.1	9	0.56150	
1984	2690.9	10	0.62500	
1976	2674.3	11	0.68750	
1971	2114.2	12	0.75600	
1977	2180.5	13	0.81250	
1981	2151.6	14	0.86900	
1978	2177.0	15	0.93750	

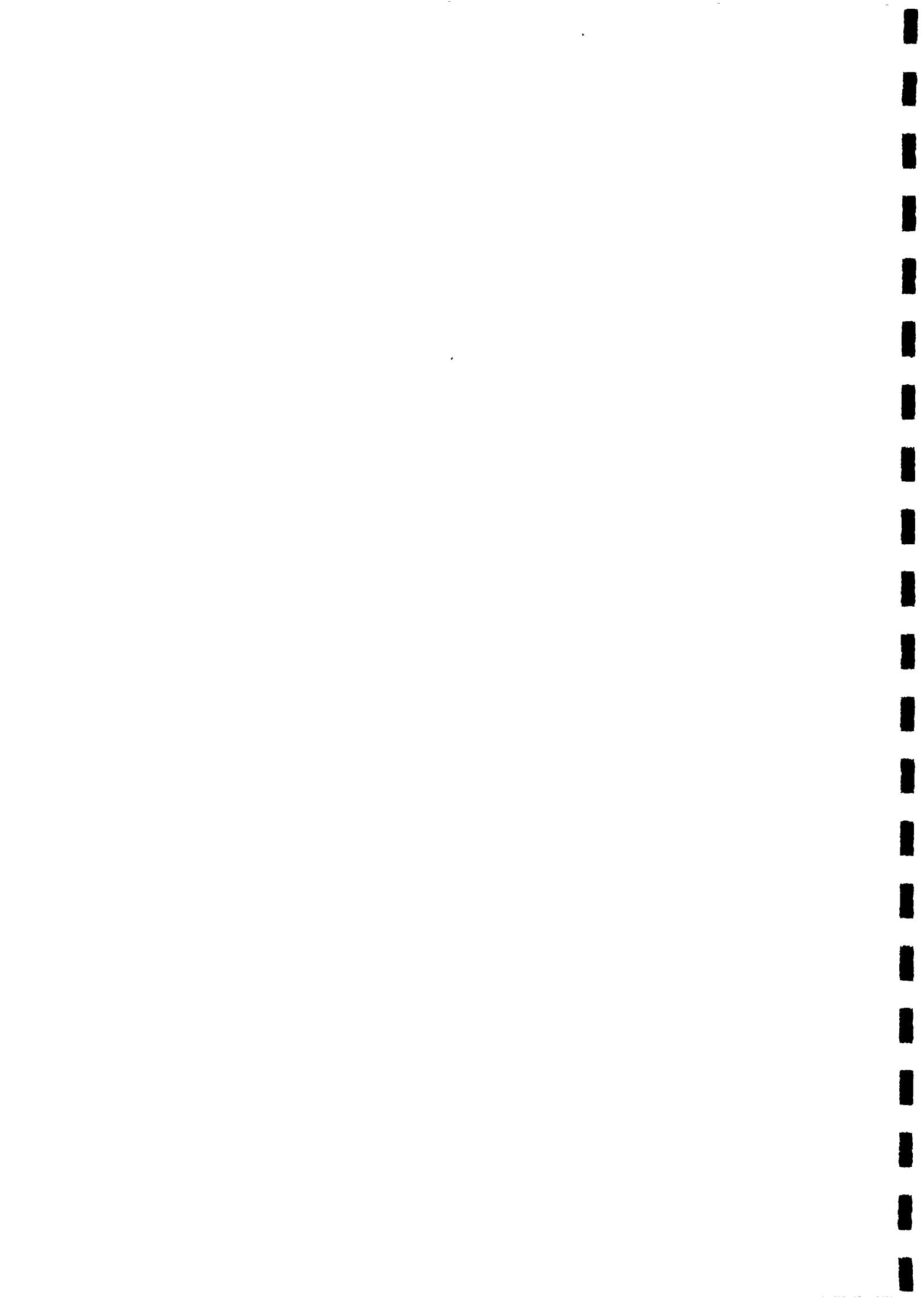


RAINFALL ANALYSIS

STATION : SIBILLE DISPENSARY

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1972	130.2	73.4	92.8	101.9	12.5	29.3	29.0	8.2	97.8	294.2	261.9	428.3	1566.3
1973	42.0	50.3	142.3	14.3	32.1	36.1	77.5	27.2	58.5	183.9	344.5	560.1	1506.8
1974	0.0	91.2	70.7	223.8	187.5	10.2	66.1	9.2	83.6	56.9	178.1	427.3	1404.6
1975	117.6	105.4	147.8	126.2	60.3	0.0	132.0	141.2	129.9	98.5	168.1	354.6	1822.4
1976	311.1	32.6	66.9	207.6	0.0	24.4	37.6	138.2	88.2	85.4	234.2	322.6	1886.8
1977	167.7	95.3	106.2	70.2	80.7	0.0	52.1	22.4	90.2	361.2	228.6	167.2	1823.8
1978	73.7	62.9	63.0	130.1	0.0	34.3	0.0	22.7	237.0	225.1	404.2	1369.9	
1979	16.6	30.5	58.5	0.0	1.6	68.9	31.6	140.5	351.3	400.1	230.9	1410.9	
1980	80.6	0.0	6.4	147.1	113.3	0.0	62.6	37.4	191.5	217.2	1077.6		
1985	211.9	191.5	153.1	64.7	0.0	39.6	53.9	100.8	57.7	140.6	128.5	406.6	1519.1
AVERAGE	130.2	73.4	92.8	101.9	61.7	14.3	55.3	56.2	80.6	200.1	240.1	301.9	1474.4
STAND.DEV.	17.8	51.8	43.8	71.2	62.3	15.3	33.6	51.9	35.6	103.4	76.8	99.3	255.1
MAXIMUM	311.1	191.5	153.1	223.8	187.5	39.6	132.0	141.2	140.5	361.2	400.1	560.1	1823.8
MINIMUM	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	22.7	66.9	128.5	1077.6

YEAR	TOTAL	RFNk	PROBABILITY
1980	1077.6	1	0.09691
1976	1381.9	2	0.10862
1974	1404.6	3	0.27373
1979	1410.7	4	0.36864
1972	1514.3	5	0.45855
1985	1541.1	6	0.54445
1973	1571.0	7	0.63396
1975	1583.4	8	0.72127
1976	1584.8	9	0.81618
1977	1621.8	10	0.90809



RAINFALL ANALYSIS

INTRODUCTION

YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE	
YEAR	TOTAL	RANK	PROBABILITY	Year	Avg.
1960	261.4	241.9	53.9	234.2	104.4
1961	161.6	154.5	169.2	210.4	241.3
1962	145.6	168.9	117.6	96.1	204.0
1963	234.5	107.2	59.2	126.0	51.1
1964	8.7	35.4	0.09677	78.3	36.9
1965	39.9	113.6	47.8	290.1	51.1
1966	114.1	6.7	85.9	137.9	77.3
1967	148.6	156.0	52.6	159.6	41.4
1968	66.6	10.5	138.2	84.6	24.9
1969	186.2	74.0	41.2	175.1	13.3
1970	114.6	21.7	167.2	265.7	5.6
1971	152.2	61.0	31.8	128.8	42.0
1972	30.0	36.1	39.4	123.9	2.6
1973	29.0	11.0	102.2	110.3	91.0
1974	25.4	123.2	80.1	172.6	60.6
1975	190.5	31.8	212.4	161.3	108.0
1976	198.2	16.6	110.3	332.3	5.1
1977	1.3	61.0	83.9	144.8	95.0
1978	58.2	118.4	102.9	152.4	0.0
1979	31.8	54.7	17.0	106.7	40.7
1980	31.3	0.0	29.5	135.9	95.3
1981	45.2	41.4	60.2	65.9	59.7
1982	0.0	91.4	208.5	164.9	8.9
1983	17.0	31.5	6.6	104.9	14.0
1984	259.0	214.1	210.8	230.4	16.0
1985	117.5	95.0	165.1	68.9	10.5
1986	368.3	141.0	176.5	142.7	46.5
1987	90.6	9.9	39.9	121.7	105.9
1988	24.4	86.7	110.7	106.4	14.7
1989	69.6	11.4	48.5	69.6	60.5
RANGE	108.3	79.8	96.2	157.0	106.6
STD.DEV.	91.6	66.9	64.6	83.3	38.4
MEAN	368.3	241.9	212.4	338.6	122.5
SD.UH	0.0	0.0	0.0	0.0	0.0
YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE	
1964	744.3	1	0.03226	60 - 69	1481.9
1965	1123.9	2	0.06452	61 - 70	1476.8
1966	1216.8	3	0.09677	62 - 71	1465.6
1967	1266.9	4	0.12903	63 - 72	1404.7
1968	1269.0	5	0.16129	64 - 73	1491.9
1969	1277.1	6	0.19355	65 - 74	1555.8
1970	1303.4	7	0.22561	66 - 75	1542.7
1971	1307.1	8	0.25806	67 - 76	1501.8
1972	1383.7	9	0.29032	68 - 77	1590.5
1973	1384.6	10	0.32260	69 - 78	1604.7
1974	1391.7	11	0.35484	70 - 79	1574.8
1975	1396.5	12	0.38710	71 - 80	1510.2
1976	1410.6	13	0.41935	72 - 81	1488.2
1977	1420.4	14	0.45161	73 - 82	1469.6
1978	1461.9	15	0.48387	74 - 83	1426.6
1979	1490.4	16	0.51613	75 - 84	1486.7
1980	1526.6	17	0.54839	76 - 85	1457.7
1981	1553.5	18	0.58065	77 - 86	1459.1
1982	1577.6	19	0.61290	78 - 87	1423.0
1983	1583.2	20	0.64516	79 - 88	1440.5
1984	1611.7	21	0.67742	80 - 89	1425.1
1985	1638.9	22	0.70968		
1986	1668.3	23	0.74194		
1987	1674.6	24	0.77419		
1988	1681.7	25	0.80645		
1989	1719.1	26	0.83871		
1990	1805.8	27	0.87097		
1991	1949.6	28	0.90323		
1992	1984.8	29	0.93543		
1993	2000.6	30	0.96774		



RAINFALL ANALYSIS
STATION : ENDULLA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
	1960	355.7	150.0	18.5	256.4	192.3	8.9	75.7	16.2	34.5	384.8	256.9	61.7
1961	216.2	188.0	235.0	190.7	103.6	29.5	41.7	64.2	95.8	199.7	332.4	303.8	2008.6
1962	201.9	41.8	154.3	149.8	172.8	59.9	14.7	197.6	1.2	156.4	153.0	220.5	1528.9
1963	292.1	151.9	39.7	246.1	129.3	50.2	24.2	94.5	197.6	174.1	334.9	318.3	2048.9
1964	219.4	302.5	98.1	214.7	34.7	36.6	143.1	60.6	18.6	146.6	100.4	186.6	1591.8
1965	86.7	175.6	160.8	106.6	196.1	7.4	57.9	270.9	70.3	283.2	421.3	364.1	2528.9
1966	166.5	54.6	144.5	226.1	65.8	31.7	17.6	125.1	116.0	229.9	364.1	255.2	1798.1
1967	170.5	199.3	96.9	115.8	92.4	178.9	97.8	30.1	60.9	243.1	372.7	163.3	1641.1
1968	106.9	4.7	92.3	91.4	53.5	41.0	13.3	28.1	106.4	236.8	213.9	183.8	1731.1
1969	213.2	77.1	107.5	312.6	77.5	8.9	41.6	170.7	43.1	205.6	70.4	637.0	1663.2
1970	193.2	286.4	118.4	351.8	51.5	3.5	63.2	79.2	64.1	95.5	492.6	336.0	2138.5
1971	212.9	183.7	65.7	336.6	38.9	1.6	37.4	217.0	155.2	158.6	212.2	359.5	1991.2
1972	120.4	2.2	37.7	163.0	100.8	53.1	74.7	204.7	204.4	546.6	255.3	379.1	1958.9
1973	30.7	32.4	104.6	103.2	83.1	22.6	219.7	52.1	181.1	231.0	168.7	1625.0	1641.1
1974	3.1	101.4	164.1	248.7	163.5	60.1	31.6	30.6	172.8	74.8	110.1	161.0	1611.1
1975	170.5	92.4	215.3	22.1	22.5	15.6	137.8	224.7	91.1	231.5	289.8	1794.5	1663.2
1976	242.1	13.8	66.4	264.0	70.5	23.4	67.1	141.2	40.0	123.9	325.3	176.3	1554.0
1977	7.8	57.0	109.6	175.7	110.2	17.3	107.2	99.7	164.7	330.1	198.8	311.4	1609.5
1978	82.3	98.9	144.8	28.0	336.6	2.2	36.7	17.7	66.6	277.4	219.3	267.4	1542.7
1979	67.0	25.9	51.3	210.4	65.5	37.2	70.9	78.6	291.9	306.8	174.1	179.7	1931.3
1980	59.2	0.1	92.9	336.5	104.8	0.3	7.4	28.9	111.7	180.4	243.2	161.3	1321.5
1981	74.0	110.0	70.2	175.2	102.3	11.5	167.9	28.1	148.4	226.8	242.6	166.8	1564.6
1982	7.7	0.0	140.4	202.6	139.1	24.4	20.2	23.9	200.6	344.8	225.0	361.8	1698.7
1983	65.8	39.8	43.5	76.2	153.0	31.3	61.8	57.7	49.6	299.3	227.8	442.4	1482.2
1984	216.9	311.1	212.4	214.5	135.2	8.7	137.9	13.9	136.5	227.1	194.9	116.1	1928.2
1985	171.2	76.4	165.4	75.6	162.2	16.9	120.4	133.6	90.8	233.3	188.9	245.1	1551.1
1986	721.5	136.5	281.0	250.1	120.4	2.0	71.3	98.0	65.8	376.2	131.4	207.8	2462.3
1987	206.5	42.7	85.7	218.7	171.6	3.6	10.2	62.9	176.0	273.8	165.2	88.4	1501.3
1988	48.4	59.0	198.7	249.0	35.6	30.0	51.9	249.6	246.1	136.8	147.1	350.9	1482.2
1989	201.0	14.9	60.7	114.1	61.3	39.0	222.5	76.5	249.6	295.7	267.6	106.4	1718.6
AVERAGE	163.4	111.0	114.7	206.8	105.2	28.9	74.1	90.1	121.3	237.7	253.6	269.0	1773.7
STD. DEV.	136.2	108.6	61.5	406.6	366.6	22.1	176.9	222.5	270.9	102.4	102.7	118.7	298.9
MM. RAIN	721.5	450.0	261.0	406.6	28.0	0.3	7.4	27.4	13.9	1.2	74.8	70.4	61.7
HIGH RAIN	3.1	0.0	18.6	22.1	0.3	0.3	0.3	0.3	0.3	74.8	70.4	61.7	1175.1

YEAR	TOTAL	RANK	PROBABILITY	10-YEAR RAINFALL AVERAGE
1960	1173.1	1	0.03226	60 - 69
1960	1328.5	2	0.06452	61 - 70
1963	1498.2	3	0.09677	62 - 71
1967	1504.3	4	0.12903	63 - 72
1962	1524.9	5	0.16129	64 - 73
1974	1541.4	6	0.19355	65 - 74
1976	1547.7	7	0.22581	66 - 75
1985	1551.1	8	0.25606	67 - 76
1976	1554.0	9	0.29032	68 - 77
1961	1554.6	10	0.32256	69 - 78
1979	1591.6	11	0.35464	70 - 79
1973	1625.0	12	0.38710	71 - 80
1977	1689.5	13	0.41935	72 - 81
1969	1691.7	14	0.45161	73 - 82
1989	1718.8	15	0.48367	74 - 83
1964	1749.5	16	0.51613	75 - 84
1968	1795.0	17	0.54639	76 - 85
1972	1953.8	18	0.58065	77 - 86
1971	1994.2	19	0.61290	78 - 87
1961	2001.6	20	0.64516	79 - 88
1963	2048.9	21	0.67742	80 - 89
1984	1925.2	22	0.70968	81 - 90
1979	1939.3	23	0.74194	82 - 91
1966	1787.1	24	0.77419	83 - 92
1967	1841.1	25	0.80645	84 - 93
1961	2001.6	26	0.83671	85 - 94
1960	2131.6	27	0.87091	86 - 95
1970	2135.6	28	0.90323	87 - 96



KINETIC ANALYSIS

3.

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
AVERAGE	115.7	90.6	210.9	298.2	143.1	23.5	22.0	20.4	41.1	217.1	345.7	197.3	1728.9
STAND. DEV.	90.8	76.3	122.7	140.5	129.0	27.0	31.7	41.7	56.5	115.3	147.5	98.5	468.4
MAXIMUM	357.1	253.7	519.6	642.3	412.4	112.5	154.6	229.6	280.4	437.1	685.5	437.8	2596.1
MINIMUM	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1938	7.6	250.1	110.3	379.2	0.5	2.0	1.7	19.5	86.3	209.5	109.2	357.8	1504.2
1939	5.0	0.0	152.4	355.6	10.6	7.3	7.3	41.4	241.8	434.0	357.8	1710.9	1710.9
1940	0.0	69.1	129.5	233.9	326.3	25.4	1.0	0.0	27.9	425.5	452.9	199.4	2011.2
1941	108.7	3.5	273.5	177.0	369.6	16.7	2.5	0.0	49.7	426.9	305.0	247.9	1643.9
1942	139.7	45.1	310.3	381.2	232.6	93.3	24.8	26.1	46.4	123.9	154.9	1682.8	1926.8
1943	121.6	65.3	426.2	177.2	321.8	24.8	1.5	6.8	5.6	223.0	287.8	242.3	2141.4
1944	146.0	237.9	208.7	341.6	179.3	36.0	0.0	0.0	45.2	437.1	352.8	129.5	1711.5
1945	4.0	68.5	166.8	26.5	18.5	56.3	27.9	6.3	0.0	263.1	685.5	194.3	2011.1
1946	96.2	6.8	150.1	551.1	79.7	0.0	18.7	90.1	210.3	276.5	202.4	1661.2	1661.2
1947	133.3	7.6	519.6	164.3	254.2	51.5	57.1	229.6	13.4	153.6	242.5	174.4	2015.2
1948	260.3	36.3	203.2	103.0	90.9	10.9	6.8	59.1	0.0	315.7	399.0	260.1	1700.3
1949	114.3	103.1	3.5	502.9	6.8	12.4	17.4	5.5	0.0	150.1	402.0	296.1	1643.9
1950	28.4	112.7	98.6	143.0	39.0	11.1	42.6	16.0	142.4	327.1	165.6	1120.6	2126.8
1951	265.2	126.7	159.5	379.4	246.6	37.3	12.9	0.0	280.4	94.7	461.7	71.8	2902.1
1952	160.0	72.1	264.6	642.3	412.4	0.0	18.2	0.0	66.8	69.3	132.0	132.0	1320.6
1953	72.6	101.0	243.3	243.5	4.8	43.4	70.6	24.1	61.2	299.4	303.0	233.4	1700.3
1954	272.0	133.8	130.5	297.1	45.9	6.0	20.5	0.0	279.4	226.3	343.9	1876.9	1876.9
1955	141.4	170.1	269.8	368.6	43.9	8.3	19.3	171.1	71.6	381.4	197.7	1718.0	1718.0
1956	72.1	0.0	282.9	143.5	12.1	98.5	14.7	0.5	8.6	139.7	445.6	132.8	1949.1
1957	29.2	75.1	223.0	367.0	199.3	33.2	18.2	12.7	5.3	356.6	605.7	137.9	2363.6
1958	83.8	33.7	405.1	136.2	132.8	50.0	10.6	9.1	68.5	192.2	444.7	133.3	1635.0
1959	39.3	253.7	71.3	270.5	257.8	112.5	20.5	6.6	25.1	275.5	451.1	162.8	1700.3
1960	267.2	248.9	63.7	269.7	12.7	5.3	154.6	0.0	58.9	293.6	314.7	162.3	1671.6
1961	177.0	130.3	265.6	166.0	29.9	32.0	20.0	14.2	260.9	283.7	108.5	1756.0	1756.0
1962	123.9	94.4	238.6	312.4	166.3	11.1	2.5	52.3	39.9	164.5	161.5	197.3	1663.9
1963	357.1	70.3	143.5	526.5	391.9	24.8	10.1	9.3	23.6	253.7	587.7	197.7	2866.1
1964	57.1	99.5	179.9	250.9	73.6	12.7	73.4	17.2	68.5	174.2	59.9	57.6	1124.1
1965	1.7	0.0	114.0	76.2	0.0	0.0	15.2	13.9	339.1	241.3	239.5	740.9	740.9
1966	104.6	12.7	69.5	157.7	39.3	0.0	0.0	0.0	61.7	299.7	0.0	121.4	121.4
1967	92.9	-47.7	0.0	0.0	75.1	8.1	1.5	0.0	0.0	0.0	0.0	72.6	297.9

YEAR

Year	Fog	Rain
1967	297.9	1
1965	740.9	0.03226
1960	1120.6	0.06452
1964	1124.4	0.09677
1966	1224.4	0.12903
1956	1349.4	0.16129
1930	1504.2	0.19353
1949	1643.9	0.22581
1946	1681.2	0.25806
1942	1682.8	0.29032
1953	1700.3	0.32258
1939	1714.3	0.35484
1945	1714.5	0.38710
1955	1718.7	0.41935
1961	1756.0	0.45161
1958	1835.0	0.48387
1960	1871.8	0.51613
1954	1875.9	0.54039
1962	1883.3	0.58065
1940	1910.9	0.61290
1943	1926.8	0.64516
1959	1945.7	0.67742
1947	2001.1	0.70968
1941	2001.2	0.74194
1948	2015.2	0.77419
1952	2092.4	0.80645
1951	2128.2	0.83871
1944	2363.6	0.87097
1963	2414.1	0.90323
1961	2596.1	0.93548
1963	2677.4	0.96774
38	17	1855.1
39	18	1909.2
40	19	1902.2
41	20	1823.1
42	21	1835.8
43	22	1876.8
44	23	1861.2
45	24	1800.3
46	25	1800.8
47	26	1787.6
48	27	1803.8
49	28	1792.8
50	29	1813.1
51	30	1666.2
52	31	1851.0
53	32	1860.1
54	33	1919.7
55	34	1844.5
56	35	1746.7
57	36	1734.2
58	37	1527.7



RAINFALL ANALYSIS

STATION : RATNAPURA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE									
1960	158.4	321.5	123.4	332.5	325.0	411.4	400.0	146.6	125.9	300.4	191.5	72.9	3209.5
1961	104.2	74.8	170.2	331.2	474.0	257.9	391.1	515.5	470.5	405.3	379.9	160.8	3753.4
1962	138.5	79.8	197.1	191.7	742.5	339.6	166.1	253.7	401.3	425.9	397.6	177.6	3521.2
1963	208.4	147.2	272.3	451.7	394.8	428.5	420.5	423.0	502.2	521.8	110.1	181.6	4162.1
1964	84.9	178.9	286.2	441.5	690.3	276.6	611.2	229.5	413.2	432.9	262.5	155.9	4145.9
1965	72.4	93.0	183.4	366.2	662.6	243.0	101.9	548.3	413.8	434.2	321.5	340.2	3801.1
1966	80.4	70.9	221.9	273.6	159.8	230.6	151.9	302.5	759.3	469.4	296.1	153.1	3169.5
1967	104.5	56.0	247.6	247.9	296.9	458.0	399.9	261.6	280.0	556.7	553.7	355.5	3924.7
1968	190.6	137.4	167.0	157.4	424.1	849.0	419.1	168.9	245.6	374.0	234.1	355.5	3918.9
1969	58.0	168.2	128.5	269.3	984.1	350.5	91.9	298.3	286.0	158.6	192.1	236.8	3530.7
1970	101.2	147.2	284.9	344.3	263.2	373.0	369.0	416.2	253.2	188.6	379.2	98.7	3519.2
1971	192.7	98.5	189.2	386.1	376.2	341.0	466.8	634.4	353.5	442.6	227.4	4150.3	
1972	124.5	60.9	172.7	325.0	641.9	325.9	217.2	234.7	596.6	530.5	323.0	3765.2	
1973	56.9	61.9	310.7	342.6	264.7	527.3	220.2	240.5	152.9	322.4	229.5	264.1	2993.6
1974	107.2	120.1	56.9	164.9	431.6	617.0	243.9	726.9	242.4	65.5	283.1	3923.2	
1975	76.6	271.2	224.9	460.0	653.2	535.6	183.2	366.8	324.5	684.1	668.5	217.3	4665.8
1976	54.3	159.5	221.1	129.5	384.3	153.6	302.2	245.3	155.1	361.0	523.8	366.8	3368.5
1977	19.1	126.3	229.3	404.8	676.5	473.6	110.9	183.7	200.0	530.7	338.8	360.9	3658.7
1978	164.7	120.9	122.9	425.2	435.2	296.5	194.4	308.9	427.5	429.4	258.5	3742.5	
1979	103.9	166.0	163.7	333.5	265.6	434.6	294.4	106.5	662.5	493.3	279.1	3940.4	
1980	42.7	27.7	21.4	379.2	400.5	333.9	327.3	273.2	220.5	293.6	507.6	249.5	3270.6
1981	99.4	145.9	174.1	260.1	292.5	317.5	325.8	141.1	124.4	199.6	379.8	187.5	3098.0
1982	55.5	24.4	316.1	455.3	632.8	307.2	267.2	237.5	628.0	638.8	129.4	4193.6	
1983	93.1	78.6	150.1	128.0	495.1	337.6	276.1	284.4	156.5	146.0	344.4	534.9	3553.5
1984	274.7	308.6	356.7	529.2	564.0	329.0	515.9	48.2	312.1	255.4	343.7	264.5	4182.0
1985	159.6	171.1	273.7	529.2	504.2	746.4	219.4	163.4	252.9	616.1	251.7	346.4	3975.9
1986	158.7	111.2	157.9	239.2	360.7	302.7	293.1	18.8	660.4	322.0	475.3	381.4	3547.0
1987	94.7	298.6	226.2	262.2	412.7	632.4	331.7	557.6	694.3	224.5	378.8	139.3	4285.0
1988	47.5	7.8	123.3	257.1	405.9	632.2	610.9	282.7	448.5	500.4	320.0	97.4	3733.7
1989	110.5	136.5	206.3	334.1	475.2	419.5	307.0	294.2	122.4	427.9	359.1	229.3	3722.0
AVERAGE	52.1	96.1	63.9	108.8	189.0	129.8	155.1	140.7	175.6	131.5	128.1	104.9	4339.0
STD. DEV.	274.7	388.6	356.7	569.6	984.1	641.5	640.2	653.6	152.9	684.1	668.5	534.8	4665.8
MAXIMUM	1.2	7.8	120.1	120.0	159.8	153.6	18.8	48.2	152.9	146.0	65.5	72.6	2998.6



PRIMFALL ANALYSIS

STATION : PELHAMDALE

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	296.9	267.7	159.2	317.2	304.2	242.5	238.7	86.3	319.0	209.8	113.0	92.4	2646.9
1961	117.6	168.6	165.3	150.1	167.3	239.2	319.7	419.1	389.6	423.1	247.9	240.5	3948.0
1962	123.9	134.6	175.7	329.9	735.0	283.2	163.3	105.1	363.7	360.1	330.7	171.1	3276.5
1963	230.6	189.9	427.2	275.8	276.8	324.1	276.8	399.0	342.3	308.8	414.4	237.9	3732.5
1964	136.4	170.6	279.5	258.5	360.9	312.1	464.3	173.2	146.2	251.7	366.5	160.2	3975.1
1965	8.8	62.9	500.9	256.7	595.1	231.1	60.4	355.6	350.5	368.0	319.7	314.7	3224.4
1966	112.2	192.3	236.2	154.6	76.2	194.8	108.7	208.5	704.0	300.9	265.2	151.6	2687.2
1967	104.3	106.1	219.2	242.5	275.0	298.7	228.6	221.9	127.0	631.1	452.6	122.1	3029.5
1968	345.2	97.7	144.5	166.3	323.5	384.5	363.4	113.7	301.7	422.4	141.9	272.7	3077.8
1969	180.5	72.8	166.4	307.7	909.6	246.6	37.0	260.8	199.6	380.1	241.3	350.2	3276.7
1970	215.9	195.5	241.3	317.5	114.3	203.2	292.1	132.0	168.1	169.9	355.6	177.6	3802.0
1971	196.8	210.8	266.7	320.0	254.0	368.3	304.8	431.8	612.8	381.0	457.2	99.3	4103.5
1972	45.9	8.6	235.9	362.5	642.8	127.7	270.0	170.1	532.1	17.5	313.1	135.3	3261.8
1973	41.1	135.6	418.1	152.1	324.6	104.6	316.9	163.1	378.7	340.6	361.6	3353.0	3953.0
1974	0.0	93.4	225.0	506.9	391.6	499.3	461.2	246.4	437.1	276.4	32.0	553.2	3572.4
1975	127.6	78.2	267.7	129.2	488.6	540.0	124.7	306.8	291.5	614.1	667.2	231.6	3697.1
1976	85.5	53.0	149.0	366.7	355.3	94.4	236.0	215.6	69.4	372.8	353.5	314.1	2668.3
1977	8.6	39.6	123.6	274.8	402.8	372.8	50.0	254.5	122.6	184.3	509.5	413.2	2969.6
1978	147.8	294.8	228.6	241.5	922.5	279.9	266.7	327.1	425.9	412.2	742.9	143.0	4192.9
1979	46.2	69.8	169.4	235.1	332.4	351.0	328.9	21.3	401.5	358.6	363.4	109.7	3008.3
1980	0.0	165.2	250.9	235.6	218.6	212.0	121.7	217.3	101.5	184.9	161.9	169.7	2238.1
1981	133.6	191.0	178.3	152.2	214.6	326.6	119.6	146.8	237.2	91.7	346.2	93.1	3273.1
1982	63.0	99.6	242.8	42.8	454.7	61.3	613.9	185.9	176.3	829.8	751.6	54.1	3175.0
1983	5.3	104.1	170.7	104.7	308.9	395.2	170.2	104.6	332.0	51.6	143.5	42.4	1933.5
1984	292.1	130.8	398.0	264.5	417.1	461.8	16.3	193.5	348.0	372.1	214.6	3060.3	3389.6
1985	206.3	166.9	193.3	207.5	150.8	522.7	190.8	106.4	122.4	336.8	510.0	378.7	3136.3
1986	110.8	230.2	230.2	284.6	398.7	308.2	241.7	215.4	326.0	312.8	366.7	214.6	3273.1
1987	0.0	27.9	321.8	320.0	8.9	8.9	282.8	159.5	572.4	420.1	214.6	3196.2	3496.8
1988	3.4	209.5	425.7	296.2	649.5	327.9	176.8	337.3	510.5	281.9	191.8	366.7	3034.0
1989	35.6	0.0	134.6	63.5	374.7	434.8	526.5	170.0	234.6	470.4	366.7	214.6	3273.1
AVERAGE	110.8	126.6	230.2	264.6	398.7	308.2	241.7	215.4	326.0	353.2	366.7	214.6	3136.3
STAND.DEV.	95.0	72.8	93.7	113.1	208.9	113.2	152.2	110.2	169.5	147.2	163.7	112.6	3176.8
MAXIMUM	345.2	294.8	415.7	568.1	922.5	540.0	613.9	431.8	612.8	644.1	751.6	653.2	4132.9
MINIMUM	0.0	27.9	63.5	76.2	86.3	8.9	16.3	89.4	51.6	32.0	42.4	32.0	1933.5

YEAR	TOTAL	RANK	PROBABILITY	10 Year Moving Average
1983	1933.5	1	0.03226	60.0
1981	2231.1	2	0.06452	61.1
1980	2238.1	3	0.09677	62.1
1982	2446.2	4	0.12903	63.1
1980	2646.9	5	0.16129	64.1
1976	2568.3	6	0.19355	65.1
1970	2880.2	7	0.22581	66.1
1966	2887.2	8	0.25806	67.1
1977	2909.6	9	0.29032	68.1
1979	3008.3	10	0.32259	69.1
1962	3029.6	11	0.35484	70.1
1969	3034.0	12	0.38710	71.1
1968	3077.5	13	0.41935	72.1
1961	3136.3	14	0.45161	73.1
1973	3153.0	20	0.48387	74.1
1964	3224.4	15	0.51613	75.1
1960	3226.5	16	0.54899	76.1
1972	3286.7	17	0.58065	77.1
1961	3281.6	18	0.61290	78.1
1974	3496.8	21	0.67742	79.1
1963	3572.4	25	0.68645	80.1
1964	3575.1	21	0.68711	81.1
1965	3660.3	22	0.70968	82.1
1984	3897.1	23	0.90323	83.1
1982	3476.6	24	0.77419	84.1
1988	3496.8	24	0.77419	85.1
1973	3572.4	25	0.80645	86.1
1964	3575.1	21	0.84516	87.1
1965	3660.3	22	0.83871	88.1
1984	3897.1	23	0.87097	89.1
1975	4103.5	29	0.93548	90.1
1978	4132.9	30	0.96774	91.1



RAINFALL ANALYSIS

STATION : MAHAWALI-ANTENNA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	277.8	267.9	360.4	399.2	60.2	6.3	160.4	18.5	39.1	302.5	131.3	173.2	2226.8
1961	266.1	68.3	275.5	432.3	149.3	60.7	94.2	75.1	40.3	220.4	294.6	205.7	2280.8
1962	276.7	99.0	265.4	362.2	280.9	31.7	69.8	14.4	129.0	308.3	291.6	157.2	2086.4
1963	274.3	124.7	266.7	462.5	309.4	138.1	62.3	13.7	75.6	381.7	786.6	501.3	3419.7
1964	78.4	115.0	378.9	310.6	90.9	105.9	122.9	14.4	142.7	144.7	59.9	72.8	1637.1
1965	5.5	245.1	207.2	293.6	290.2	57.1	12.7	73.9	90.4	190.2	422.6	280.9	2169.6
1966	165.1	62.7	205.2	394.4	1.7	42.4	36.9	20.3	219.2	146.6	229.3	176.2	2001.8
1967	117.0	127.2	231.9	326.8	147.5	77.7	34.6	64.0	15.7	369.5	467.3	144.2	2123.3
1968	129.7	10.9	159.5	175.2	117.8	76.7	91.6	2.2	75.1	542.5	278.3	234.6	1894.1
1969	32.5	146.8	100.8	165.9	164.5	72.8	7.3	66.5	49.2	162.2	412.4	2305.4	1917.0
1970	135.8	168.1	315.2	310.1	160.0	21.8	33.5	7.1	29.7	148.0	368.6	178.6	2179.9
1971	219.4	114.0	349.5	329.4	58.6	143.5	70.9	242.5	233.1	382.7	157.2	1024.5	1953.1
1972	46.4	20.5	142.9	144.7	215.6	7.3	72.3	12.9	127.7	319.2	322.3	92.7	1024.5
1973	71.1	0.5	302.8	338.3	118.1	66.2	22.3	35.0	5.3	411.9	270.0	314.6	1953.1
1974	253.2	131.0	359.9	97.2	75.6	120.9	44.1	98.0	116.1	126.4	419.6	1042.0	1953.1
1975	92.2	263.6	114.3	240.5	232.4	275.5	31.4	20.3	93.2	61.4	457.2	154.1	2036.1
1976	21.8	68.6	2.2	263.6	192.2	7.1	52.0	38.3	255.2	16.9	107.4	1114.7	1917.0
1977	167.6	329.9	265.1	352.6	59.1	34.2	0.0	36.3	534.1	336.2	190.9	2310.8	1932.8
1978	65.2	152.1	365.7	269.4	383.5	28.7	69.5	99.3	89.4	335.7	530.3	259.8	2649.6
1979	21.8	11.6	163.6	253.2	245.6	73.1	80.0	37.5	142.4	466.5	272.5	2077.1	1953.1
1980	2.0	33.5	130.8	195.3	156.2	55.3	36.5	73.1	28.1	347.7	56.1	1646.4	1953.1
1981	6.6	126.3	167.9	132.6	166.5	118.1	39.3	70.4	135.6	53.3	371.3	24.9	1404.8
1982	56.4	0.0	212.8	190.3	320.5	191.8	10.2	41.3	82.9	386.8	150.9	190.9	2147.8
1983	102.9	117.0	243.3	265.6	84.9	7.3	34.0	70.2	70.2	369.3	203.3	1932.8	1953.1
1984	270.8	152.8	104.2	319.2	60.5	83.0	92.4	6.9	154.4	123.3	457.9	245.4	2146.4
1985	103.6	197.8	379.8	191.9	321.9	351.2	5.4	41.5	41.5	62.9	283.2	319.5	190.9
1986	102.9	117.0	243.3	219.6	171.9	94.9	54.1	41.5	67.0	219.5	109.6	211.1	1953.1
1987	72.9	20.8	105.7	332.6	28.9	36.1	12.5	65.0	33.7	190.3	48.9	174.9	1522.3
1988	42.6	62.9	354.3	348.6	163.9	100.0	78.7	123.6	13.3	159.8	35.0	72.8	1941.9
1989	29.4	12.4	27.1	36.2	82.0	11.8	13.3	34.8	20.1	112.3	118.1	43.8	1941.9
AVERAGE	102.9	117.0	243.2	265.6	180.0	84.9	54.0	41.5	62.9	283.2	319.5	190.9	1953.1
STDEV.	84.8	88.1	109.2	99.0	108.0	74.8	39.8	31.1	57.9	135.3	162.3	112.5	1953.1
MAXIMUM	277.8	329.9	442.9	462.6	464.5	351.2	168.4	123.6	242.5	542.5	786.8	501.3	35.0
MINIMUM	0.0	0.9	2.2	4.2	1.7	7.1	0.7	0.0	5.3	53.3	35.0	3.0	541.9

YEAR TOTAL RANK PROBABILITY

10 Year Moving Average

Year

Avg.

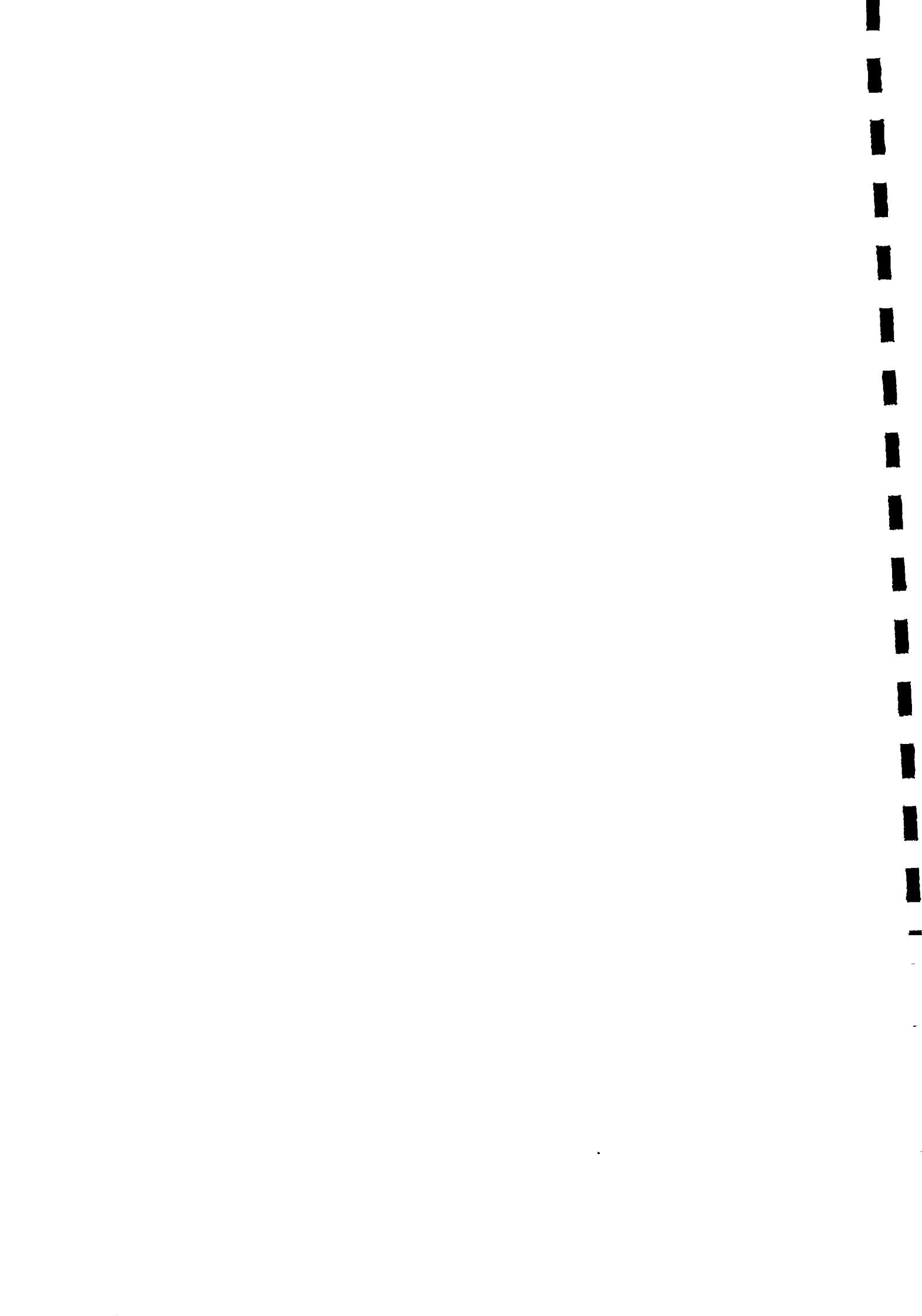
1969	541.9	1	0.03226	60	- 69	2204.5
1970	114.7	2	0.06152	61	- 70	2173.5
1971	1404.0	3	0.09677	62	- 71	2193.5
1972	1522.9	4	0.12903	63	- 72	2167.3
1973	1594.9	5	0.16129	64	- 73	2020.6
1974	1637.1	6	0.19355	65	- 74	2041.1
1975	1646.4	7	0.22581	66	- 75	2027.7
1976	1753.8	8	0.25806	67	- 76	1939.0
1977	1824.5	9	0.29032	68	- 77	1957.7
1978	1842.0	10	0.32258	69	- 78	2033.2
1979	1894.1	11	0.35464	70	- 79	2010.4
1980	1917.0	12	0.38710	71	- 80	1983.3
1981	1932.0	13	0.41935	72	- 81	1885.8
1982	1953.1	14	0.45161	73	- 82	1918.1
1983	2001.8	15	0.48387	74	- 83	1916.1
1984	2036.1	16	0.51613	75	- 84	1976.5
1985	2077.1	17	0.54039	76	- 85	2015.7
1986	2086.1	18	0.59065	77	- 86	2079.6
1987	2123.3	19	0.61290	78	- 87	2000.8
1988	2147.8	20	0.64516	79	- 88	1895.4
1989	2169.8	21	0.67742	80	- 89	1741.9
1990	2180.5	22	0.70968			
1991	2226.8	23	0.74194			
1992	2305.1	24	0.77419			
1993	2310.5	25	0.80645			
1994	2379.9	26	0.83871			
1995	2417.6	27	0.87097			
1996	2446.4	28	0.90323			
1997	2510.6	29	0.93546			
1998	2541.9	30	0.96774			



RAINFALL ANALYSIS

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	226.5	315.9	137.9	278.6	478.5	419.6	492.7	224.7	733.5	342.9	256.5	130.5	4032.9
1961	138.6	106.9	285.4	334.0	713.4	319.7	439.1	810.7	501.3	564.1	482.6	352.5	5048.3
1962	208.7	169.1	296.7	306.3	613.5	280.9	306.0	346.9	415.0	632.9	140.9	272.5	4191.7
1963	264.9	248.4	284.2	411.7	543.8	548.1	495.5	525.7	625.0	568.9	458.7	5226.8	5226.8
1964	135.1	205.2	419.0	290.5	655.7	429.7	702.0	306.0	654.0	406.4	456.9	158.4	5019.9
1965	86.3	134.8	419.6	378.4	934.2	467.6	121.6	770.6	544.3	473.1	502.1	354.0	5168.9
1966	102.3	147.3	327.9	654.0	275.5	261.6	193.5	315.2	951.9	375.1	380.2	166.1	4150.6
1967	121.9	118.3	213.3	270.7	245.8	465.6	296.9	419.9	310.8	817.3	196.7	4032.4	4032.4
1968	300.2	140.2	156.4	259.0	493.9	1013.9	570.2	334.7	507.7	364.9	390.6	418.5	1949.3
1969	73.6	95.5	312.4	1132.0	600.2	119.3	331.4	398.6	536.1	241.8	370.8	1370.8	1370.8
1970	246.8	206.5	374.9	418.3	276.6	530.6	456.1	391.9	444.2	661.8	284.4	181.6	4173.5
1971	132.0	224.7	233.1	595.8	652.7	545.5	470.4	576.5	1191.7	391.9	162.0	5701.8	5701.8
1972	102.8	35.5	131.5	261.1	615.9	367.7	539.1	472.1	937.5	784.0	530.8	129.2	5106.9
1973	96.5	148.0	226.8	318.5	292.6	613.4	411.4	348.7	166.4	428.4	391.1	447.2	3879.0
1974	0.0	291.3	205.2	417.0	566.6	667.7	917.4	382.2	889.7	365.7	239.7	357.5	5309.8
1975	32.2	201.4	353.5	618.6	666.9	912.6	273.3	758.9	496.3	1040.8	772.4	332.9	5569.8
1976	92.7	80.0	178.8	619.7	337.0	219.2	458.2	372.8	202.6	479.0	540.2	404.1	3984.3
1977	43.1	180.0	298.1	470.6	754.7	519.6	148.8	323.7	343.4	674.6	520.9	346.2	4553.6
1978	165.3	372.1	236.4	310.6	830.3	291.8	424.6	504.2	747.7	306.8	561.9	168.6	5100.3
1979	90.6	198.3	203.2	264.1	734.0	501.3	398.7	116.8	913.3	577.0	626.8	223.5	4049.8
1980	53.6	54.9	138.2	386.6	417.6	412.5	476.0	519.8	576.6	329.7	428.2	350.7	3824.1
1981	158.0	118.1	238.2	317.2	412.0	557.0	501.7	412.8	601.0	273.8	541.5	156.5	4135.8
1982	94.0	37.9	330.4	395.7	751.8	1210.6	497.3	298.7	272.8	653.8	693.9	100.6	5277.2
1983	56.4	103.1	67.9	57.4	423.1	450.1	332.5	164.4	530.9	214.9	296.2	459.2	3196.1
1984	349.9	196.1	103.6	685.6	775.5	512.0	717.1	82.5	451.3	405.6	386.9	165.4	5223.6
1985	306.8	119.6	139.7	195.3	628.8	1159.1	392.7	285.0	396.0	636.9	276.9	407.7	5272.9
1986	133.9	294.4	129.0	430.0	362.0	313.8	313.8	359.1	7.9	436.1	715.8	505.0	4268.5
1987	160.1	18.2	165.8	486.3	503.3	359.1	638.1	410.8	605.0	594.6	149.6	4168.5	4168.5
1988	125.2	198.3	415.5	478.0	745.0	690.4	545.6	635.1	161.1	174.1	293.1	183.9	5800.4
1989	95.5	8.9	176.8	389.1	977.9	887.5	814.1	515.9	728.5	744.7	650.5	137.7	6129.1
AVERAGE	137.5	170.0	257.5	385.7	623.0	550.9	426.3	432.3	573.1	513.9	453.0	265.1	4789.3
STANDARD DEV.	86.2	107.0	100.3	136.8	232.6	251.5	200.9	190.5	246.9	191.1	142.2	108.9	719.4
MINIMUM	0.0	498.3	438.0	685.5	1132.0	1210.6	917.4	835.1	1191.7	1040.8	772.4	459.2	6553.8
MAXIMUM	349.5	498.3	87.9	687.4	245.8	219.2	82.5	156.4	174.0	239.7	100.6	3498.1	3498.1

YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE
1983	3496.1	1	0.03226	60 - 69
1980	3824.1	2	0.06452	61 - 70
1973	3079.0	3	0.09677	62 - 71
1976	3984.3	4	0.12903	63 - 72
1987	4032.4	5	0.16129	64 - 73
1980	1037.8	6	0.19355	65 - 74
1981	1135.8	7	0.22581	66 - 75
1986	1150.6	8	0.25806	67 - 76
1987	1168.5	9	0.29032	68 - 77
1986	1286.5	10	0.32258	69 - 78
1969	1370.8	11	0.35484	70 - 79
1970	1473.5	12	0.38710	71 - 80
1962	1491.7	13	0.41935	72 - 81
1977	1553.6	14	0.45161	73 - 82
1979	1484.9	15	0.46387	74 - 83
1968	1494.9	16	0.51613	75 - 84
1984	1619.9	17	0.54839	76 - 85
1961	5048.3	18	0.58065	77 - 86
1985	5272.9	21	0.77419	78 - 87
1982	5100.3	19	0.61290	79 - 88
1972	5106.9	20	0.64516	80 - 89
1965	5188.9	21	0.67742	80 - 89
1971	5701.5	27	0.87097	80 - 89
1988	5800.4	28	0.90323	80 - 89
1989	6129.1	29	0.93548	80 - 89
1975	6559.8	30	0.96774	80 - 89



RAINFALL ANALYSIS

STATION NAME: HAMBURG

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	231.9	139.7	96.0	199.1	18.2	0.0	162.8	11.6	110.4	325.6	278.6	93.9	1662.9
1961	378.9	141.4	173.9	238.2	67.8	25.1	42.1	29.4	19.0	271.5	237.7	82.8	1737.6
1962	87.6	30.7	79.5	225.2	106.9	7.3	8.3	13.2	13.9	89.5	290.0	195.0	1144.1
1963	131.0	80.0	66.1	235.9	152.9	19.8	35.8	7.6	28.4	108.1	393.7	93.9	1675.2
1964	131.0	112.2	135.3	177.8	62.9	23.6	195.9	7.1	62.9	132.5	73.6	32.5	1068.3
1965	0.0	159.5	168.9	285.2	125.7	7.3	22.0	82.0	41.4	235.9	345.4	154.9	1628.2
1966	53.3	20.3	379.2	481.3	25.4	50.8	12.7	162.8	93.9	144.7	1721.2		
1968	45.9	82.6	155.9	230.9	72.5	18.7	34.9	29.1	66.0	208.1	251.6	144.1	1340.1
1969	9.3	50.0	162.5	431.0	208.0	28.1	0.0	220.7	39.6	309.6	205.9	317.7	1962.4
1970	92.7	218.6	153.9	177.0	16.5	0.0	25.6	0.0	106.2	146.8	637.7	263.9	2140.9
1971	103.1	261.8	135.1	199.0	0.0	0.0	73.1	81.5	192.6	261.4	180.3	1501.8	
1972	0.0	0.0	203.2	370.8	147.3	0.0	0.0	0.0	36.1	276.3	156.2	1260.6	
1973	15.2	86.3	166.6	97.0	43.9	44.7	39.3	26.9	203.9	319.2	273.8	271.7	1510.5
1974	4.3	87.1	135.3	210.3	34.0	2.4	12.7	13.7	24.8	92.1	334.7	39.6	923.6
1975	17.7	15.7	169.1	321.0	132.0	65.2	117.0	7.1	95.8	12.7	348.1	136.9	1410.3
1976	22.3	0.0	95.2	135.8	0.0	0.0	0.0	0.0	7.6	231.1	373.8	221.9	1067.7
1977	0.0	147.0	71.1	255.7	107.6	8.8	27.9	13.2	36.8	132.8	385.8	51.0	1537.7
1985	64.4	70.2	390.2	53.6	119.3	64.6	4.1	24.0	115.6	12.8	137.1	489.2	1744.7
1986	129.0	108.3	210.6	16.9	37.1	15.2	0.0	21.9	3.1	80.3	47.5	2.5	810.4
1987	16.2	0.0	46.2	110.3	11.1	0.0	0.0	23.1	83.9	268.0	87.2	109.6	755.6
1988	9.4	66.6	121.4	169.4	40.6	17.8	14.0	24.6	44.5	79.8	266.4	67.1	941.6
1989	18.6	0.0	61.2	64.5	66.0	12.7	77.9	0.0	34.5	22.1	33.0	9.4	399.9
AVERAGE	71.0	82.6	155.9	230.9	72.5	18.7	34.9	29.1	66.0	208.1	251.6	144.1	1345.5
STAND. DEV.	89.3	72.1	86.2	120.2	55.9	20.1	46.0	46.6	49.5	118.6	139.5	113.3	422.3
MAXIMUM	378.9	261.6	390.2	481.3	208.0	65.2	162.8	220.7	203.9	32.8	637.7	489.2	2140.9
MINIMUM	0.0	0.0	46.2	83.6	0.0	0.0	0.0	3.1	12.7	33.0	2.6	399.9	

YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE
1989	399.9	1	0.04348	60 - 70
1987	755.6	2	0.06696	61 - 71
1986	610.4	3	0.13043	62 - 72
1974	923.6	4	0.17391	63 - 73
1988	941.6	5	0.21739	64 - 74
1976	1087.7	6	0.26067	65 - 75
1984	1088.3	7	0.30435	66 - 76
1962	1141.1	8	0.34763	66 - 77
1972	1260.6	9	0.39130	69 - 85
1968	1340.4	10	0.43478	70 - 86
1975	1440.3	11	0.47826	71 - 87
1971	1501.8	12	0.52174	72 - 88
1966	1721.2	18	0.78261	73 - 89
1961	1737.8	19	0.82609	74 - 90
1985	1744.7	20	0.86957	75 - 91
1969	1822.4	21	0.91304	76 - 92
1970	2140.9		0.95652	



RAINFALL ANALYSIS

STATION : LAUDERDALE GROUP

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTL
1960	149.5	341.1	164.3	319.2	295.9	193.8	323.5	65.5	726.6	326.3	294.8	74.1	3577.6
1961	258.5	76.9	155.7	330.2	498.0	263.9	192.2	356.6	237.9	429.2	596.3	399.2	3791.1
1962	303.5	161.0	302.5	711.4	712.9	262.2	341.3	602.2	514.8	559.3	563.3	602.4	625.6
1963	247.9	163.6	221.2	570.9	523.2	579.6	726.6	157.5	462.5	340.8	153.1	206.7	179.3
1964	270.0	169.1	371.0	336.0	576.5	579.6	726.6	162.4	472.1	451.3	335.0	411.9	409.4
1965	6.0	4.5	128.2	355.0	587.2	159.7	70.6	247.1	451.3	335.0	411.9	409.4	473.2
1965	40.4	4.5	815.3	232.4	56.3	156.7	92.9	37.8	669.5	522.2	185.4	284.2	3164.9
1967	215.6	113.0	232.9	298.1	204.2	351.2	159.7	246.6	227.3	814.0	392.1	295.4	2165.3
1968	160.5	49.5	69.5	79.7	127.2	557.5	570.7	135.1	348.8	139.7	131.6	146.8	3682.1
1969	43.4	101.0	292.8	309.1	1265.1	372.8	86.8	294.9	271.4	562.6	335.0	2518.5	4701.6
1970	208.7	138.9	419.8	282.4	277.6	246.1	223.0	220.2	201.4	374.1	484.8	195.3	3272.1
1971	264.1	192.0	147.0	398.5	288.7	355.3	279.9	312.6	850.6	193.8	813.3	453.8	4549.5
1972	131.1	69.8	121.1	240.5	637.9	177.5	278.3	260.0	613.9	530.6	634.2	99.8	3197.9
1973	62.7	191.5	516.0	262.8	107.9	339.3	140.9	303.8	474.9	514.3	232.6	361.5	3157.3
1974	11.4	90.4	11.9	263.1	331.7	133.5	130.7	250.9	214.6	276.3	166.8	2166.2	4701.6
1975	93.7	159.7	215.3	412.8	605.5	141.4	304.8	295.4	475.4	423.9	422.4	3161.7	4701.6
1976	122.4	45.7	252.9	269.7	227.0	67.8	162.6	56.1	302.7	386.0	427.9	2454.7	4701.6
1977	6.8	141.7	217.1	343.4	439.6	224.0	224.0	255.1	212.5	330.7	874.8	264.9	3262.3
1978	83.0	245.1	240.7	246.3	707.6	181.8	224.6	111.7	368.3	291.5	723.1	194.8	3116.4
1979	55.8	103.1	55.1	334.0	389.0	284.0	273.2	116.1	489.7	386.1	468.1	350.9	3284.8
1980	36.1	8.9	105.2	252.0	132.6	269.2	219.0	291.0	89.9	229.9	140.9	200.8	1829.5
1981	93.2	159.8	67.6	387.5	406.1	371.2	89.7	317.3	119.7	162.5	371.3	155.3	2714.2
1982	0.0	80.1	236.2	547.4	643.2	651.8	315.4	192.0	62.9	383.6	621.0	87.4	1621.0
1983	117.6	119.1	68.9	41.6	293.3	141.8	122.2	186.6	302.0	124.3	251.8	366.7	2362.3
1984	412.9	140.9	254.7	504.9	257.5	347.3	245.4	0.0	246.1	337.8	529.7	134.4	3116.4
1985	214.9	226.4	311.4	199.4	557.1	771.2	107.8	72.0	107.9	619.7	344.3	319.4	3157.3
1986	129.7	168.6	198.6	163.5	115.4	120.0	100.9	335.3	505.8	264.5	213.4	149.0	2166.2
1987	129.5	0.0	175.0	252.6	175.0	221.7	0.0	413.8	89.6	181.2	192.1	212.5	2166.2
1988	78.7	101.5	221.4	330.2	310.5	281.7	173.0	255.1	348.8	378.6	403.5	294.5	377.5

YEAR	TOTAL	RANK	PROBABILITY	10 Year Moving Average
1980	1973.6	1	0.03333	60 - 69
1983	2161.1	2	0.06667	61 - 70
1987	2412.5	3	0.10000	62 - 71
1976	2454.7	4	0.13333	63 - 72
1968	2518.6	5	0.16667	64 - 73
1981	2741.2	6	0.20000	65 - 74
1966	2765.3	7	0.23333	66 - 75
1983	2774.7	8	0.26667	67 - 76
1974	2966.2	9	0.30000	68 - 77
1965	3164.9	10	0.33333	69 - 78
1988	3177.5	11	0.36667	70 - 79
1973	3257.3	12	0.40000	71 - 80
1977	3262.5	13	0.43333	72 - 81
1970	3272.4	14	0.46667	73 - 82
1979	3284.8	15	0.50000	74 - 83
1984	3411.6	16	0.53333	75 - 84
1975	3452.1	17	0.56667	76 - 85
1960	3577.6	18	0.60000	77 - 86
1982	4024.0	24	0.63333	78 - 87
1964	4373.2	25	0.66667	79 - 88
1965	3851.5	20	0.70000	
1978	3918.4	21	0.73333	
1984	3981.7	22	0.76667	
1972	3997.9	23	0.80000	
1961	3794.1	19	0.63333	
1964	4373.2	25	0.66667	
1971	4549.6	26	0.66667	
1969	4701.2	27	0.90000	
1962	5693.9	28	0.93333	
1963	5732.9	29	0.96667	



RAINFALL ANALYSIS

STATION NAME: GODAKAMELA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	194.0	192.7	203.9	229.8	135.6	90.4	236.5	35.8	179.3	320.5	160.5	88.6	2070.4
1961	217.6	156.2	115.8	125.2	143.7	72.3	125.2	172.9	102.8	226.0	409.4	165.1	2032.2
1962	169.1	121.9	160.7	220.7	334.2	34.0	134.1	73.6	124.4	167.3	240.5	193.5	1974.0
1963	230.6	147.5	148.0	350.7	233.6	135.6	112.5	112.2	168.6	223.5	353.8	231.6	2446.2
1964	29.1	116.5	285.2	205.4	131.8	100.8	159.0	74.6	209.8	116.3	115.0	184.9	1726.7
1965	32.0	150.8	142.7	356.6	204.4	59.6	40.1	134.8	158.4	256.5	320.0	213.8	2068.7
1966	88.9	28.7	382.2	219.9	29.2	57.9	96.2	60.9	298.1	352.5	146.0	177.9	1938.3
1967	74.1	111.2	92.7	218.4	113.0	198.0	136.6	122.1	61.7	512.5	378.2	69.1	2105.6
1968	226.0	8.6	247.3	168.4	111.9	238.6	213.8	57.9	168.4	257.8	101.3	141.4	1973.0
1969	16.5	73.4	137.9	196.5	106.4	108.4	61.9	166.1	367.7	234.4	630.4	2485.4	
1970	118.1	78.7	310.6	204.4	165.1	134.1	122.6	86.1	61.7	217.9	367.0	252.4	2116.7
1971	181.6	223.0	451.3	202.7	96.7	156.2	116.0	121.1	329.6	272.2	378.7	252.2	2681.3
1972	22.3	15.2	163.3	102.3	299.7	53.3	151.6	81.5	239.7	363.2	482.6	127.0	2101.7
1973	33.7	6.6	439.1	261.6	51.8	123.4	37.3	182.3	14.9	233.9	242.6	203.4	1690.5
1974	1.7	15.6	64.0	323.4	90.4	119.6	219.7	165.9	261.1	61.9	138.9	121.1	1609.7
1975	9.1	57.1	144.7	107.9	412.4	123.4	310.6	221.7	350.0	483.3	144.5	2605.4	
1976	18.2	3.5	312.1	301.1	103.6	25.6	62.4	0.0	146.8	299.9	429.5	1787.2	
1977	7.6	129.7	134.0	222.7	198.1	190.2	44.9	38.3	40.1	350.2	327.1	225.6	2208.7
1978	126.7	128.7	165.8	223.5	95.5	95.5	96.2	159.7	223.5	330.4	386.1	2036.1	
1979	129.5	34.2	12.1	92.7	176.2	234.9	170.6	55.3	287.7	205.4	157.2	180.3	1915.7
1980	3.0	12.7	50.9	279.4	101.6	76.2	105.4	76.2	127.0	152.4	182.6	132.0	1600.1
1981	92.5	84.0	329.2	172.2	127.9	113.5	100.1	143.2	246.0	129.6	31.0	2086.2	
1982	29.0	62.5	239.0	341.3	275.9	315.6	134.6	50.0	187.9	29.2	79.5	2178.6	
1983	16.0	57.1	37.6	83.1	91.7	55.9	90.7	85.6	176.1	142.9	220.6	355.5	1419.8
1984	269.2	131.5	207.0	301.3	167.2	155.5	150.9	16.0	159.5	105.2	393.8	117.1	2168.2
1985	83.6	170.5	277.9	107.9	290.6	343.1	56.4	57.3	120.9	367.7	337.3	211.7	2434.1
1986	119.5	107.9	169.3	299.8	15.3	102.7	47.6	184.6	219.2	221.7	176.1	51.1	1694.8
1987	177.7	23.8	56.7	183.5	86.6	63.2	0.0	166.0	115.0	257.0	247.2	111.4	1490.1
1988	118.1	155.5	252.2	300.7	128.9	132.4	26.5	92.9	197.6	24.4	461.5	216.3	2159.5
1989	31.0	0.0	105.7	179.5	174.5	126.0	271.6	91.9	98.7	260.3	185.4	26.2	1550.8
AVERAGE	95.6	86.8	204.8	223.4	178.5	132.2	117.3	103.5	152.8	239.8	311.1	180.7	2026.4
STAND.DEV.	79.9	62.8	120.7	79.7	104.2	77.8	81.8	60.9	102.6	118.0	121.7	93.2	1301.3
MAXIMUM	269.2	223.0	451.3	355.6	112.4	343.1	271.6	310.6	329.6	512.5	483.3	630.1	2881.3
MINIMUM	1.7	0.0	12.1	83.1	15.3	25.6	0.0	16.0	0.0	24.4	101.3	26.2	1413.8

YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE
1983	1413.8	1	0.03226	2082.5
1987	1490.1	2	0.06452	2087.3
1989	150.0	3	0.03677	2087.3
1980	160.1	4	0.12903	2172.2
1974	1609.7	5	0.16129	2185.0
1986	1694.6	6	0.19355	2123.2
1984	1728.7	7	0.22581	2111.3
1978	1767.2	8	0.25806	2165.0
1973	1830.5	9	0.29032	2147.9
1966	1938.3	10	0.32258	2158.2
1968	1973.0	11	0.35484	2162.4
1982	1971.0	12	0.38710	2117.5
1978	2015.7	13	0.41935	2065.6
1981	2032.2	14	0.45161	1985.9
1979	2036.1	15	0.48387	1986.3
1965	2068.7	16	0.57742	1994.0
1980	2070.4	17	0.51613	1952.4
1981	2088.2	18	0.54039	2010.2
1972	2101.7	19	0.58065	2117.5
1977	2208.7	25	0.61290	2117.5
1985	2434.1	26	0.64516	2127.8
1963	2448.2	27	0.87097	1879.2
1969	2485.4	28	0.90323	1879.2
1975	2605.1	29	0.93548	1879.2
1971	2881.3	30	0.96774	1879.2



Rainfall Analysis

STATION : EMBILIPITTA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	114.9	110.8	33.8	305.2	61.4	14.7	161.6	3.2	94.3	284.8	215.0	90.9	1498.6
1961	202.7	184.7	150.5	47.0	96.1	18.6	58.8	56.3	201.1	226.3	128.9	1508.6	
1962	215.3	34.5	94.9	167.9	140.1	21.3	28.5	20.4	113.2	103.5	375.9	160.3	1471.0
1963	115.8	66.6	59.7	92.1	141.8	46.4	22.3	68.3	395.4	317.5	96.0	1471.0	
1964	115.8	96.4	141.8	151.6	85.5	32.2	92.6	43.8	78.2	93.4	66.6	78.2	1092.1
1965	0.0	143.8	98.6	114.1	178.1	11.6	68.5	68.5	103.0	280.0	324.4	184.0	1572.6
1966	68.5	72.1	216.0	287.7	2.5	9.1	13.1	20.0	216.9	291.5	90.7	143.1	1431.5
1967	68.5	44.4	19.3	221.6	112.2	31.8	87.3	43.4	51.1	369.5	198.6	26.2	1334.2
1968	322.4	0.0	115.7	69.0	105.0	74.4	66.2	7.5	36.0	5.7	324.4	66.4	1917.7
1969	2.7	5.5	197.9	224.5	170.0	33.3	0.7	222.8	102.2	367.3	598.7	2188.1	
1970	167.1	61.7	169.9	176.2	75.3	11.3	32.8	22.7	16.1	42.1	293.7	198.6	1918.8
1971	38.3	60.1	155.8	142.4	82.4	34.6	31.9	35.5	23.2	305.2	144.4	279.6	1383.4
1972	19.7	61.7	83.6	190.4	92.5	39.2	52.4	40.0	109.6	73.5	104.9	105.6	873.7
1973	13.5	54.5	151.9	251.6	161.8	330.6	188.0	65.6	30.8	47.4	289.9	208.8	1778.0
1974	24.8	3.0	36.7	242.2	85.7	5.1	17.1	30.2	23.3	211.2	341.6	91.6	118.0
1975	19.7	43.7	169.7	93.9	131.1	12.3	9.5	63.9	38.1	266.7	291.0	127.2	1242.6
1976	34.1	46.2	15.7	79.0	212.1	8.9	25.0	78.3	106.9	136.2	93.7	94.3	
1977	2.0	107.2	2.3	202.3	129.5	91.8	19.8	3.3	91.4	88.6	318.2	290.5	1269.9
1978	19.8	0.8	42.6	210.9	56.7	16.3	25.5	1.0	53.6	118.3	555.8	290.5	374.3
1979	19.8	5.1	45.5	127.1	117.1	201.8	112.5	47.6	48.8	12.7	277.8	439.1	106.3
1980	19.8	0.0	45.0	22.6	43.5	52.0	6.1	29.2	13.2	87.3	132.5	265.4	1541.0
1981	19.8	61.3	155.2	183.8	114.2	52.3	24.1	391.1	8.5	13.2	331.7	291.3	129.5
1982	19.8	54.7	253.6	47.4	154.0	15.6	4.7	18.4	135.0	264.6	223.9	178.9	1562.4
1983	19.8	143.2	128.7	137.5	49.0	18.6	6.7	55.1	99.2	165.0	57.0	43.9	1001.3
1984	19.8	66.6	1.1	167.1	238.2	28.8	11.3	0.0	111.5	101.1	265.2	57.0	54.5
1985	19.8	40.6	149.5	177.7	82.5	13.6	50.2	37.7	79.9	187.3	314.8	123.1	1361.8
1986	19.8	66.9	120.7	152.8	111.9	44.4	54.9	41.2	71.8	201.2	243.6	160.1	1345.3
1987	19.8	51.9	68.7	72.8	67.5	38.1	76.6	43.5	45.9	112.5	121.5	114.8	308.6
1988	19.8	184.1	253.6	305.2	330.6	145.6	391.1	222.8	216.9	395.4	555.8	598.7	2181.1
1989	19.8	0.0	2.3	43.5	2.5	54.6	0.0	1.0	12.7	5.7	57.0	26.2	652.9
AVERAGE	75.9	66.9	120.7	152.8	111.9	44.4	54.9	41.2	71.8	201.2	243.6	160.1	1345.3
STD.DEV.	79.9	51.9	68.7	72.8	67.5	38.1	76.6	43.5	45.9	112.5	121.5	114.8	308.6
MAXIMUM	321.4	184.1	253.6	305.2	330.6	145.6	391.1	222.8	216.9	395.4	555.8	598.7	2181.1
MINIMUM	0.0	0.0	0.0	2.3	2.5	54.6	0.0	1.0	12.7	5.7	57.0	26.2	652.9

YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE
1983	657.9	1	0.03704	60 - 69
1974	678.7	2	0.07407	61 - 70
1978	949.3	3	0.11111	62 - 73
1985	1001.3	4	0.14815	63 - 74
1984	1097.1	5	0.10519	64 - 75
1976	1116.0	6	0.22222	55 - 76
1987	1122.7	7	0.25926	66 - 77
1970	1120.8	8	0.29630	67 - 78
1968	1191.7	9	0.33333	68 - 79
1977	1247.6	10	0.37037	69 - 80
1979	1269.9	11	0.40741	70 - 82
1967	1311.2	12	0.44144	73 - 83
1966	1364.8	13	0.48148	74 - 84
1960	1371.3	14	0.51652	75 - 85
1973	1388.1	15	0.55556	76 - 86
1966	1436.5	16	0.59259	77 - 87
1963	1471.0	17	0.62963	78 - 88
1962	1476.8	18	0.66667	
1960	1490.6	19	0.70370	
1961	1506.8	20	0.74074	
1982	1541.0	21	0.77778	
1985	1562.4	22	0.81481	
1965	1572.6	23	0.85185	
1984	1579.5	24	0.88669	
1975	1778.0	25	0.92593	
1969	2188.1	26	0.96296	



וְאֶת־עַמּוֹדָה

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	146.9	324.2	120.4	174.5	340.4	356.2	603.3	137.5	411.8	421.7	135.4	116.1	3888.4
1961	143.6	144.6	361.7	522.3	639.1	3865.9	364.8	573.1	470.7	322.6	4771.1	424.5	4771.1
1962	93.4	45.8	234.7	470.7	675.7	307.9	277.2	293.9	365.6	622.1	516.9	62.6	1024.5
1963	149.9	363.3	157.7	856.8	510.5	466.2	433.4	743.9	654.9	270.0	572.3	277.7	5573.6
1964	49.8	113.0	177.6	393.8	745.8	350.3	654.9	290.6	448.9	572.3	344.2	161.6	4453.1
1965	93.5	171.6	364.0	367.1	757.7	229.4	189.8	690.9	587.9	344.0	419.1	1486.6	4186.6
1966	162.1	34.8	315.0	615.2	174.8	247.2	204.0	762.8	698.0	358.1	401.6	4168.1	4168.1
1967	90.2	94.8	387.7	216.2	872.0	529.5	316.8	306.9	791.9	299.3	226.6	4224.6	4224.6
1968	91.5	108.5	482.6	490.3	300.5	735.1	432.4	225.9	355.9	306.4	16.6	4286.0	4286.0
1969	69.8	279.0	74.5	808.6	1123.0	325.7	68.5	291.4	276.9	513.9	327.5	163.9	4386.9
1970	127.6	186.5	386.9	627.8	47.3	419.3	234.5	355.9	672.6	205.0	295.2	4386.9	4386.9
1971	192.3	153.0	129.3	573.8	625.1	481.1	293.9	505.5	666.8	382.8	233.7	233.7	233.7
1972	20.1	23.4	77.7	380.5	630.0	537.8	213.7	166.9	640.6	776.5	839.0	1449.7	1449.7
1973	23.4	320.6	305.6	329.7	307.4	492.8	321.1	236.3	185.7	428.9	304.3	376.3	376.3
1974	0.0	172.3	234.7	570.7	459.5	465.4	585.3	220.6	727.0	223.3	63.6	3962.4	3962.4
1975	91.4	151.5	309.7	434.9	616.4	497.6	363.3	312.2	592.4	624.6	947.5	131.1	5162.7
1976	35.6	17.3	216.5	478.6	221.8	197.2	303.6	481.8	154.0	519.5	505.0	281.5	3792.6
1977	15.5	204.0	426.3	512.9	746.0	546.7	93.0	270.3	234.7	612.8	374.7	150.7	4375.6
1978	167.7	279.7	160.8	349.0	931.2	187.5	251.3	210.4	368.3	543.9	636.1	262.7	4350.6
1979	60.2	410.1	252.6	353.6	368.9	168.9	325.9	106.7	801.2	568.5	605.8	319.1	4730.7
1980	1.3	13.1	193.6	415.6	479.9	293.4	294.2	312.9	344.0	414.3	599.2	238.6	3650.1
1981	145.0	143.3	267.7	321.6	399.5	379.1	235.5	210.6	606.8	493.8	507.2	242.2	3982.7
1982	29.7	0.0	214.6	545.1	727.5	686.5	338.9	241.2	625.6	654.3	632.5	211.3	4607.1
1983	17.3	18.6	25.3	803.8	194.3	320.5	216.4	356.7	738.1	319.3	340.8	706.5	3337.8
1984	355.3	270.4	391.0	811.0	774.9	389.5	593.1	367.1	257.4	276.3	621.8	34.9	4812.5
1985	332.6	319.3	292.4	163.5	652.4	743.2	157.2	319.6	168.5	527.4	305.6	470.9	4729.2
1986	162.5	194.3	251.0	196.3	319.6	239.5	15.0	424.6	232.7	630.2	546.7	304.3	3610.7
1987	154.8	17.8	21.2	202.5	442.6	232.7	15.0	672.0	672.0	304.8	724.1	365.6	199.0
1988	56.7	196.2	315.2	416.1	191.3	472.3	585.1	564.7	129.7	416.8	80.5	4092.2	4092.2
1989	27.7	15.2	127.3	212.9	313.9	741.8	596.5	215.6	420.3	463.5	265.4	146.2	3547.3
AVERAGE	103.9	160.5	244.2	428.9	531.2	434.9	338.6	311.4	470.7	534.0	421.1	250.3	4229.8
STAND. DEV.	85.5	119.1	119.7	153.8	230.6	179.1	192.3	157.9	189.9	178.9	172.6	138.1	529.3
MAXIMUM	355.3	418.1	482.6	811.8	1123.0	872.0	864.9	690.9	801.2	827.3	947.5	706.5	3337.8
MINIMUM	0.0	0.0	21.2	63.8	174.6	168.5	15.0	36.1	154.0	129.7	63.6	34.9	3337.8
YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE									
1983	3337.9	1	0.03226	50	-	69	50	-	69	4961.8	4911.6	4911.6	4911.6
1987	3352.4	2	0.06452	0.09677	62	-	70	62	-	71	4797.4	4797.4	4797.4
1976	3332.6	3	0.12903	0.16129	63	-	72	63	-	73	1490.9	1490.9	1490.9
1989	3547.3	4	0.19355	0.22581	64	-	73	64	-	74	1313.2	1313.2	1313.2
1986	3610.7	5	0.22581	0.25806	65	-	75	65	-	75	1284.1	1284.1	1284.1
1980	3650.1	6	0.35484	0.29032	66	-	76	66	-	77	1295.7	1295.7	1295.7
1973	3796.0	7	0.3952	0.32250	67	-	76	67	-	77	1231.2	1231.2	1231.2
1981	3888.1	8	0.4244	0.39710	68	-	77	68	-	78	1216.1	1216.1	1216.1
1974	3962.1	9	0.45161	0.45161	69	-	77	69	-	78	1161.7	1161.7	1161.7
1972	4024.5	10	0.49387	0.49387	70	-	78	70	-	79	4135.9	4135.9	4135.9
1962	4024.5	11	0.51613	0.51613	71	-	78	71	-	79	4220.9	4220.9	4220.9
1988	4092.2	12	0.54839	0.54839	72	-	79	72	-	80	4239.7	4239.7	4239.7
1972	4139.5	13	0.58065	0.49135	73	-	80	73	-	81	4268.3	4268.3	4268.3
1966	4188.1	14	0.61290	0.49135	74	-	80	74	-	81	4194.7	4194.7	4194.7
1967	4224.6	15	0.64516	0.49135	75	-	82	75	-	82	4145.0	4145.0	4145.0
1971	4266.0	16	0.67742	0.49135	76	-	82	76	-	83	4069.5	4069.5	4069.5
1968	4266.0	17	0.67742	0.49135	77	-	82	77	-	83	4095.2	4095.2	4095.2
1978	4350.6	18	0.74194	0.50065	78	-	85	78	-	86	4069.2	4069.2	4069.2
1963	4360.6	19	0.74194	0.50065	79	-	86	79	-	87	3959.2	3959.2	3959.2
1985	4467.4	20	0.80645	0.77419	80	-	88	80	-	89	0.96774	0.96774	0.96774
1961	4471.9	21	0.83871	0.77419	81	-	88	81	-	89	0.93548	0.93548	0.93548
1964	4453.1	22	0.87097	0.74194	82	-	88	82	-	89	0.90323	0.90323	0.90323
1982	4507.1	23	0.87097	0.74194	83	-	88	83	-	89	0.93548	0.93548	0.93548
1979	4647.4	24	0.87419	0.77419	84	-	88	84	-	89	0.96774	0.96774	0.96774
1970	4386.9	25	0.88045	0.77419	85	-	88	85	-	89	0.96774	0.96774	0.96774
1971	4414.9	26	0.8871	0.77419	86	-	88	86	-	89	0.96774	0.96774	0.96774
1964	4453.1	27	0.8871	0.77419	87	-	88	87	-	89	0.96774	0.96774	0.96774
1965	4466.7	28	0.90323	0.77419	88	-	88	88	-	89	0.96774	0.96774	0.96774
1979	4582.7	29	0.93548	0.77419	89	-	88	89	-	89	0.96774	0.96774	0.96774
1983	4573.5	30	0.96774	0.77419	90	-	88	90	-	89	0.96774	0.96774	0.96774



RAINFALL ANALYSIS

STATION : BALANGODA

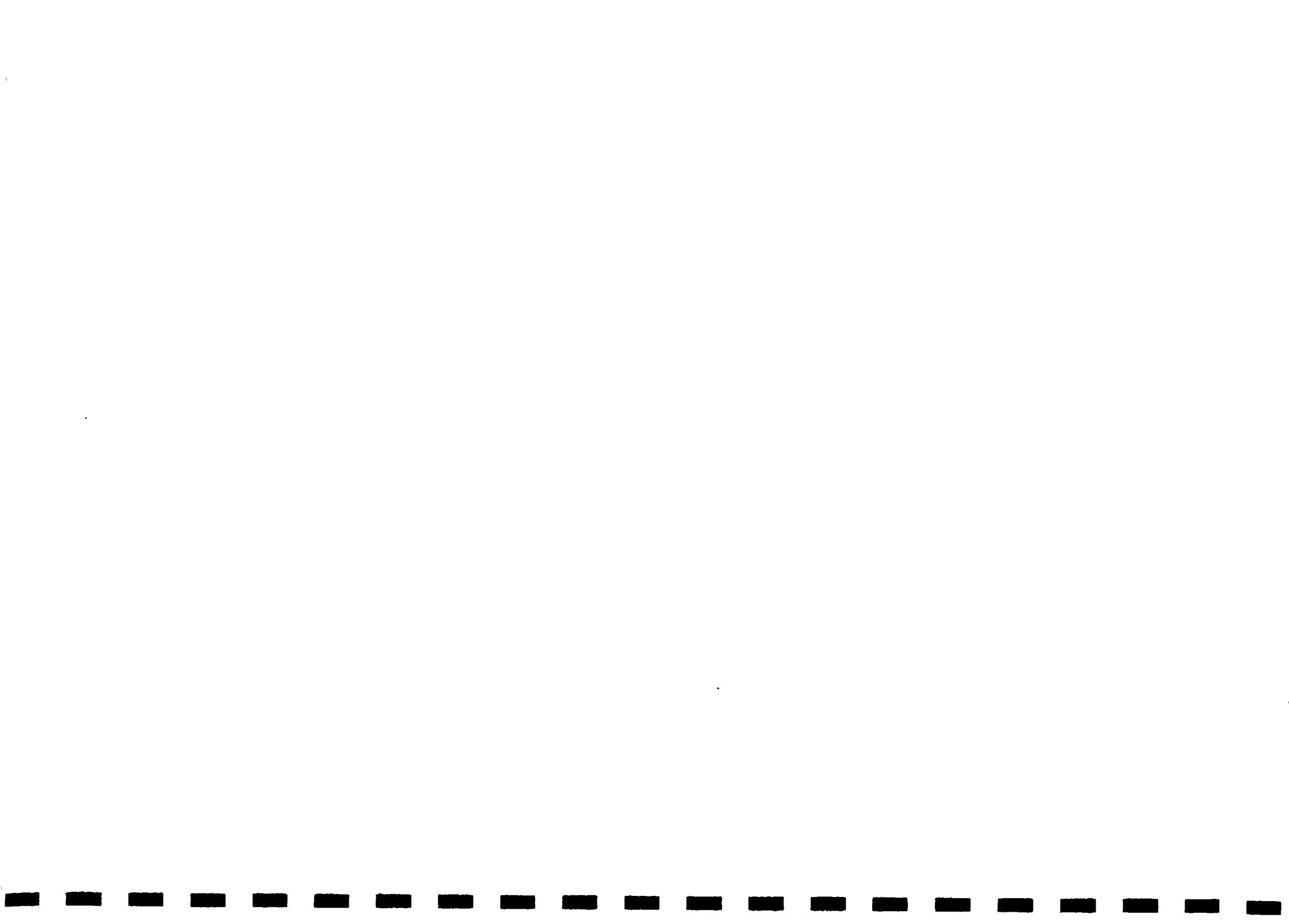
YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	192.0	347.4	272.0	203.9	112.2	41.3	191.0	22.0	187.4	150.1	143.0	151.7	2102.4
1961	176.1	100.8	191.2	281.1	262.1	177.5	40.6	138.4	17.5	329.7	593.7	201.6	2813.3
1962	149.3	152.3	174.5	330.9	320.4	63.0	203.6	100.1	166.1	100.1	239.5	163.6	2211.2
1963	327.2	152.3	207.9	458.9	121.7	245.7	139.4	60.9	93.6	218.1	537.0	332.5	2891.0
1964	149.3	124.0	223.2	195.2	129.4	113.2	180.7	48.0	143.9	134.6	132.4	206.3	1781.1
1965	23.6	100.2	170.5	410.1	332.7	64.0	19.2	125.2	122.0	235.2	396.2	307.5	2301.5
1966	184.3	60.2	168.4	434.7	13.9	41.2	36.2	38.4	308.5	380.9	276.7	232.2	2228.4
1967	167.1	142.2	207.9	150.9	121.7	173.4	36.1	60.2	20.0	451.4	608.3	161.8	2617.0
1968	2.4	0.0	134.0	164.4	68.9	247.1	202.8	-	-	-	-	639.6	639.6
1969	-	-	-	-	-	113.8	-	-	-	-	-	113.8	113.8
1970	-	-	-	-	-	-	-	-	-	-	-	831.7	831.7
1971	361.5	169.3	223.2	367.7	154.5	161.0	77.9	294.8	411.1	290.6	357.0	239.1	2589.8
1972	-	-	-	-	-	-	-	-	-	-	-	-	-
1973	54.6	29.1	287.9	165.0	64.0	141.7	30.1	120.3	30.2	365.4	280.7	367.1	1941.1
1974	0.0	236.0	241.5	397.9	104.4	164.5	175.6	151.7	211.6	53.9	253.0	411.9	2403.0
1975	72.1	167.3	367.5	503.8	200.2	489.2	40.8	179.9	140.7	122.9	499.1	197.9	3001.2
1976	37.8	55.8	167.5	273.4	173.3	7.6	26.0	81.0	22.7	-	-	-	845.1
1977	-	-	-	-	-	-	-	-	-	-	-	-	-
1978	29.8	55.8	23.0	92.0	350.0	7.6	50.0	162.0	170.0	240.0	366.0	77.0	1014.8
1979	167.2	60.0	18.2	269.5	473.0	95.4	153.9	27.7	404.5	617.5	490.2	232.0	3007.1
1980	10.0	33.5	85.7	333.3	151.6	70.1	60.0	71.8	113.5	140.6	523.0	183.5	1791.5
1981	103.0	74.6	102.1	159.9	473.0	163.1	7.6	-	-	-	-	1083.3	-
1982	-	-	-	-	-	-	-	-	-	-	-	-	-
1983	20.0	57.5	18.0	200.9	341.3	39.1	30.5	55.0	83.4	258.2	281.6	282.5	1662.0
1984	292.8	164.3	701.5	403.7	62.0	142.0	124.0	43.0	172.0	196.3	189.4	206.9	3042.2
1985	85.9	123.1	291.7	244.7	124.0	51.0	31.1	21.4	107.1	513.3	362.0	365.4	3081.5
1986	135.2	65.0	172.0	662.8	16.1	91.9	58.5	141.1	217.6	168.1	123.5	178.1	2021.9
1987	105.1	55.5	175.6	135.1	312.8	10.1	0.0	129.8	105.0	272.2	410.0	220.9	2109.1
1988	67.0	160.8	436.4	458.5	127.8	141.6	210.1	66.5	222.5	208.3	252.7	255.6	2611.6
AVERAGE	121.8	115.3	211.0	320.3	206.4	147.6	89.6	97.0	152.2	273.2	384.6	231.1	2351.7
STD.DEV.	99.3	76.6	142.5	136.8	125.2	71.4	61.5	112.3	144.0	163.3	79.5	79.4	3081.8
MAXIMUM	361.5	347.4	701.5	662.8	473.0	511.0	210.1	294.8	411.1	617.5	701.0	411.9	3081.5
MINIMUM	0.0	0.0	92.0	13.9	7.6	0.0	21.4	0.0	53.9	123.5	77.0	77.0	113.8



RAINFALL ANALYSIS

STATION : THIRAGODA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	106.7	149.8	67.3	136.6	174.7	123.6	173.1	111.5	140.2	120.9	171.1	68.8	1546.8
1961	59.6	60.7	94.2	105.1	401.3	117.8	201.9	423.4	416.5	518.6	152.4	78.2	1709.7
1962	98.5	0.0	64.7	103.6	389.6	150.6	152.1	187.1	122.4	133.0	240.7	351.5	1995.3
1963	137.1	85.3	41.9	126.4	232.1	175.1	211.8	361.7	510.5	405.3	245.3	122.4	2674.9
1964	33.0	108.2	30.7	54.3	249.1	189.9	68.5	173.9	298.9	264.4	210.8	24.4	1703.8
1965	20.3	62.9	12.9	141.7	258.6	50.8	37.5	171.1	356.6	368.8	138.6	270.0	1893.2
1966	29.9	36.0	5.3	262.3	43.1	56.3	59.6	147.6	316.6	204.4	185.6	116.3	1461.5
1967	68.3	30.4	10.1	25.3	167.6	141.1	101.8	117.6	166.6	137.3	187.9	84.6	1689.0
1968	226.8	0.0	72.1	43.1	60.4	265.9	127.5	142.9	26.9	27.9	35.6	20.5	951.8
1969	30.4	28.4	0.0	18.0	248.1	32.0	9.9	257.8	23.3	209.6	212.3	500.6	1870.8
1970	12.9	5.0	12.4	157.4	6.6	55.8	169.6	147.8	179.9	141.7	147.0	84.5	933.0
1971	81.7	25.9	20.3	41.1	93.9	65.0	155.4	25.9	88.6	186.9	161.0	145.0	1091.0
1972	223.2	31.4	124.7	69.9	289.6	149.3	90.9	90.6	342.1	235.2	342.1	40.8	2050.0
1973	41.4	100.4	27.1	254.7	393.4	336.5	205.6	208.1	382.7	124.4	367.2	2608.9	1879.1
1974	0.0	19.3	21.0	267.2	126.7	151.6	238.6	418.3	111.2	54.6	148.6	2262.0	2094.0
1975	45.4	60.5	96.5	256.0	336.6	309.6	75.6	153.1	156.9	361.9	22.0	588.2	324.3
1976	27.6	12.1	128.2	129.2	175.7	57.4	102.8	131.5	276.4	395.0	185.9	352.0	1867.3
1977	12.4	40.6	168.6	168.2	250.9	125.2	62.4	175.0	185.9	352.0	148.3	2356.5	2094.0
1978	101.0	15.4	265.7	192.0	540.7	151.3	95.5	292.6	148.6	379.6	148.3	106.6	2344.8
1979	20.0	170.4	67.5	193.9	260.3	201.6	264.1	58.1	493.7	80.5	397.2	198.1	1822.3
1980	7.1	56.1	9.9	268.9	110.1	106.6	94.0	70.6	108.1	283.4	435.6	185.9	1660.1
1981	40.4	55.4	33.0	171.2	313.2	59.7	49.8	162.8	237.2	33.0	150.6	131.8	1460.1
1982	6.0	0.0	83.6	222.0	182.9	162.9	276.4	29.2	134.4	568.0	816.9	137.9	2739.5
1983	65.0	0.0	20.6	67.3	88.6	178.3	134.9	166.9	310.1	10.6	178.6	157.5	1940.8
1984	240.8	169.4	69.1	246.4	372.4	288.5	0.0	68.9	103.6	236.7	56.4	2062.0	1879.1
1985	37.3	65.0	129.9	135.6	360.9	432.0	77.2	314.7	121.4	389.2	247.9	148.9	2461.0
1986	110.2	80.8	126.2	117.1	176.3	33.5	15.7	42.9	217.7	233.7	220.7	125.7	1502.5
1987	53.5	51.1	43.7	136.4	104.1	128.5	6.3	42.9	187.3	393.9	306.1	79.8	1931.0
1988	42.3	46.5	107.2	113.3	157.8	318.1	300.5	351.5	252.0	22.1	180.3	60.4	1982.1
1989	46.7	0.9	1.9	77.3	141.2	246.2	326.6	242.6	183.7	255.8	414.7	37.1	1978.7
AVERAGE	67.5	53.0	77.9	126.4	232.1	175.1	146.6	169.6	206.1	246.4	250.0	145.0	1895.7
STAND. DEV.	64.1	47.7	71.3	75.3	114.1	122.8	98.8	119.9	130.9	151.8	130.2	112.0	167.8
MAXIMUM	240.8	170.4	205.7	268.4	540.7	606.2	336.5	429.5	610.5	585.0	588.2	500.6	2739.5
MINIMUM	0.0	0.0	0.0	12.4	43.1	6.6	6.3	0.0	14.7	22.1	35.6	20.5	933.0
YEAR	TOTAL	RANK	PROBABILITY	10 Year Moving Average	Year	Year	Year	Year	Year	Year	Year	Year	Year
1970	933.0	1	0.03226	60 - 69	60	61 - 70	61	62 - 71	62	63 - 72	63	64 - 73	64
1968	951.8	2	0.06452	70 - 79	70	71 - 79	71	72 - 80	72	73 - 80	73	74 - 80	74
1971	1091.0	3	0.09677	80 - 89	80	81 - 89	81	82 - 90	82	83 - 90	83	84 - 90	84
1983	1340.8	4	0.12903	90 - 99	90	91 - 99	91	92 - 100	92	93 - 100	93	94 - 100	94
1966	1461.5	5	0.16129	0 - 9	0	1 - 9	1	2 - 9	2	3 - 9	3	4 - 9	4
1981	1468.1	6	0.19355	10 - 19	10	11 - 19	11	12 - 19	12	13 - 19	13	14 - 19	14
1986	1502.5	7	0.22581	20 - 29	20	21 - 29	21	22 - 29	22	23 - 29	23	24 - 29	24
1960	1546.8	8	0.25006	30 - 39	30	31 - 39	31	32 - 39	32	33 - 39	33	34 - 39	34
1969	1570.6	9	0.29032	40 - 49	40	41 - 49	41	42 - 49	42	43 - 49	43	44 - 49	44
1967	1589.0	10	0.32258	50 - 59	50	51 - 59	51	52 - 59	52	53 - 59	53	54 - 59	54
1964	1703.8	11	0.35484	60 - 69	60	61 - 69	61	62 - 69	62	63 - 69	63	64 - 69	64
1980	1822.3	12	0.38710	70 - 79	70	71 - 79	71	72 - 79	72	73 - 79	73	74 - 79	74
1977	1867.3	13	0.41935	80 - 89	80	81 - 89	81	82 - 89	82	83 - 89	83	84 - 89	84
1974	1879.1	14	0.45161	90 - 99	90	91 - 99	91	92 - 99	92	93 - 99	93	94 - 99	94
1985	1893.2	15	0.48387	100 - 109	100	101 - 109	101	102 - 109	102	103 - 109	103	104 - 109	104
1987	1931.0	16	0.51613	110 - 119	110	111 - 119	111	112 - 119	112	113 - 119	113	114 - 119	114
1976	2094.2	22	0.54746	120 - 129	120	121 - 129	121	122 - 129	122	123 - 129	123	124 - 129	124
1975	2262.0	23	0.57494	130 - 139	130	131 - 139	131	132 - 139	132	133 - 139	133	134 - 139	134
1979	2344.8	24	0.67419	140 - 149	140	141 - 149	141	142 - 149	142	143 - 149	143	144 - 149	144
1978	2356.5	25	0.80645	150 - 159	150	151 - 159	151	152 - 159	152	153 - 159	153	154 - 159	154
1985	2461.0	26	0.83871	160 - 169	160	161 - 169	161	162 - 169	162	163 - 169	163	164 - 169	164
1984	2062.0	27	0.64516	170 - 179	170	171 - 179	171	172 - 179	172	173 - 179	173	174 - 179	174
1976	2094.2	28	0.67742	180 - 189	180	181 - 189	181	182 - 189	182	183 - 189	183	184 - 189	184
1961	2174.9	29	0.80323	190 - 199	190	191 - 199	191	192 - 199	192	193 - 199	193	194 - 199	194
1963	2274.6	30	0.93548	200 - 209	200	201 - 209	201	202 - 209	202	203 - 209	203	204 - 209	204
1982	2739.5	31	0.96774	210 - 219	210	211 - 219	211	212 - 219	212	213 - 219	213	214 - 219	214



RAINFALL ANALYSIS

STATION : MAWARELLA ESTATE

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	289.0	210.3	147.0	271.7	286.2	136.9	315.9	113.0	260.0	232.1	233.6	51.3	2548.6
1961	199.6	110.7	218.4	143.2	367.5	169.9	266.4	371.6	425.1	338.5	345.9	270.2	3229.0
1962	121.1	73.6	178.5	219.9	367.2	166.6	119.3	212.0	290.5	216.6	405.1	107.4	2777.8
1963	231.6	160.2	179.5	451.3	315.9	6.0	279.4	332.4	543.5	557.7	355.0	179.6	3593.1
1964	140.2	158.7	146.3	281.4	374.3	197.3	331.4	147.5	260.4	96.2	230.1	295.6	2679.1
1965	15.2	103.8	190.5	165.8	451.8	209.5	67.3	257.3	471.4	419.3	556.7	358.3	3266.9
1966	166.3	73.1	236.9	396.2	74.4	121.1	93.2	197.3	660.4	637.7	250.4	318.2	3225.2
1967	289.3	59.6	151.3	210.3	189.4	338.0	386.0	199.8	192.5	615.6	530.3	169.9	3332.8
1968	845.8	45.9	266.4	90.1	181.6	386.5	424.1	99.3	196.3	194.5	100.3	250.9	2781.9
1969	27.1	91.1	137.6	116.8	668.6	212.5	48.0	306.3	164.3	324.1	494.0	840.9	3433.2
1970	169.1	143.2	256.0	261.6	224.5	281.4	175.0	185.4	163.3	166.8	381.7	216.9	2924.9
1971	281.4	227.8	323.5	458.9	230.1	267.4	226.0	172.7	455.5	383.7	341.1	205.9	3573.9
1972	118.5	4.8	258.5	232.4	616.2	100.5	107.4	165.6	536.4	577.5	403.8	160.7	3299.3
1973	27.4	151.3	353.3	291.0	201.1	462.2	151.8	160.2	160.5	564.1	303.7	556.7	3303.3
1974	0.0	168.9	157.2	397.0	297.1	247.6	300.9	190.5	417.0	123.1	254.7	249.6	2741.4
1975	119.1	256.3	337.5	420.9	426.2	512.0	78.4	190.5	167.6	496.0	600.7	470.9	4076.0
1976	150.1	96.7	229.6	387.6	295.4	114.5	205.2	157.9	10.9	387.6	572.0	273.0	2680.5
1977	7.6	123.4	305.0	291.5	421.6	230.1	176.0	208.5	158.2	524.5	426.2	372.8	3247.4
1978	235.1	136.8	342.9	175.6	847.1	132.0	158.5	230.6	190.5	259.3	521.2	102.1	3132.4
1979	70.8	156.2	56.6	457.2	255.2	200.9	209.5	45.4	189.7	353.8	456.1	237.2	2986.6
1980	22.0	65.8	47.2	378.2	298.1	202.6	103.6	138.1	100.3	334.0	567.1	174.2	2421.6
1981	87.9	169.4	136.6	223.8	298.3	197.0	60.6	64.3	260.8	210.4	491.4	145.7	2364.2
1982	72.9	90.2	301.6	352.7	408.3	615.0	181.3	173.2	200.8	513.3	665.0	190.0	3762.5
1983	145.2	14.3	145.0	19.0	112.2	196.9	116.7	231.8	412.3	115.7	358.1	669.8	2640.8
1984	142.3	203.9	292.8	326.8	380.3	318.0	214.0	3.1	187.9	251.8	479.1	117.6	3247.7
1985	215.3	130.9	242.1	257.7	326.7	760.0	198.8	223.8	591.3	250.4	323.8	3706.8	2741.8
1986	169.5	132.0	246.1	437.0	128.5	139.2	117.4	208.7	169.1	308.0	198.7	210.3	2693.6
1987	167.9	33.2	309.2	229.9	231.0	133.4	2.3	452.5	235.0	634.7	275.0	169.3	3296.1
1988	171.4	149.6	202.7	342.6	350.9	238.7	203.4	337.3	369.9	187.4	506.0	167.7	2174.4
1989	49.2	39.9	202.7	75.4	236.7	356.4	297.8	266.3	57.3	187.6	363.6	39.5	
AVERAGE	159.8	119.2	222.3	276.8	321.7	255.1	187.2	202.0	291.7	370.1	397.3	273.2	3076.4
STAND.DEV.	125.7	62.4	80.2	118.1	142.0	158.1	101.6	92.5	150.6	167.4	135.6	173.0	412.5
MAXIMUM	545.8	258.3	353.3	458.9	668.5	760.0	424.1	452.1	60.4	637.7	840.9	4078.0	4078.0
MINIMUM	0.0	4.8	45.2	19.0	74.4	6.8	2.3	3.1	10.9	96.2	100.3	39.5	2174.4

10 Year Rolling Average

YEAR	TOTAL	RANK	PROBABILITY	10 Year Rolling Average
1989	2174.1	1	0.03226	60 - 69
1981	2364.2	2	0.06452	61 - 70
1980	2421.5	3	0.09677	62 - 71
1983	2540.8	4	0.12903	63 - 72
1960	2548.6	5	0.16129	64 - 73
1964	2679.1	6	0.19355	65 - 74
1974	2744.1	7	0.22581	66 - 75
1986	2764.6	8	0.25806	67 - 76
1962	2777.8	9	0.29032	68 - 77
1978	2781.9	10	0.32258	69 - 78
1976	2880.5	11	0.35404	70 - 79
1987	2893.6	12	0.38710	71 - 80
1970	2924.9	13	0.41935	72 - 81
1979	2988.6	14	0.45161	73 - 82
1988	3296.1	15	0.48387	74 - 83
1972	3299.3	16	0.51613	75 - 84
1961	3225.2	17	0.54039	76 - 85
1977	3247.1	18	0.58065	77 - 86
1984	3247.7	19	0.61290	78 - 87
1969	3433.2	20	0.64516	79 - 88
1971	3573.9	21	0.67742	80 - 89
1963	3593.1	22	0.70969	
1985	3332.8	23	0.74194	
1982	3762.5	24	0.77419	
1975	3383.3	25	0.80645	
1971	3286.9	26	0.83871	
1972	3296.1	27	0.87097	
1963	3593.1	28	0.90323	
1985	3706.8	29	0.93548	
1975	4078.0	30	0.96774	

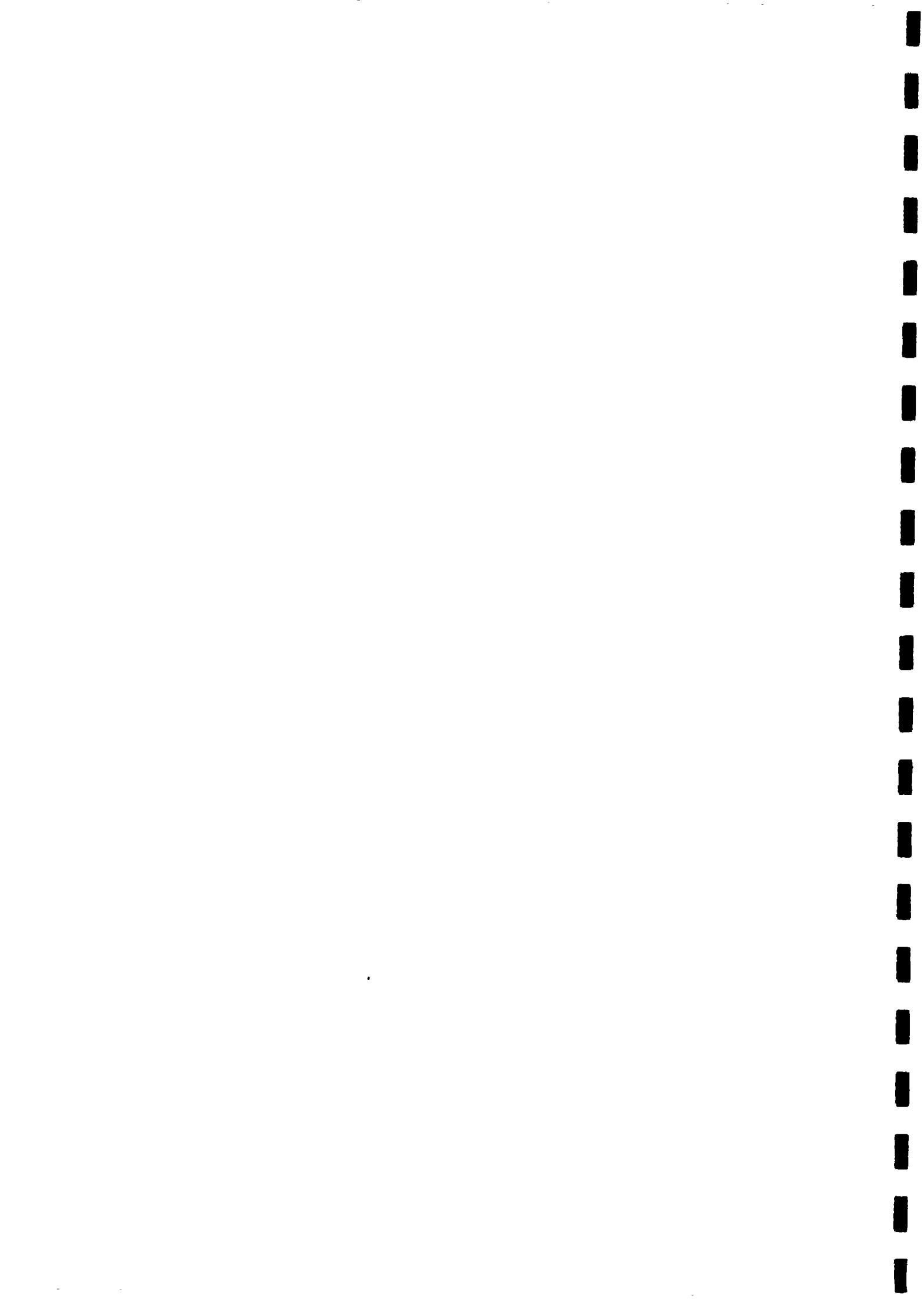


RAINFALL ANALYSIS

STATION NAME: KEKENADORA

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1960	114.5	101.3	103.1	62.9	165.6	106.1	157.1	92.9	71.6	147.3	112.7	26.9	1262.3
1961	154.0	37.6	41.9	52.8	320.5	100.0	87.6	436.1	367.0	457.2	128.7	87.1	2285.9
1962	183.5	6.0	65.7	84.3	338.3	124.7	202.1	209.5	141.9	61.4	182.1	127.5	1627.0
1963	157.4	18.7	25.4	73.1	526.2	129.0	212.9	218.4	364.7	104.3	239.7	313.9	340.9
1964	48.2	66.2	68.3	34.5	217.6	218.4	364.7	104.3	239.7	313.9	210.9	52.3	2979.2
1965	0.0	69.9	14.9	85.8	256.2	111.5	76.2	296.9	340.1	400.5	306.8	323.8	1936.9
1966	19.0	18.2	108.9	78.7	86.6	82.8	142.4	243.0	383.0	158.4	136.6	2272.6	2272.6
1967	199.8	43.1	0.0	69.3	228.0	220.2	220.9	163.8	191.0	418.8	265.4	51.3	1790.3
1968	216.6	57.6	53.5	32.0	189.2	365.5	219.9	54.6	118.3	144.5	145.5	87.6	2072.4
1969	29.9	63.5	33.7	61.2	398.2	97.6	210.0	284.7	83.3	213.6	214.6	590.2	1632.6
1970	17.7	101.6	212.5	200.6	424.9	36.8	84.5	116.8	26.2	154.4	172.2	109.4	2064.1
1971	358.9	2.5	227.0	191.2	115.8	170.6	72.3	230.1	253.7	260.0	151.1	241.3	1707.6
1972	17.0	30.4	86.1	38.6	338.5	71.8	66.8	76.9	275.0	303.5	280.0	14.7	1582.3
1973	57.4	60.1	112.2	64.1	187.1	323.8	188.4	53.9	149.6	294.1	153.1	191.5	1835.4
1974	0.0	20.6	31.9	176.7	281.9	146.0	209.2	100.8	303.0	26.6	102.1	87.8	1886.4
1975	61.5	122.9	121.6	194.5	211.6	206.2	31.7	80.7	75.1	232.9	239.0	96.7	1664.9
1976	8.0	0.0	10.4	124.2	94.2	74.6	110.3	130.8	3.5	234.1	179.0	181.4	1462.3
1977	0.0	31.4	91.9	56.1	270.0	132.3	115.0	119.8	310.1	185.6	27.6	1429.1	2275.5
1978	13.9	195.5	155.7	99.8	408.1	103.9	56.8	166.6	150.8	142.7	334.7	67.5	1895.2
1979	19.7	148.0	16.0	108.4	30.9	195.8	175.2	44.7	368.8	121.6	476.2	152.1	1886.4
1980	58.3	66.0	4.5	172.2	93.2	127.0	62.2	91.6	104.1	221.4	306.4	114.9	1494.5
1981	25.9	34.5	0.0	16.6	165.6	21.3	32.6	139.4	193.6	254.2	249.4	104.9	1239.4
1982	325.2	188.4	130.3	121.9	179.8	292.6	221.7	389.5	115.0	34.2	46.0	140.5	2105.9
1983	81.6	857.8	83.0	11.2	62.7	109.5	92.5	128.8	282.7	72.1	17.6	155.2	1155.7
1984	144.8	91.2	52.6	235.0	290.1	138.4	164.6	71.4	41.7	199.9	17.5	147.2	1217.2
1985	19.3	24.9	32.8	39.1	186.7	268.5	35.8	136.4	85.3	128.0	167.4	96.0	1733.8
1986	94.5	29.5	89.1	98.3	65.8	14.5	20.1	20.1	61.7	98.0	127.5	14.7	1193.2
1987	47.0	29.0	24.1	99.3	17.0	65.5	3.5	292.1	77.5	313.4	218.0	35.5	1999.1
1988	2.0	50.8	39.6	126.2	97.3	154.1	169.4	139.2	16.0	94.1	17.8	665.6	665.6
1989	64.8	25.4	17.8	26.2	95.5	90.9	45.0	79.5	55.4	62.8	99.6	12.7	1233.7

YEAR	TOTAL	RANK	PROBABILITY	10 YEAR MOVING AVERAGE
1989	655.6	1	0.03226	60 - 69
1986	733.8	2	0.08452	70 - 79
1988	999.1	3	0.09677	62 - 71
1983	1155.7	4	0.12903	63 - 72
1987	1193.2	5	0.16129	64 - 73
1985	1217.2	6	0.19355	65 - 74
1981	1239.4	7	0.22581	66 - 75
1960	1262.3	8	0.25806	67 - 76
1977	1429.1	9	0.29032	68 - 77
1984	1447.2	10	0.32250	69 - 78
1976	1462.3	11	0.35484	70 - 79
1974	1494.5	12	0.38710	71 - 80
1980	1499.6	13	0.41935	72 - 81
1972	1582.3	14	0.45161	73 - 82
1982	1627.0	15	0.48387	74 - 83
1968	1632.5	16	0.51613	75 - 84
1975	1664.9	17	0.54839	76 - 85
1970	1707.6	18	0.58065	77 - 86
1966	1790.3	19	0.61290	78 - 87
1967	2072.4	20	0.64516	79 - 88
1982	2185.4	21	0.67742	60 - 89
1965	2272.6	22	0.70968	0.93023
1971	2276.5	23	0.74194	0.93548
1964	2308.9	24	0.77419	0.96774
1969	2064.1	25	0.80645	0.96774
1973	1835.4	26	0.83871	0.96774
1978	1866.4	27	0.87097	0.96774
1971	2276.5	28	0.90323	0.96774
1963	2265.9	29	0.93548	0.96774
	2979.2	30		



KHAJURAHOS

SIRIUS I KINBOKUFT

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
1960	114.9	110.8	33.8	305.2	61.4	14.7	161.6	3.2	94.3	204.8	215.0	90.9	1191.6
1961	202.7	184.7	150.5	47.0	96.1	68.8	85.8	56.3	201.1	226.3	126.9	1505.8	
1962	216.3	94.9	167.9	21.3	28.5	20.4	113.2	103.5	375.9	160.3	177.8	1471.8	
1963	116.8	66.6	59.7	92.1	141.8	46.1	22.3	68.3	395.4	317.5	96.0	1171.6	
1964	216.3	96.4	141.8	151.6	65.5	52.2	92.6	43.8	93.4	68.6	78.2	1191.6	
1965	0.0	143.9	141.8	114.1	178.1	11.6	68.5	103.0	280.0	324.4	184.0	1612.0	
1966	68.5	216.4	287.7	2.5	9.1	13.1	20.0	216.9	291.6	90.7	143.1	1431.5	
1967	68.5	41.4	49.3	221.6	112.2	61.8	87.3	43.4	369.5	324.4	28.2	1684.0	
1968	321.4	0.0	115.7	69.0	105.0	74.4	66.2	7.5	36.0	5.7	198.6	66.4	1065.9
1969	2.7	5.5	197.9	224.5	170.0	93.3	0.7	222.6	102.2	367.3	202.5	598.7	2181.1
1970	167.4	84.7	69.9	176.2	75.3	11.3	32.8	22.7	16.1	42.1	293.7	198.6	1191.6
1971	192.3	38.3	60.1	155.8	142.4	62.4	84.3	31.9	23.5	305.2	141.4	279.6	1831.4
1972	0.0	61.7	63.6	90.3	92.5	39.2	52.1	40.0	109.8	73.5	104.9	105.8	873.7
1973	54.5	151.9	251.6	181.8	330.6	108.0	66.2	30.5	56.8	47.4	269.9	208.9	1771.0
1974	32.6	24.8	3.0	36.7	242.2	85.7	51	17.1	23.3	211.2	391.6	94.8	1113.0
1975	0.5	43.7	169.7	93.9	131.1	12.3	9.5	63.9	38.1	266.7	291.0	127.2	1429.6
1976	19.8	34.1	46.2	115.7	79.0	212.1	8.9	13.2	25.0	76.3	106.9	136.2	937.7
1977	2.0	107.2	2.3	202.3	129.5	31.8	19.8	3.3	94.4	88.6	318.2	280.5	1289.9
1978	0.8	2.0	42.8	210.9	16.3	25.6	10	53.6	118.3	555.8	290.5	1379.3	
1979	91.2	5.1	46.5	122.1	117.1	201.8	112.5	47.2	10.6	12.7	277.8	439.1	106.3
1980	0.0	0.0	22.7	43.5	52.0	6.1	6.1	23.2	13.2	87.3	132.5	265.4	1541.0
1981	64.3	155.2	183.8	114.2	52.3	24.1	391.1	8.5	13.2	87.3	291.3	129.5	1657.9
1982	84.7	54.9	253.6	44.2	154.0	145.6	4.7	18.4	135.0	264.6	223.9	1562.4	1513.1
1983	143.2	97.4	128.7	137.5	49.0	18.6	6.7	155.1	99.2	165.0	67.0	1001.3	1122.7
1984	66.6	14.1	187.4	28.2	28.8	11.3	0.0	111.5	101.1	265.2	57.0	54.5	1341.5
1985	67.7	40.9	149.5	177.7	82.5	63.6	50.2	37.7	79.9	187.3	314.8	123.1	1356.8
1986	66.9	122.4	152.8	111.9	44.4	54.9	41.2	71.8	191.8	243.6	160.1	303.8	
1987	68.6	72.8	67.7	38.4	76.6	43.5	45.9	111.4	121.5	114.8	114.8	114.8	
1988	181.7	253.6	320.6	145.6	391.1	222.8	216.9	395.4	555.8	555.8	318.1	318.1	



GOVT CHICKEN MESH DESIGN FOR RAIN WATER HARVESTING

Community Water Supply & Sanitation Project

Ministry of Housing, Construction & Public Utilities



CEMENT AND SAND
MIX 1:3

TWO LAYERS OF 1/2"
CHICKEN MESH

1700mm
100mm
100mm
20mm
700

DOWN PIPE FROM GUTTER

FLY PROOF NETTING

COVER MADE OF
G SHEETING

750mm
100mm

50 mm DIA
OVERFLOW PIPE

FLY PROOF
NETTING

SIPHONING PIPE
20 MM DIA

1:2.4 (3/4")
CONCRETE

1:3 PLASTER
20 mm THICK

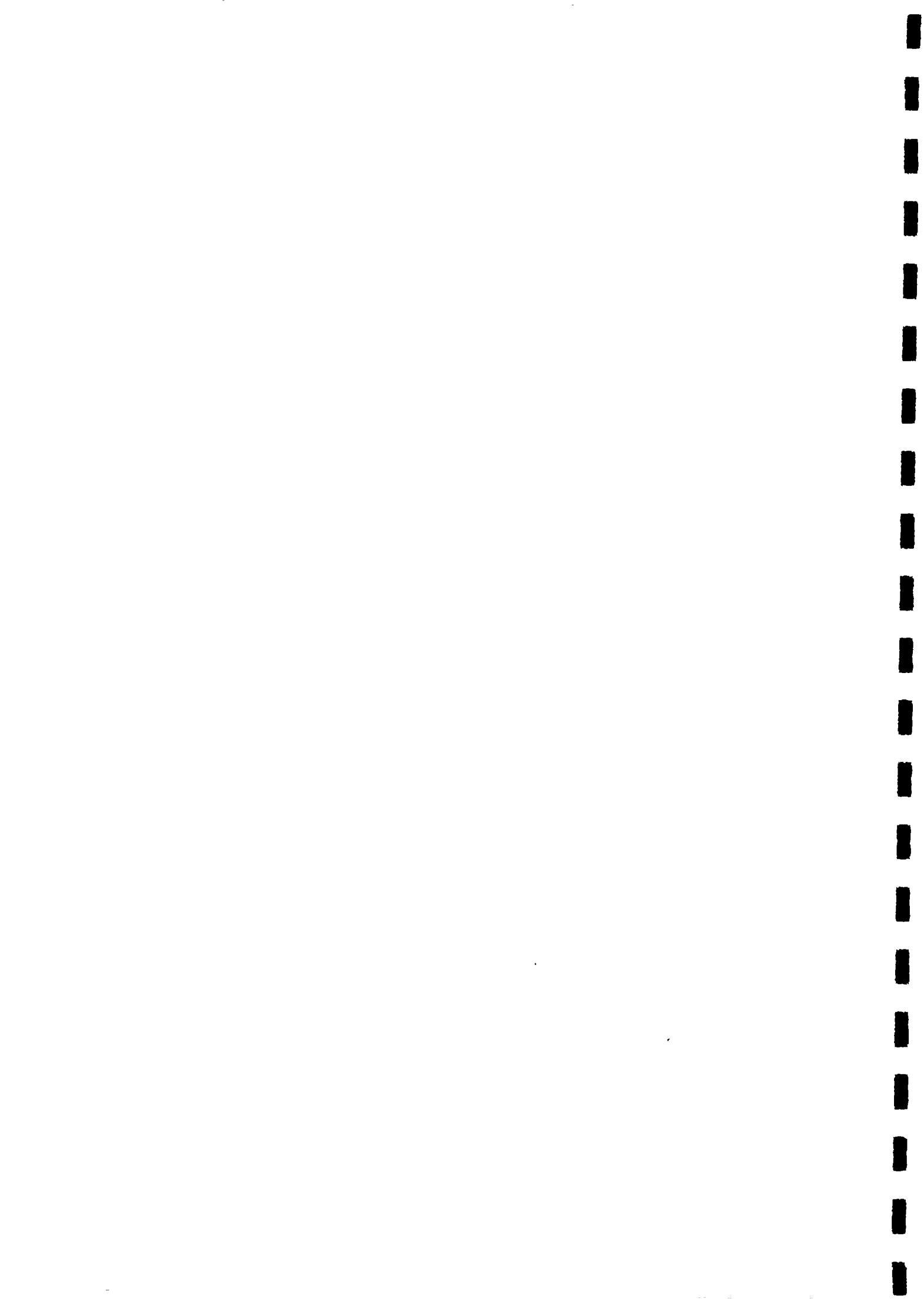
2150mm

1450mm

100

450mm

67



Annex - 4

5M³ RAIN WATER HARVESTING TANK – RATNAPURA DISTRICT (FERRO-CEMENT TYPE)

MAY 95

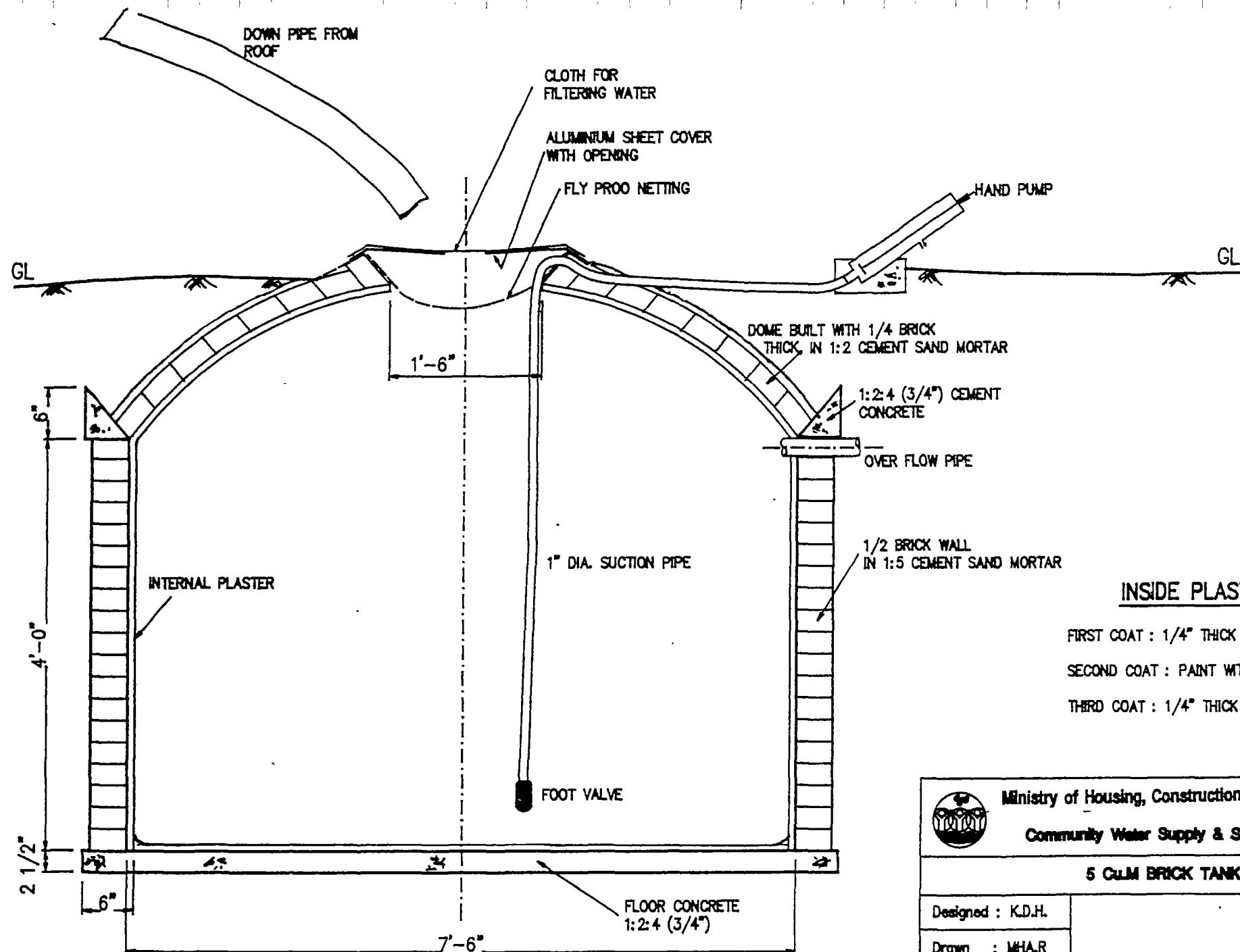
MAJOR COSTS (TRIAL CONSTRUCTION)

MATERIAL	UNIT	QTY	UNIT COST	COST	COST INTERNAL	COST EXTERNAL
CEMENT	Bag	8	265	2120		2120
SAND	ft ³	55	3.5	192.5		192.5
METAL	ft ³	6	18	108	54	54
1/2" CHICKEN MESH	ft ²	366	4	1464 3884		1464
MOULD				325		325
TRANSPORT				500	150	350
SKILLED LABOUR	HR	56	22	1232		1232
UNSKILLED LABOUR	HR	112	12.5	1400	1400	
				7341.5	1604	5737
					Contributions 22% HH	73% CWSSP

Cost of a liter

- Note:
- 1. Material + Skill Labour + Mould = 5441 1.09
 - Material + Skill Labour + Mould + Transport = 5941 1.19
 - Material + Skill Labour + Mould + Transport + Unskill Labour = 7342 1.47
 - 2. The mould is used for the construction of ten tanks. Total Cost of the mould is Rs. 3250/-.





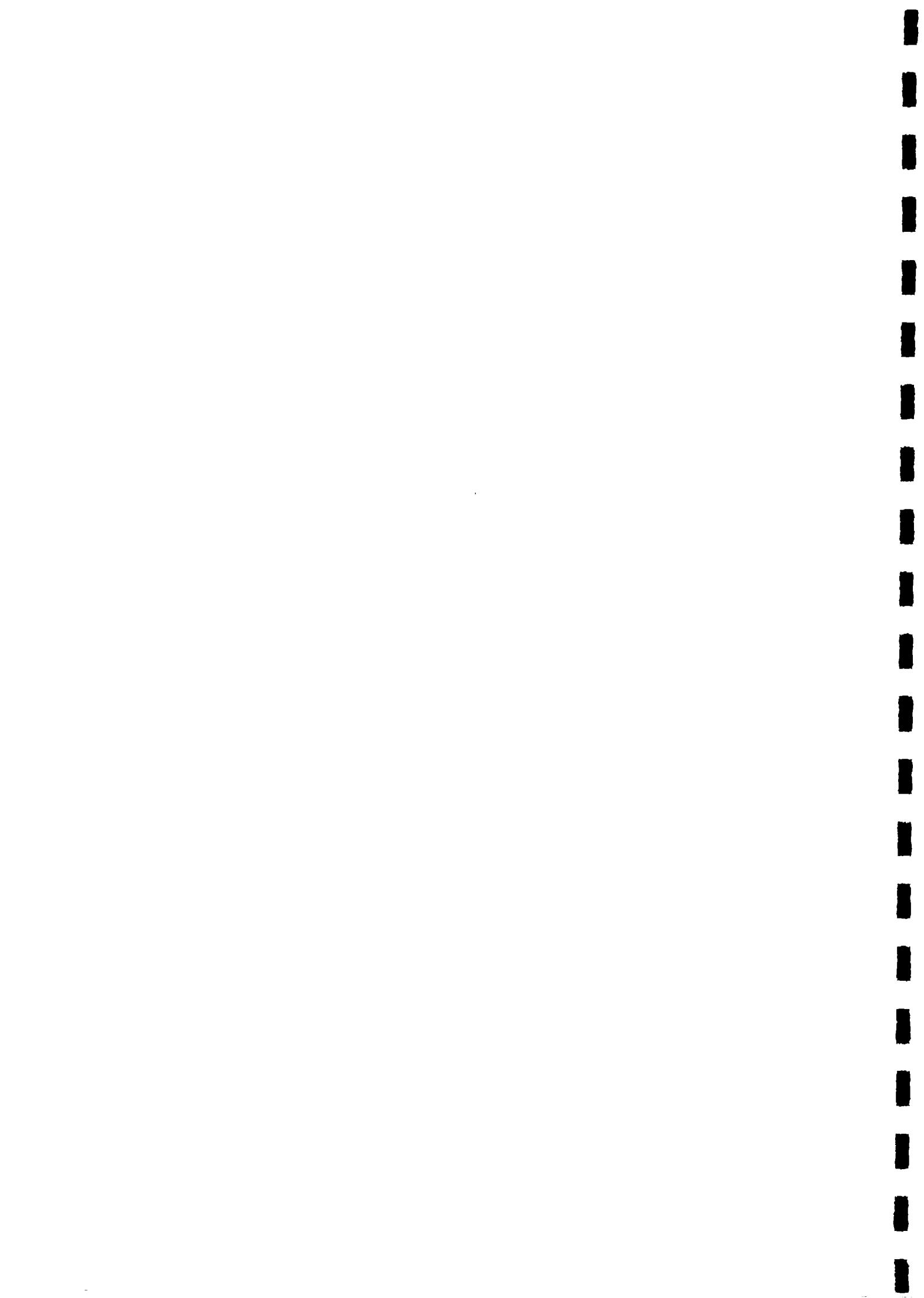
INSIDE PLASTERING

FIRST COAT : 1/4" THICK IN 1:3 CEMENT, SAND

SECOND COAT : PAINT WITH NEAT CEMENT SLURRY

THIRD COAT : 1/4" THICK IN 1:2 CEMENT, SAND

	Ministry of Housing, Construction & Public Utilities	
	Community Water Supply & Sanitation Project	
	5 Cu.M BRICK TANK	
	Designed : K.D.H.	
Drawn : M.H.A.R		
Scale : 1:15		
Date :		



Annex -- 6

RAIN WATER HARVESTING TANK Brick Dome Type Badulla District

February 1995

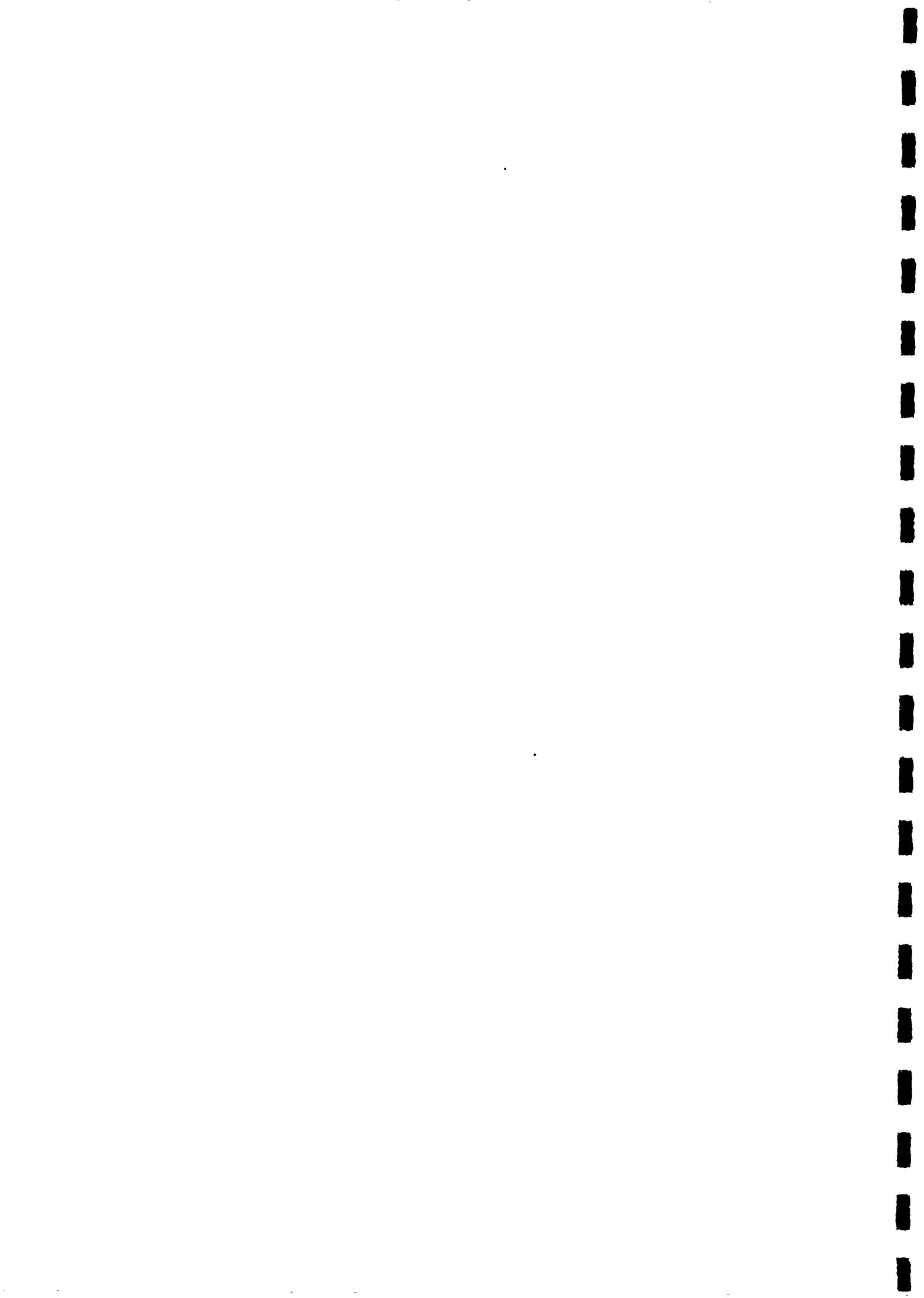
Size
5 m³
D = 6'4"
Hwall = 5'
Hdome = 1'6"

Material	Unit	Quantity	Unit Cost	Cost	Cost internal	Cost external
Cement	Bag	8.6	265	2279		2279
Sand	ft ³	33	3.5	115.5		115.5
Metal (3/4")	ft ³	9	18	162	81	81
Bricks (2")	nos.	750	1.5	1125		1125
				<u>3681.5</u>		
Transport				1000	300	700
Skilled labour	hour	28	22	616		616
Unskilled labour	hour	96	12.5	1200	<u>1200</u>	<u>1581</u>
						<u>4916.5</u>
Contributions						
					24% HH	76% CWSSP

Conclusion

Under normal circumstances a brick rainwater storage tank will be acceptable within the project criteria and will be affordable to the householder in terms of labour and cash

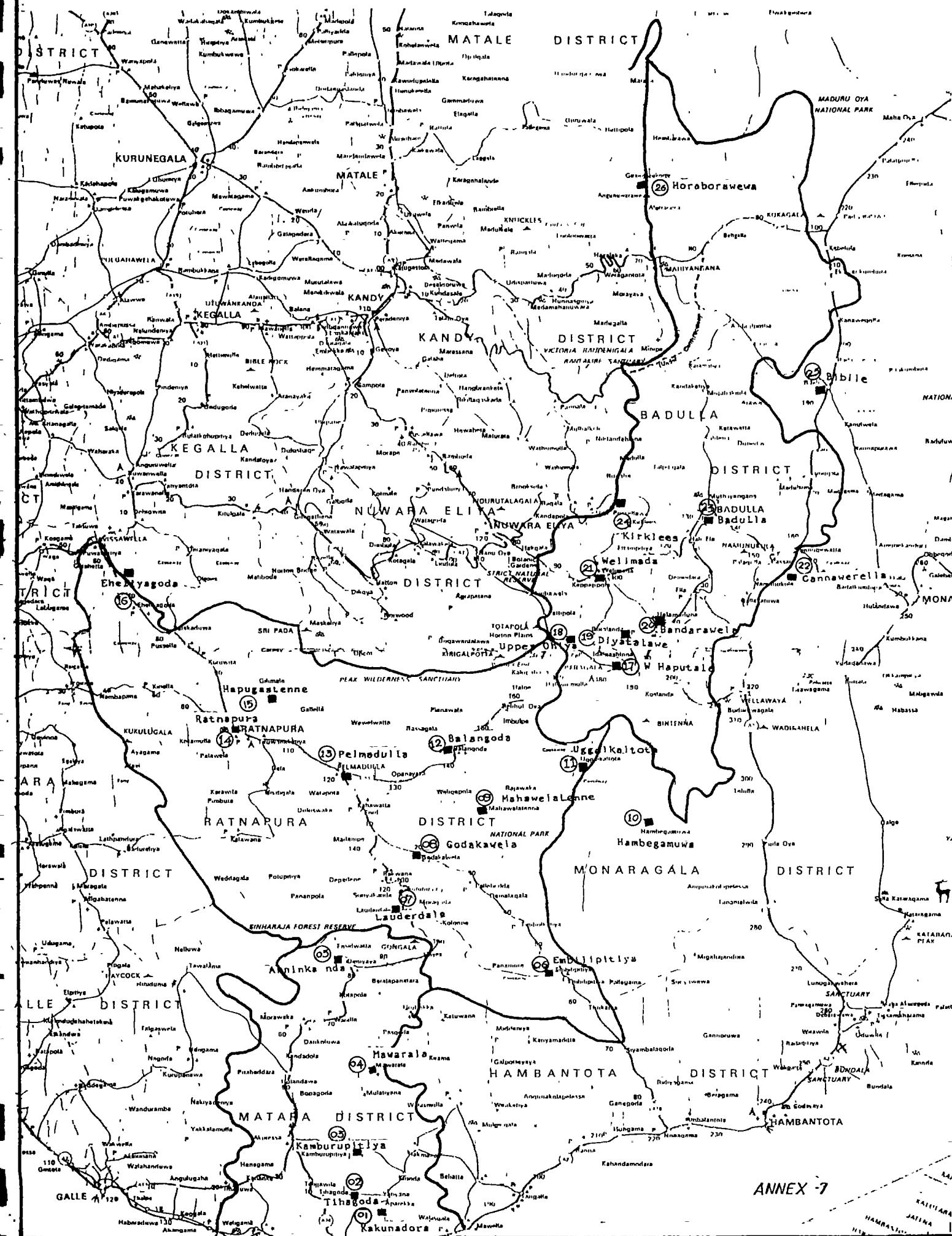
Material + skilled labour	Rs.	4297.5
Material + skilled labour + transport	Rs.	5297.5
Material + skilled labour +transport and unskilled labour	Rs.	6497.5



MAP SHOWING LOCATIONS OF RAINFALL STATIONS

S. A. Sequia Imperata
RESERVE

CATALOGUE





RAIN REGION GRAPH

BADULLA REGION

BADULLA DISTRICT

STORAGE REQUIRED (as % of AVG. ANNUAL SUPPLY)

80
40
20
0

10

30

50

70

90

DEMAND (as % of AVG. ANNUAL SUPPLY)

$$Y = 0.53X - 8.25$$
$$X = 1.89Y + 15.57$$

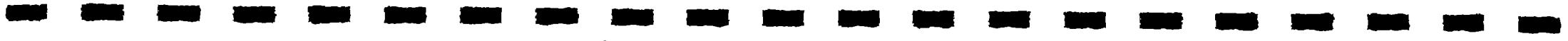
DATA USED

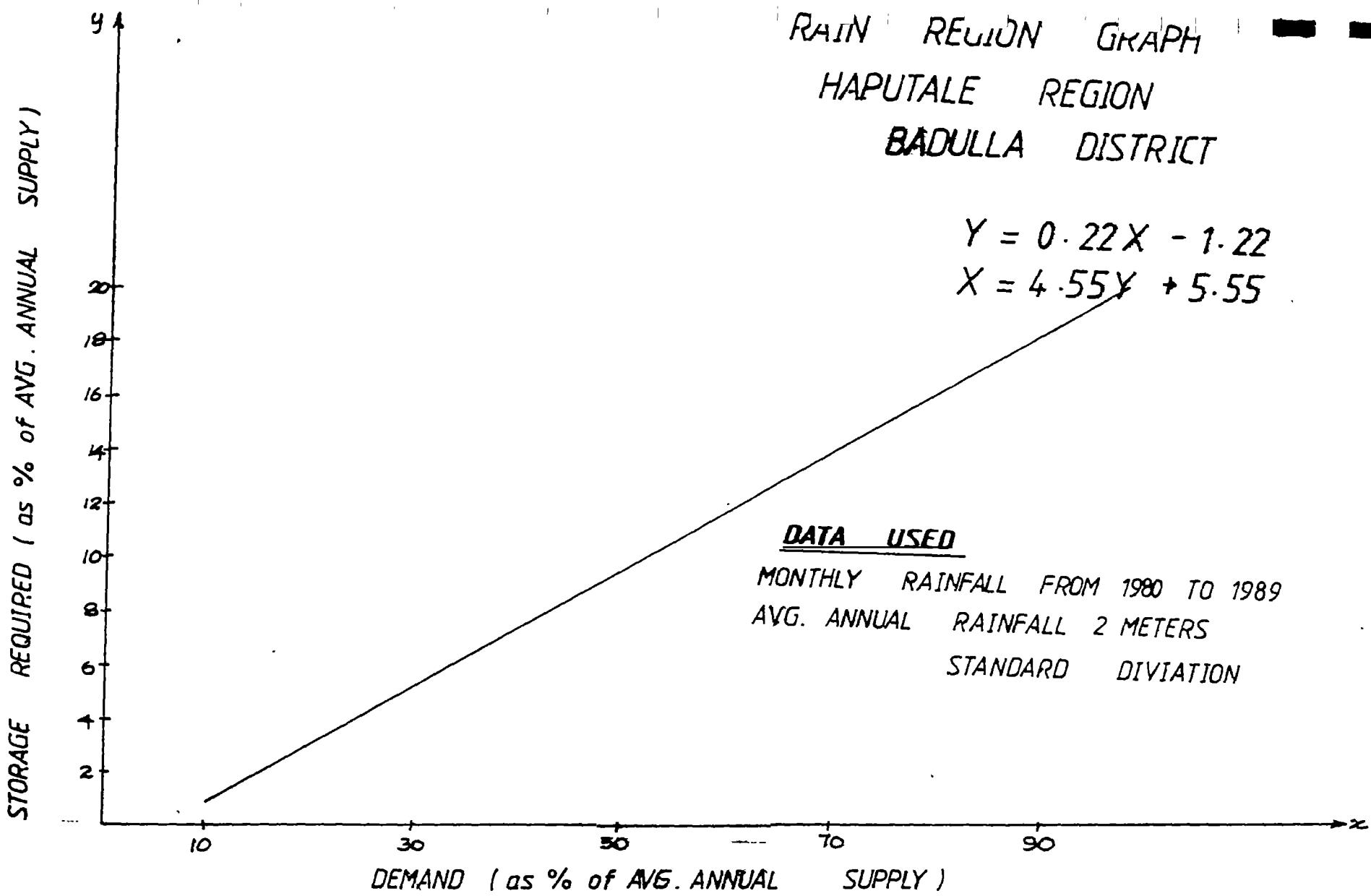
MONTHLY RAINFALL DATA

FROM 1985 TO 1994

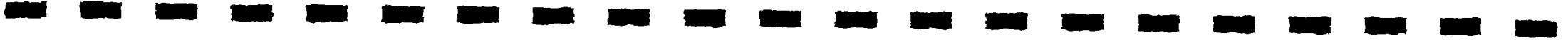
Avg. Annual Rainfall 1.75 Meters

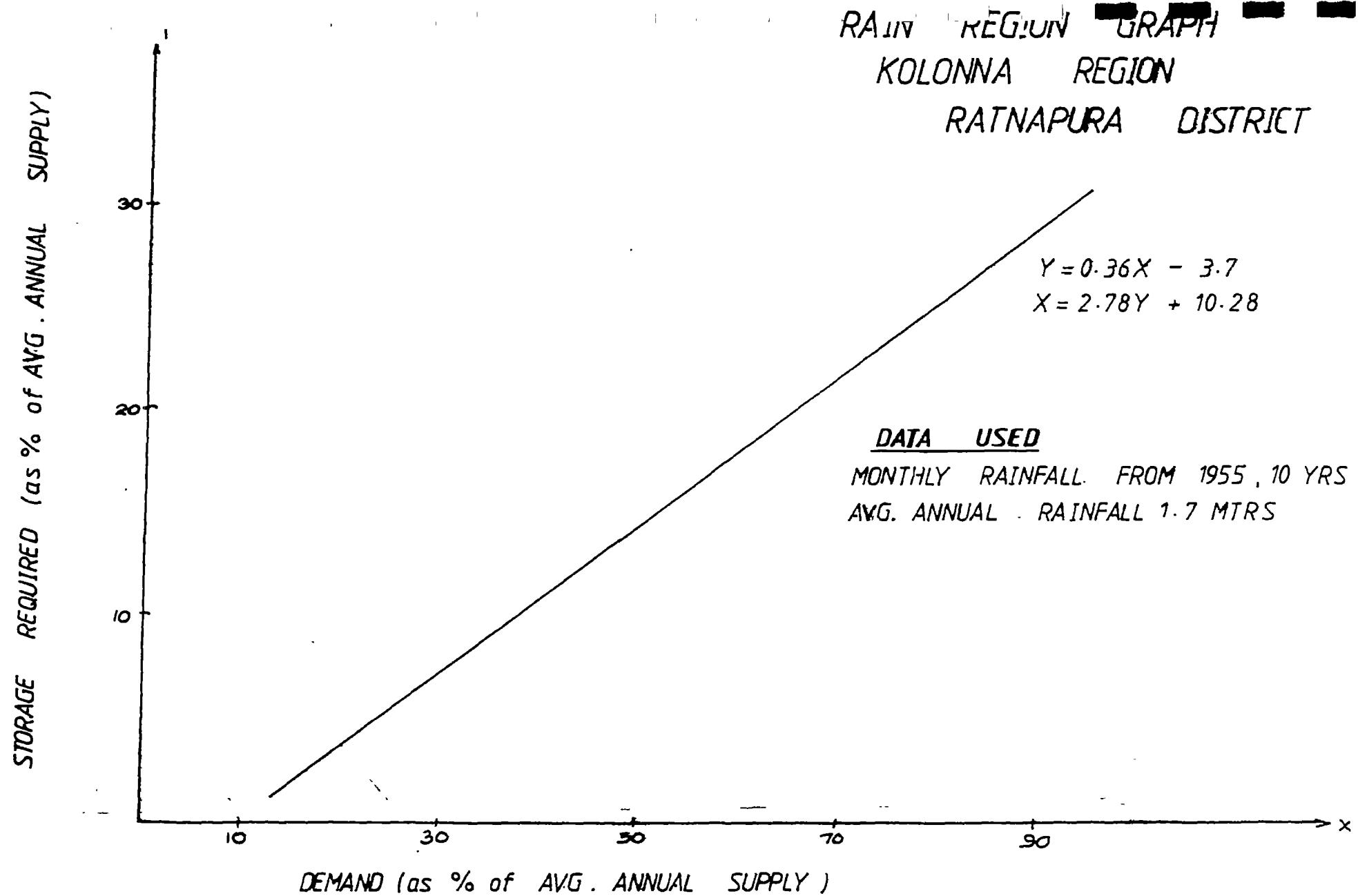
GRAPH - A
ANNEX - 8





GRAPH - B
ANNEX - 8

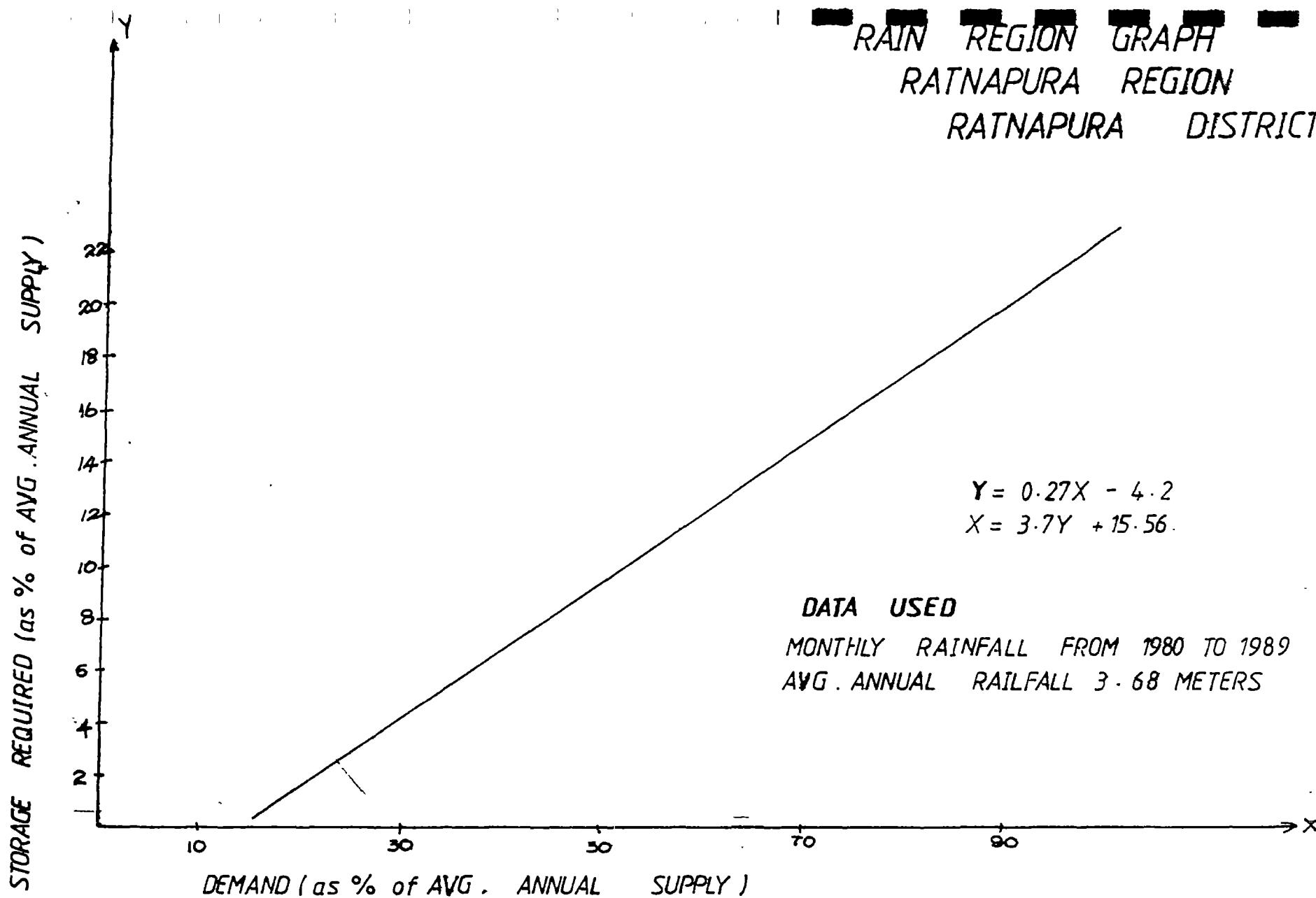




GRAPH - C
ANNEX - 8



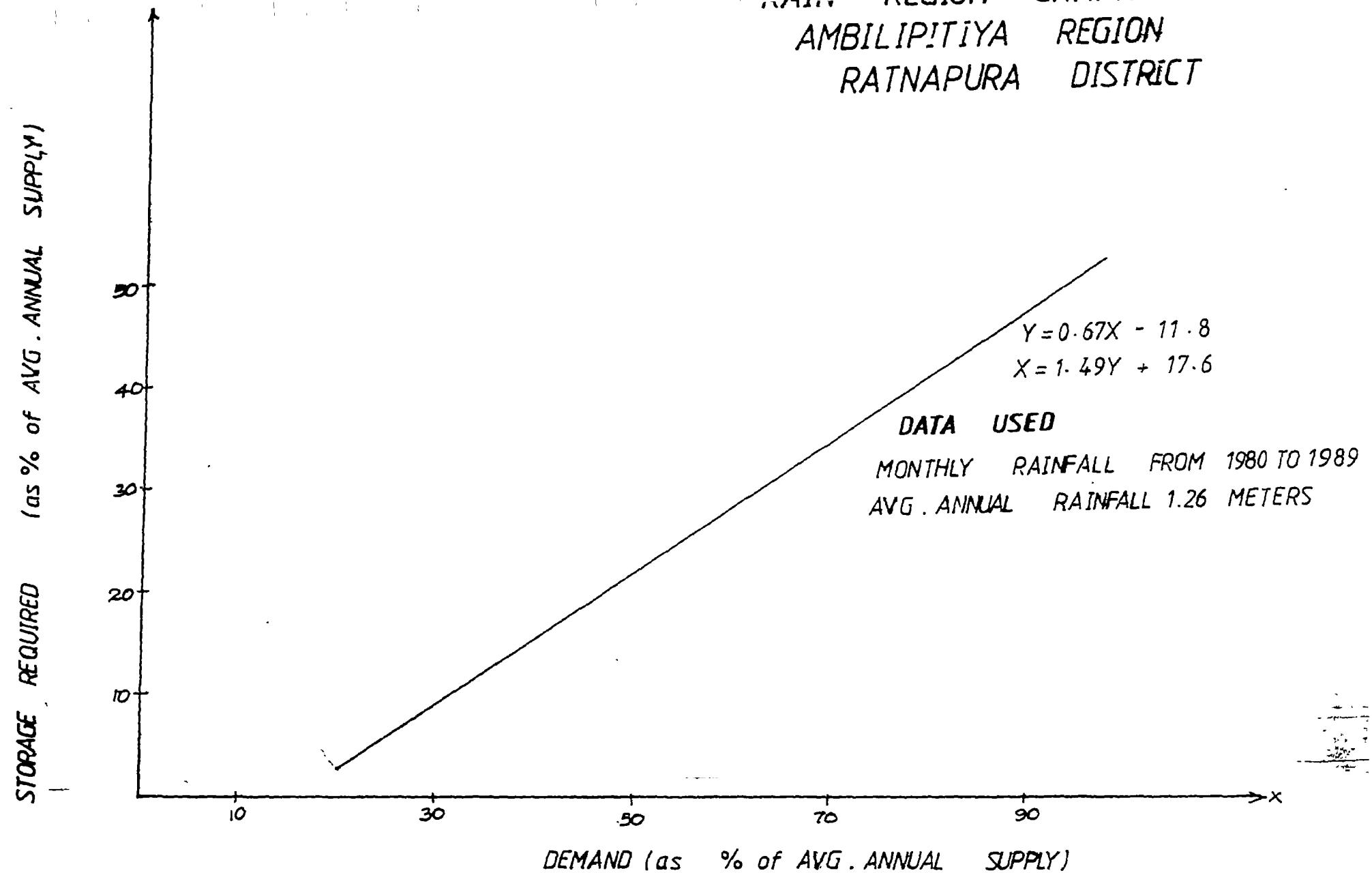
RAIN REGION GRAPH
RATNAPURA REGION
RATNAPURA DISTRICT



GRAPH - D
ANNEX - 8



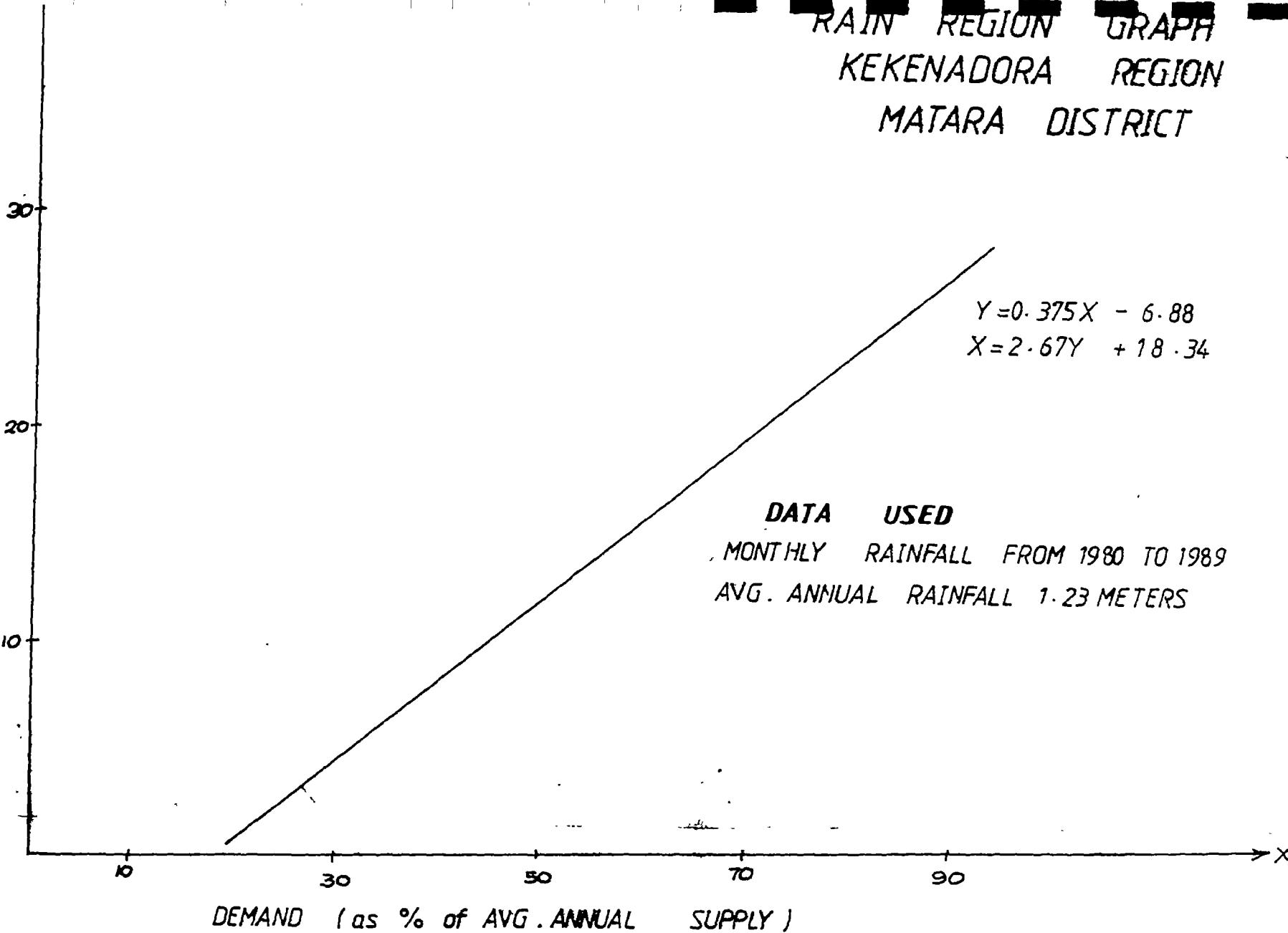
AMBILIPITIYA REGION
RATNAPURA DISTRICT



GRAPH - E
ANNEX - 8

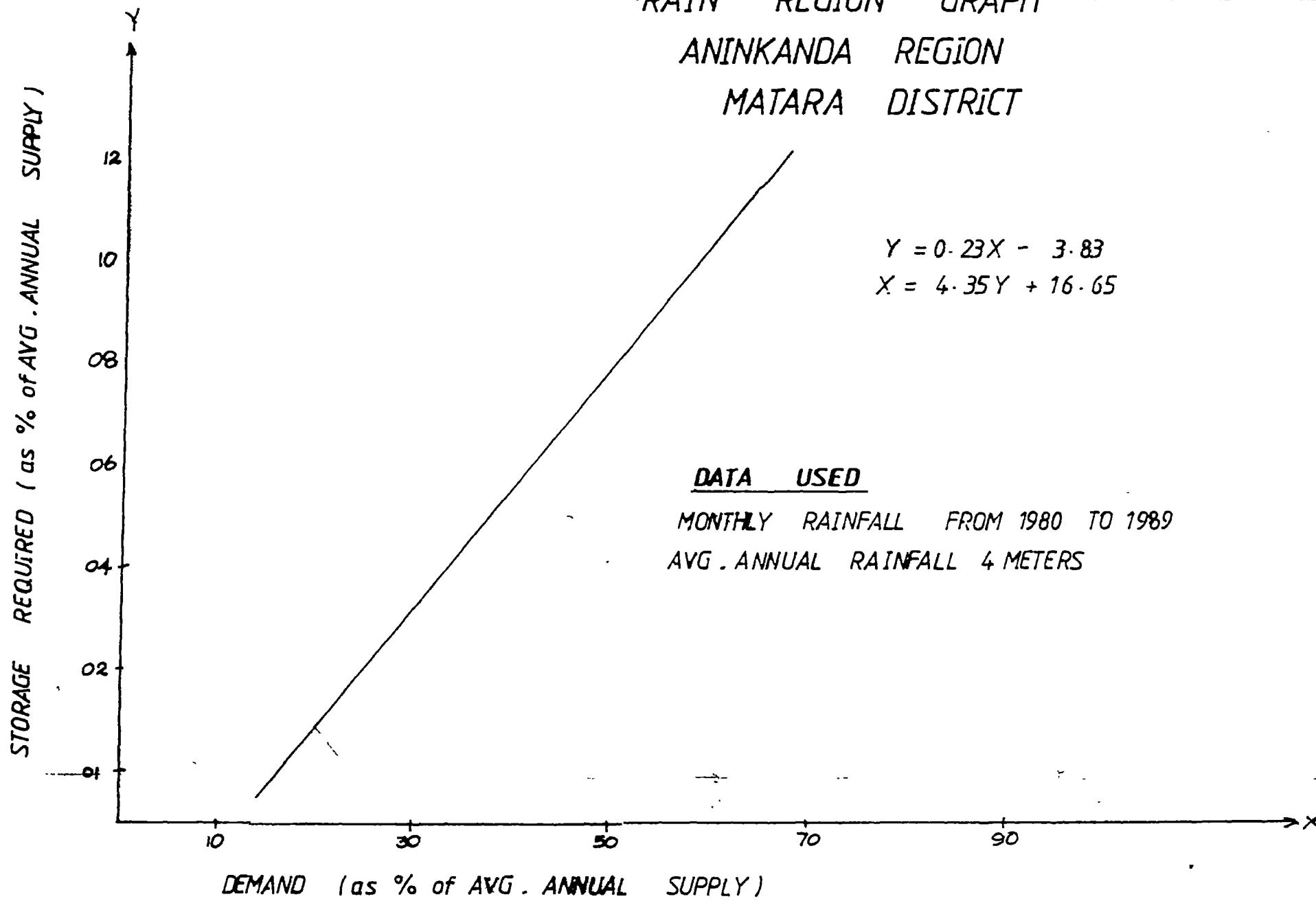


STORAGE REQUIRED (as % of AVG. ANNUAL SUPPLY)



GRAPH - F
ANNEX - 8

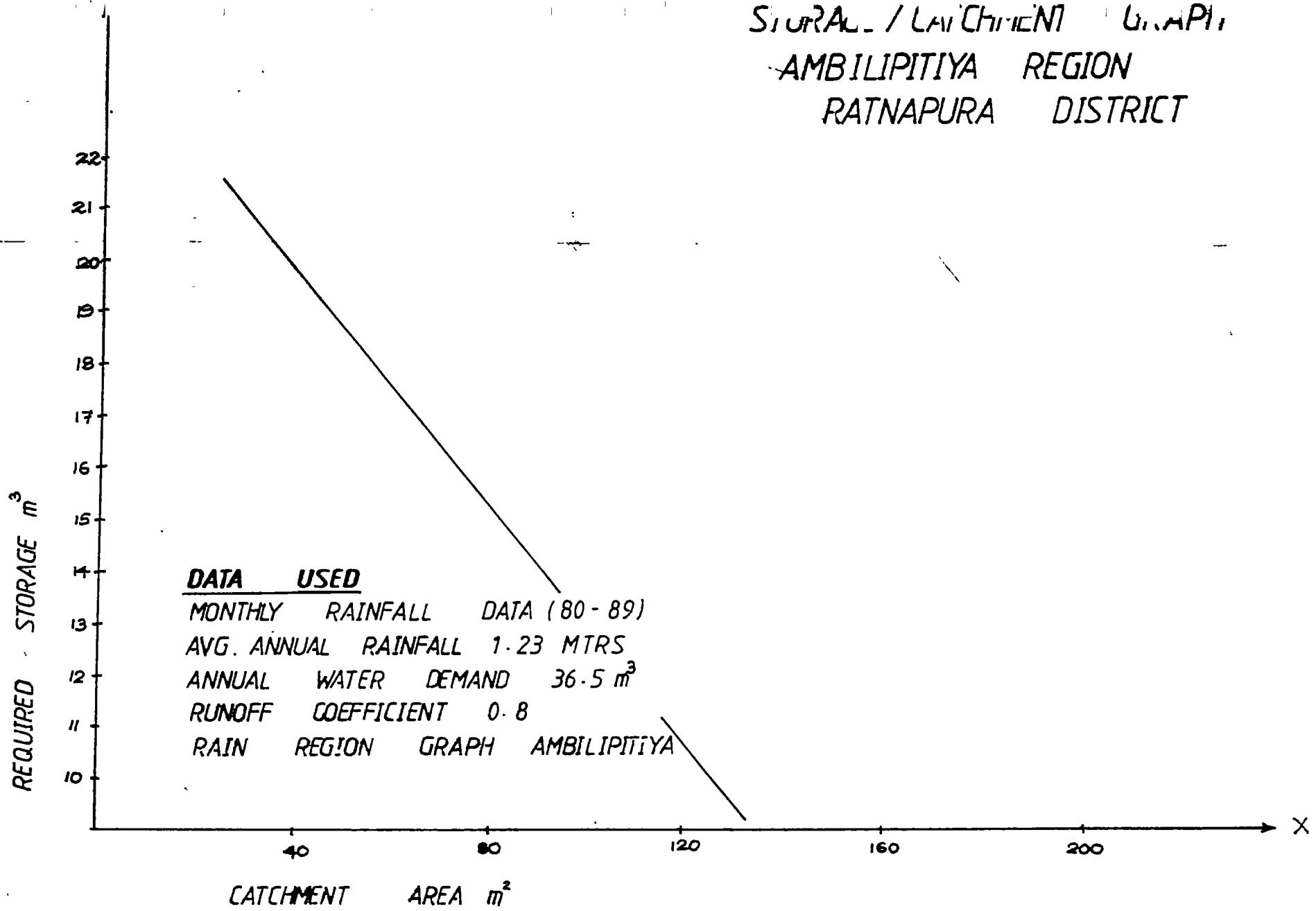




GRAPH - G
ANNEX - 8

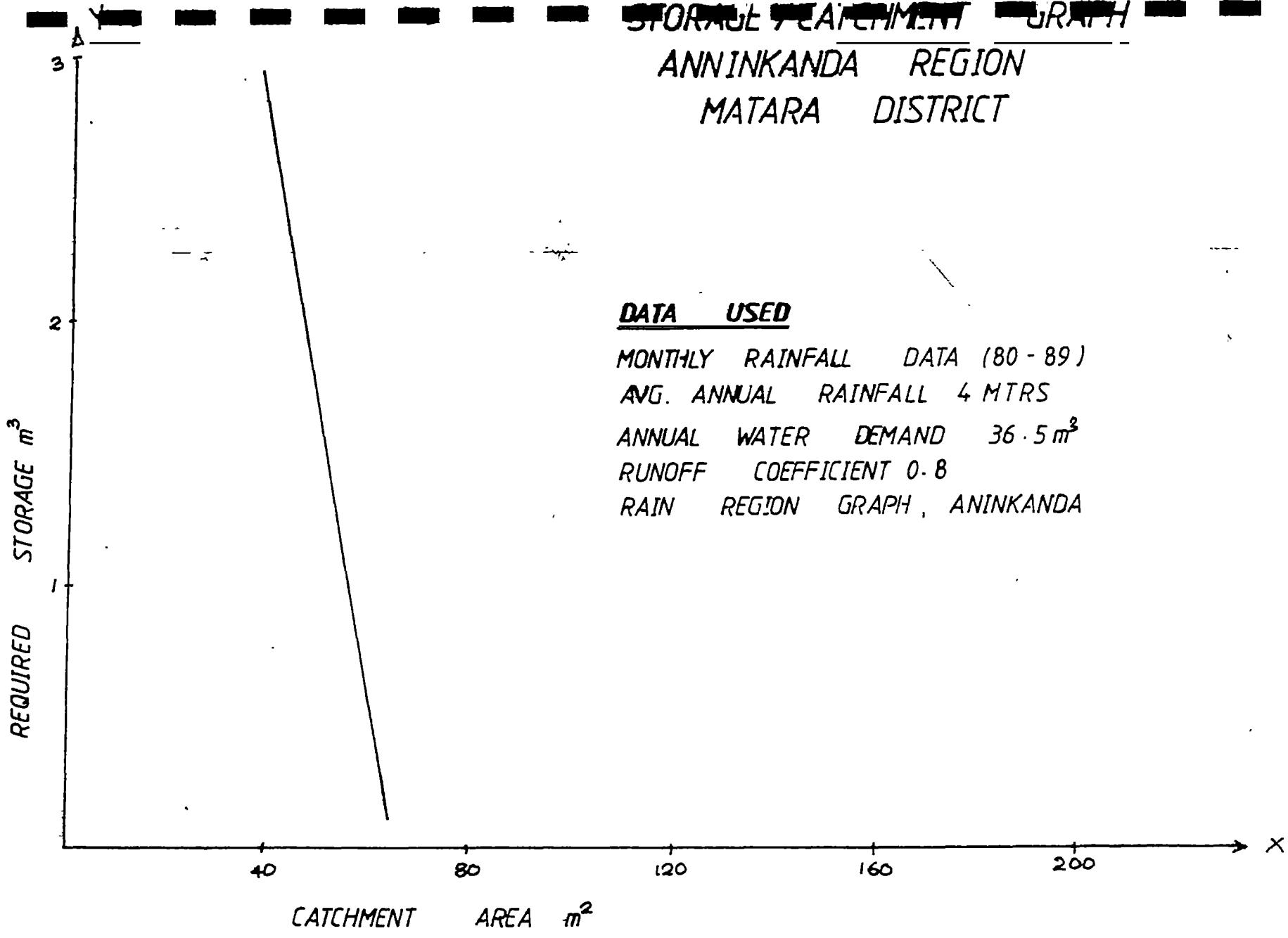


SURFACE / LAUNCHMENT GRAPH,
AMBILIPITIYA REGION
RATNAPURA DISTRICT



GRAPH - 0
ANNEX - 9

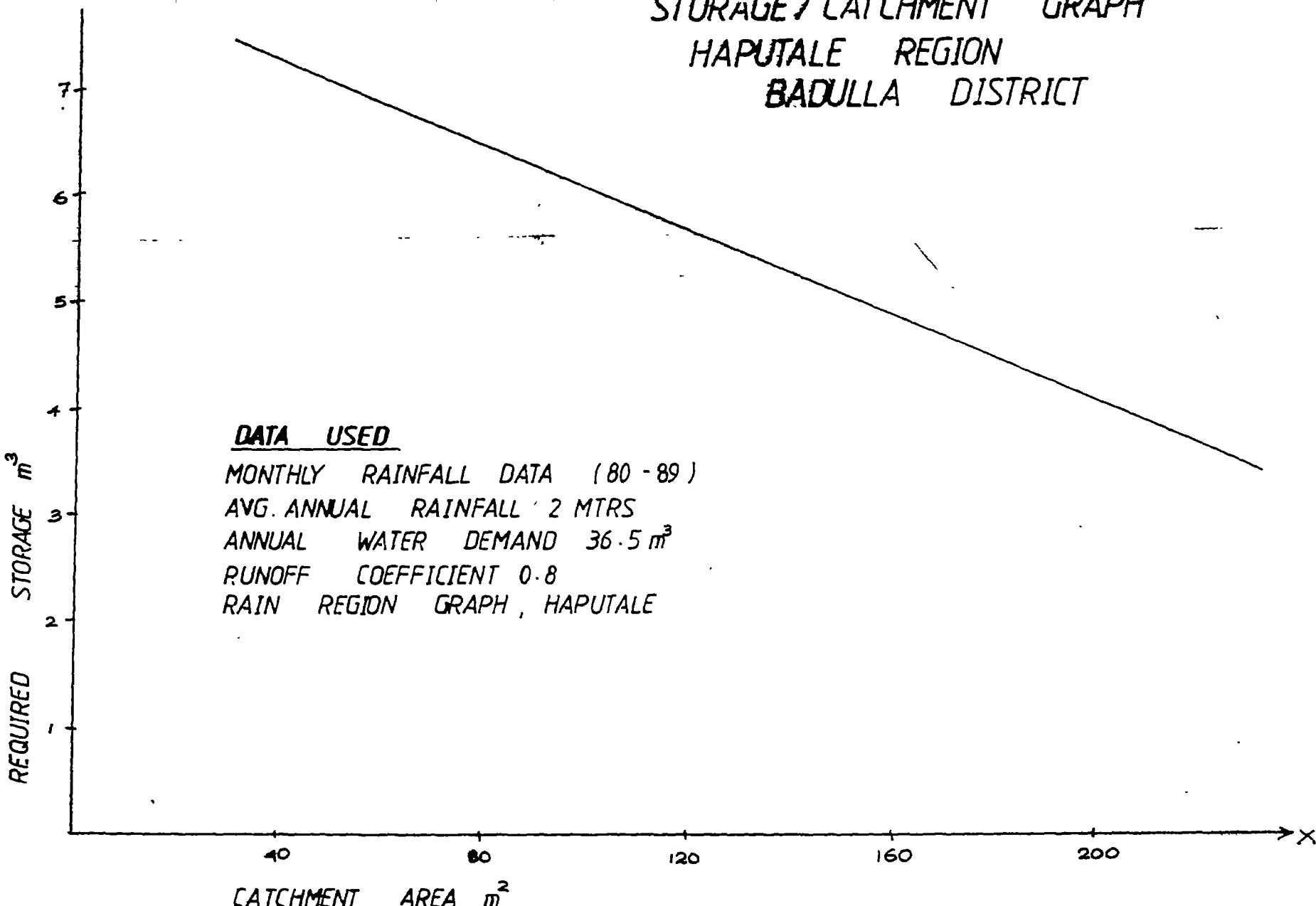




GRAPH - P
ANNEX - 9



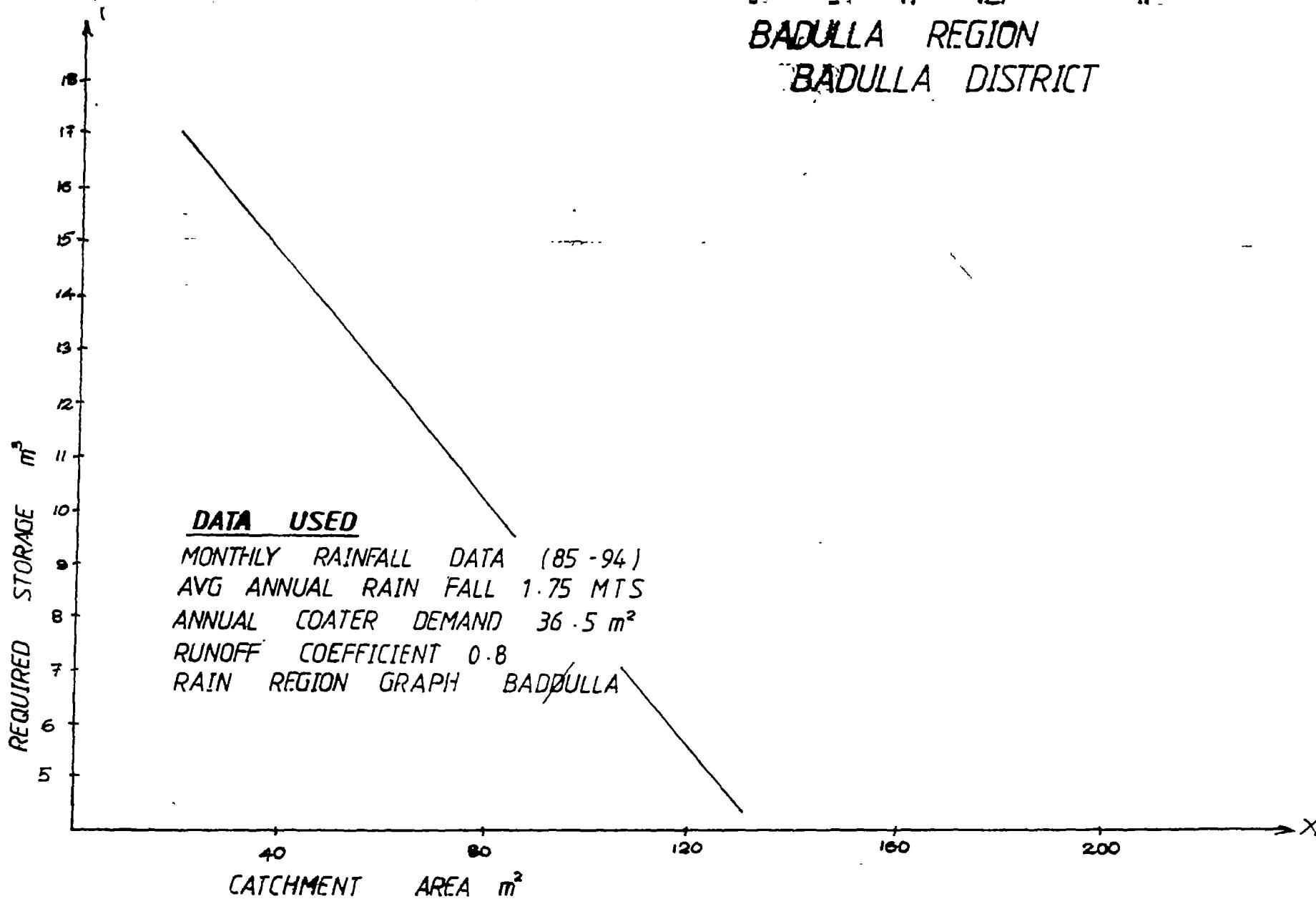
STORAGE / CATCHMENT GRAPH
HAPUTALE REGION
BADULLA DISTRICT



GRAPH - Q
ANNEX - 9



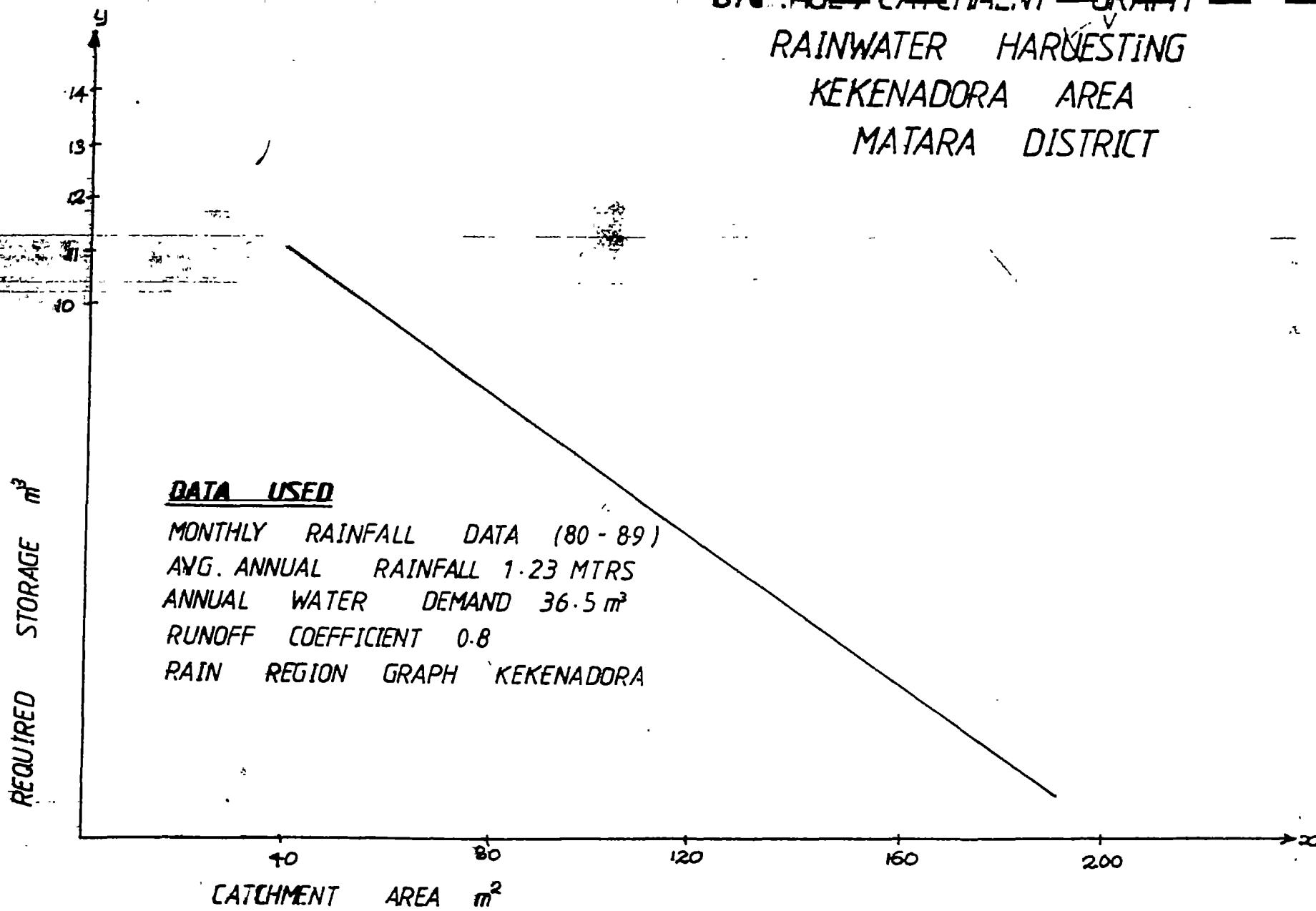
BADULLA REGION
BADULLA DISTRICT



GRAPH - R
ANNEX - 9



~~DATA CATCHMENT GRAPH~~
RAINWATER HARVESTING
KEKENADORA AREA
MATARA DISTRICT



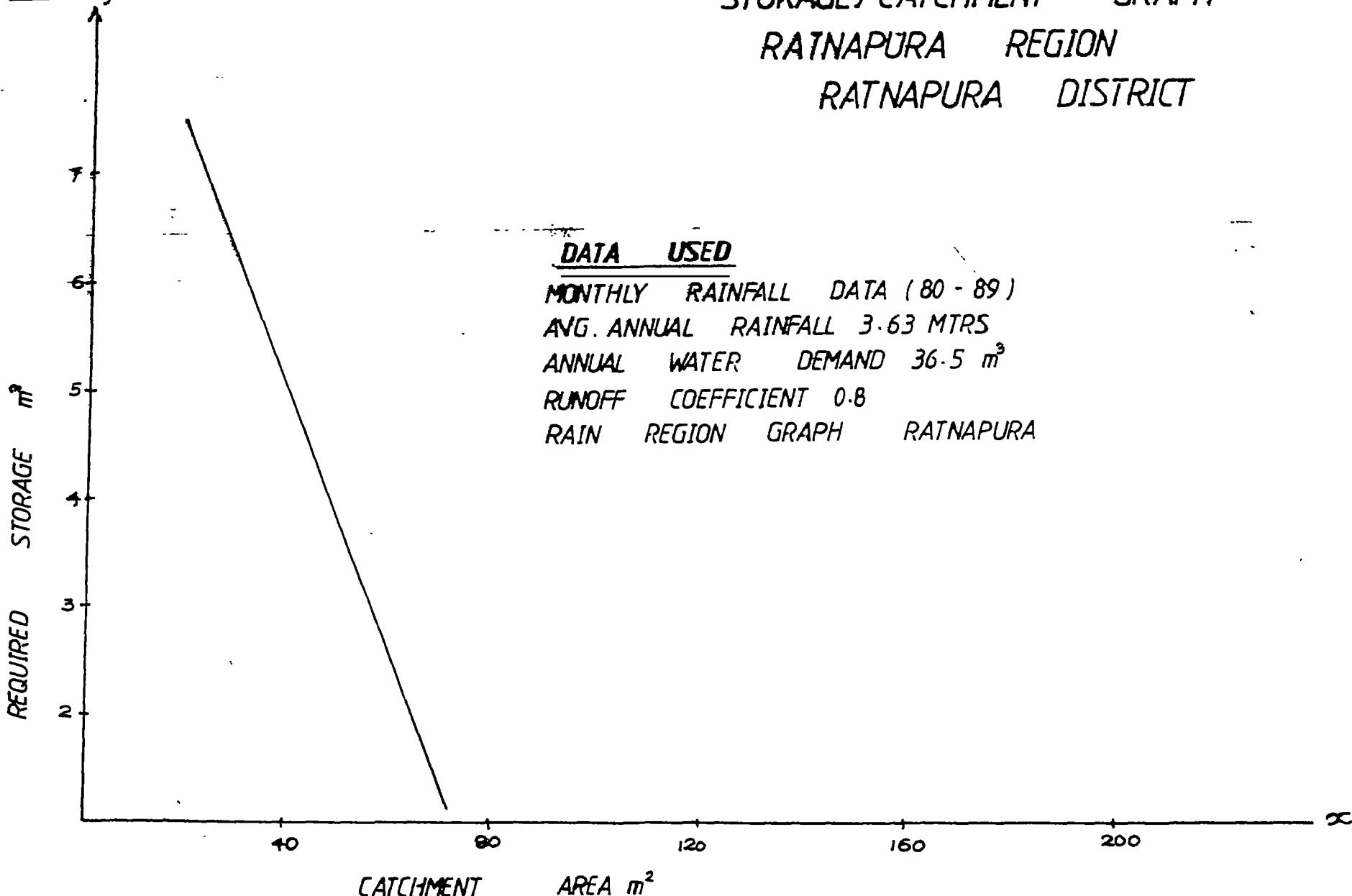
GRAPH - 5
ANNEX - 9



STORAGE / CATCHMENT GRAPH

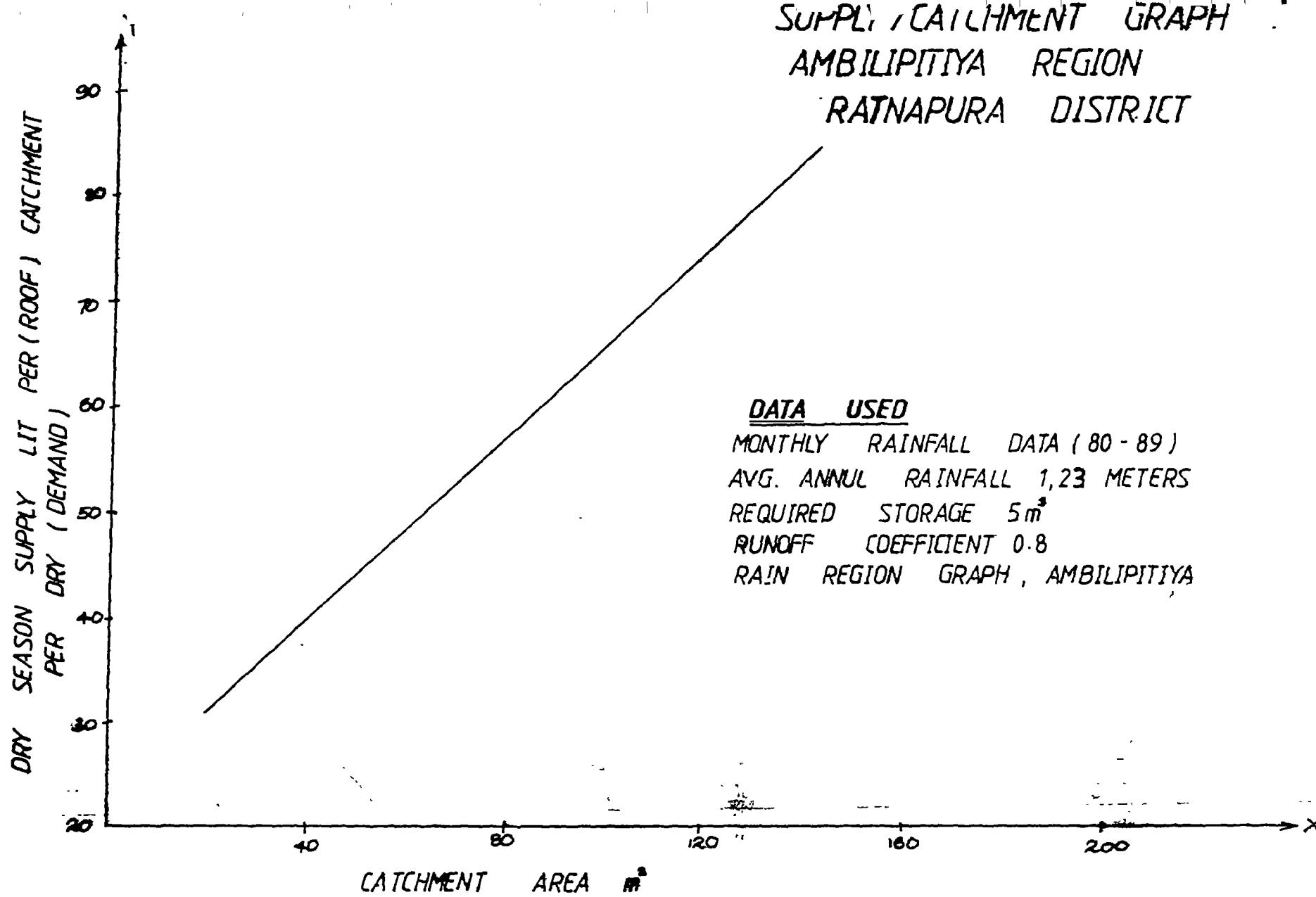
RATNAPURA REGION

RATNAPURA DISTRICT

GRAPH - T
ANNEX - 9



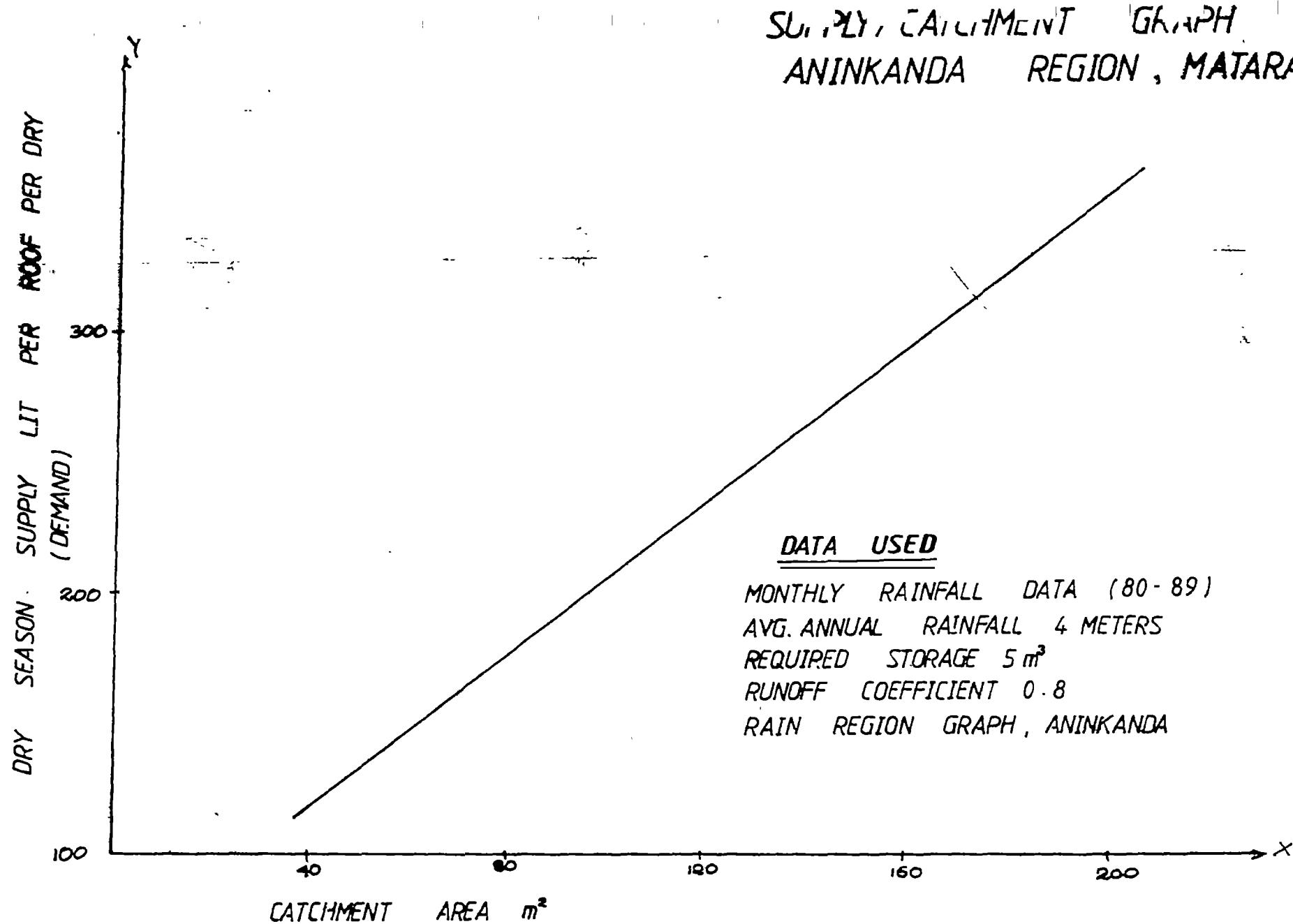
SUMPLI / CATCHMENT GRAPH
AMBILIPITIYA REGION
RATNAPURA DISTRICT



GRAPH - U
ANNEX - 10



SUPPLY, CATCHMENT GRAPH
ANINKANDA REGION, MATARA



GRAPH - V
ANNEX - 10



SUPPLY / CATCHMENT GRAPH

HAPUTALE REGION
BADDULLA DISTRICT

DRY SEASON SUPPLY LIT PER ROOF PER DAY
(DEMAND)

110
100
90
80
70
60

10

80

120

160

200

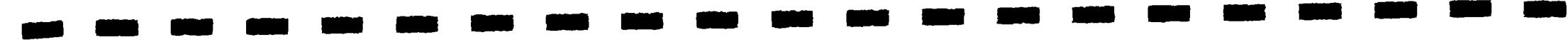
$\rightarrow x$

CATCHMENT AREA m^2

DATA USED

MONTHLY RAINFALL DATA (80 - 89)
AVG. ANNUAL RAINFALL 2 METERS
REQUIRED STORAGE $5m^3$
RUNOFF COEFFICIENT 0.8
RAIN REGION GRAPH, HAPUTALE

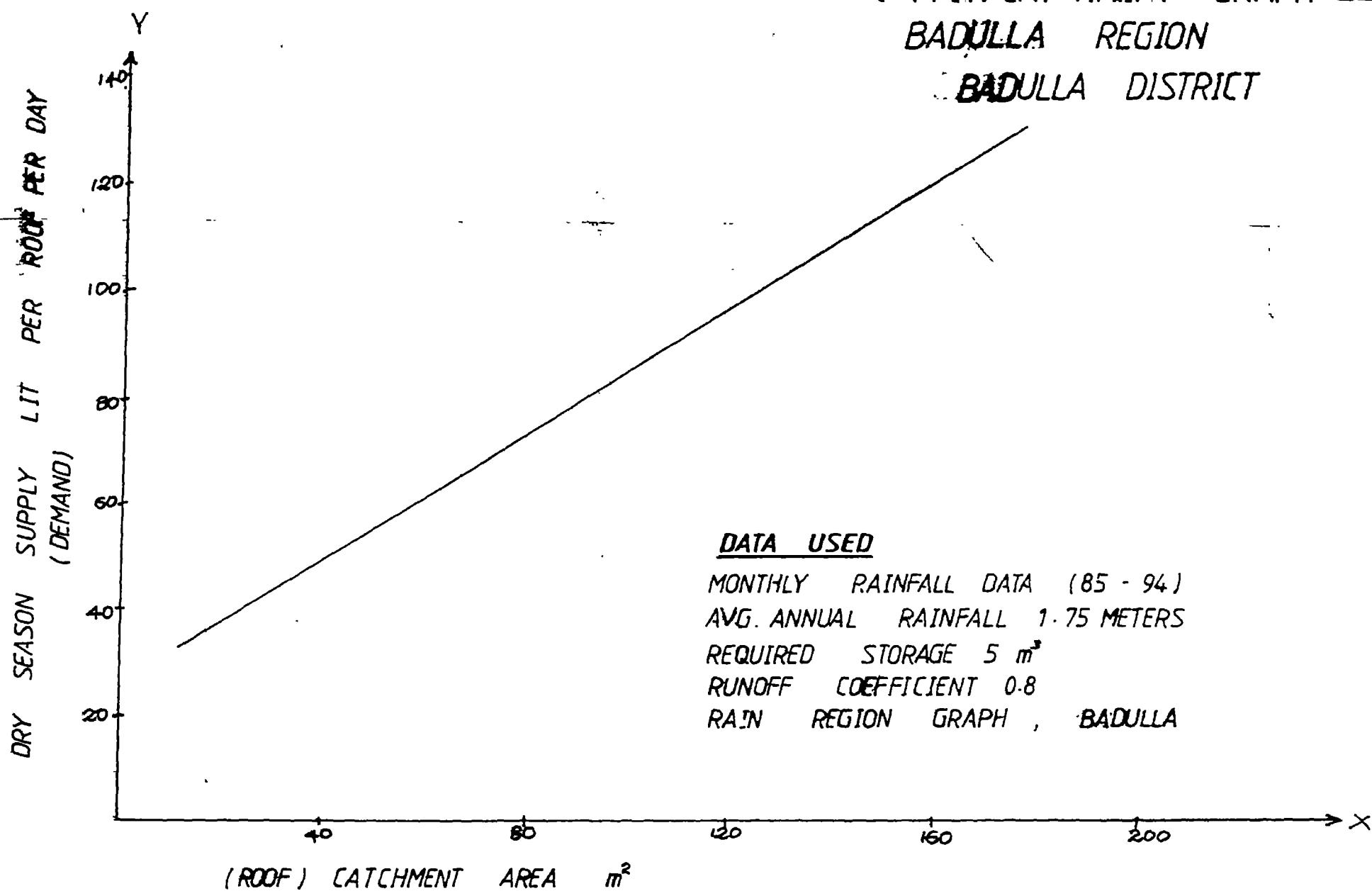
GRAPH - W
ANNEX - 10



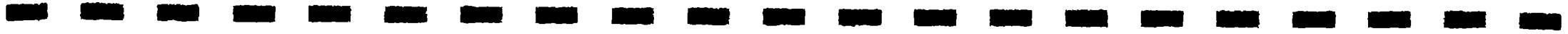
M.L.A. HANNAI GRAPH

BADULLA REGION

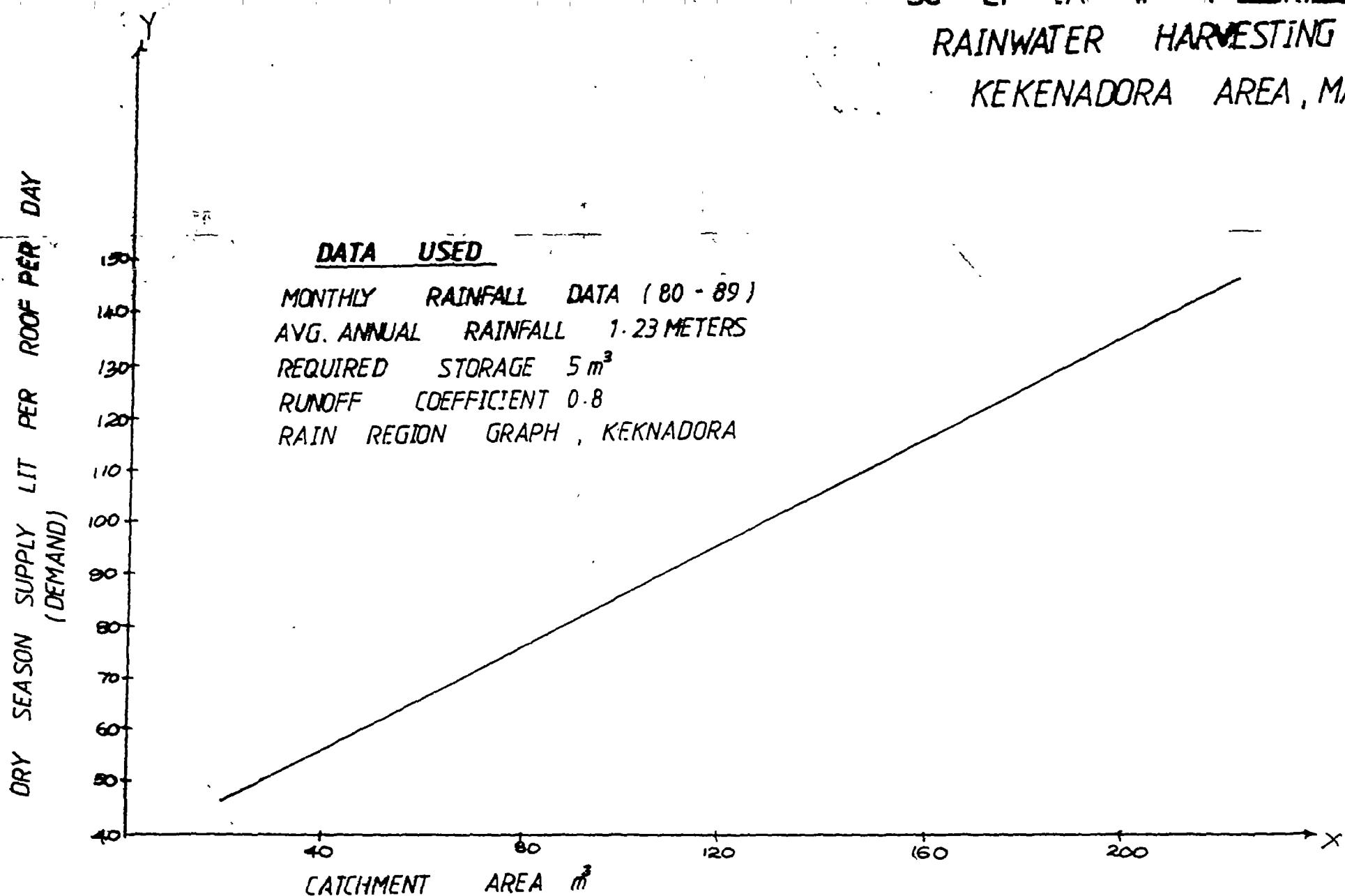
BADULLA DISTRICT



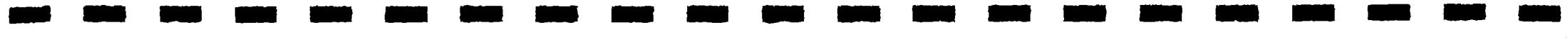
GRAPH - X
ANNEX - 10

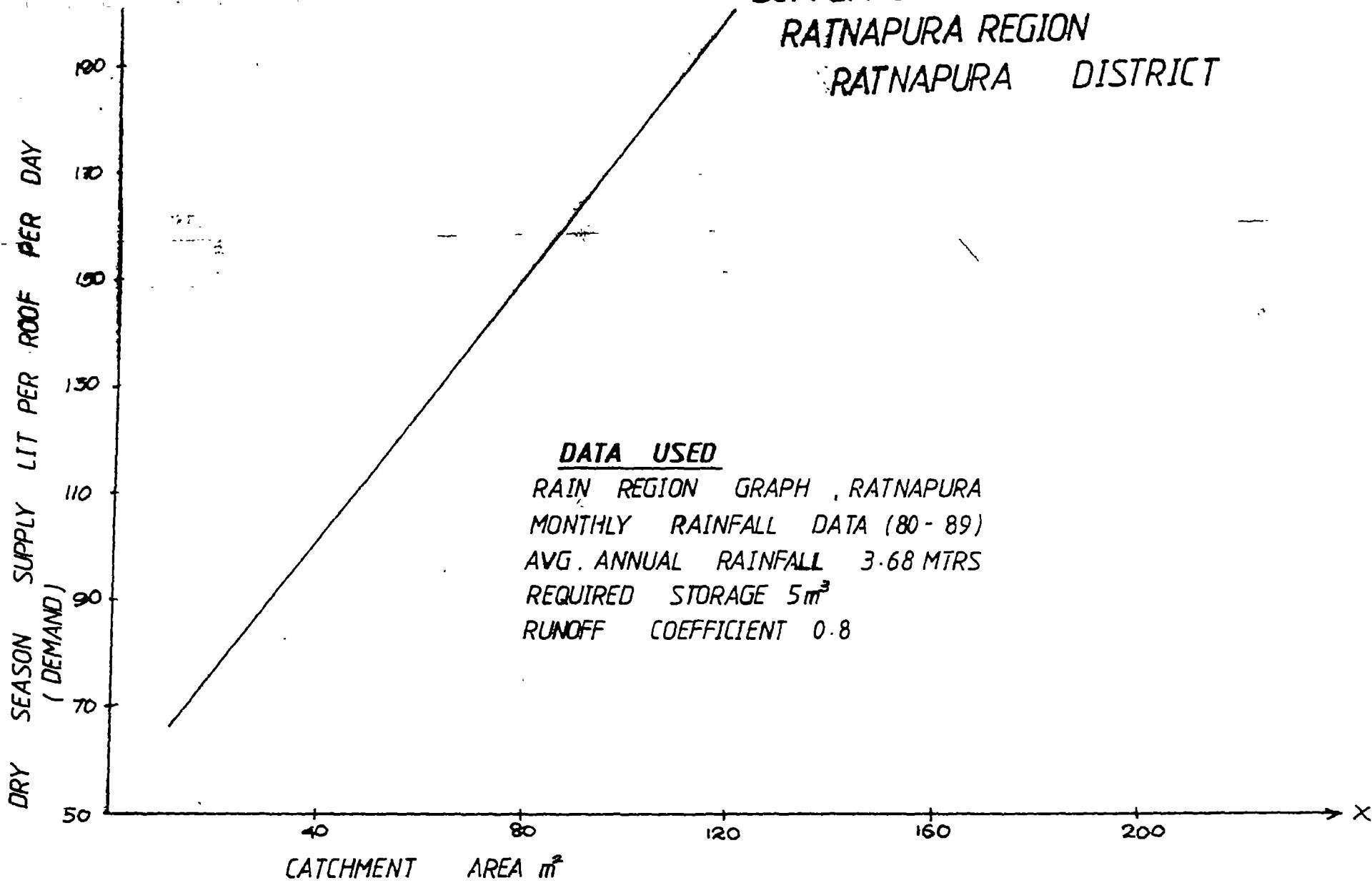


SU LI A # 1 ~~KR~~
RAINWATER HARVESTING
KEKENADORA AREA, MATAR



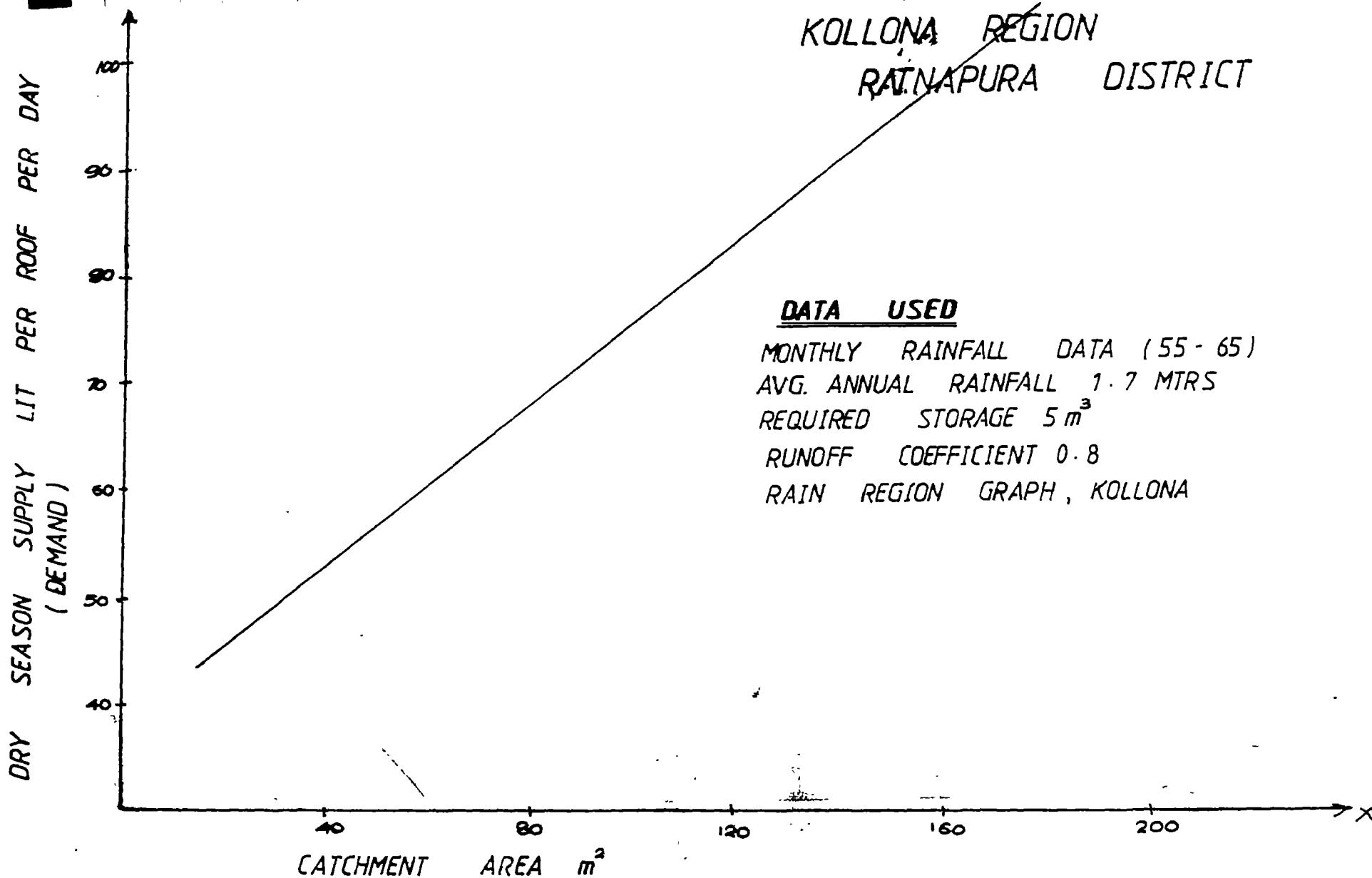
GRAPH - Y
ANNEX - 10





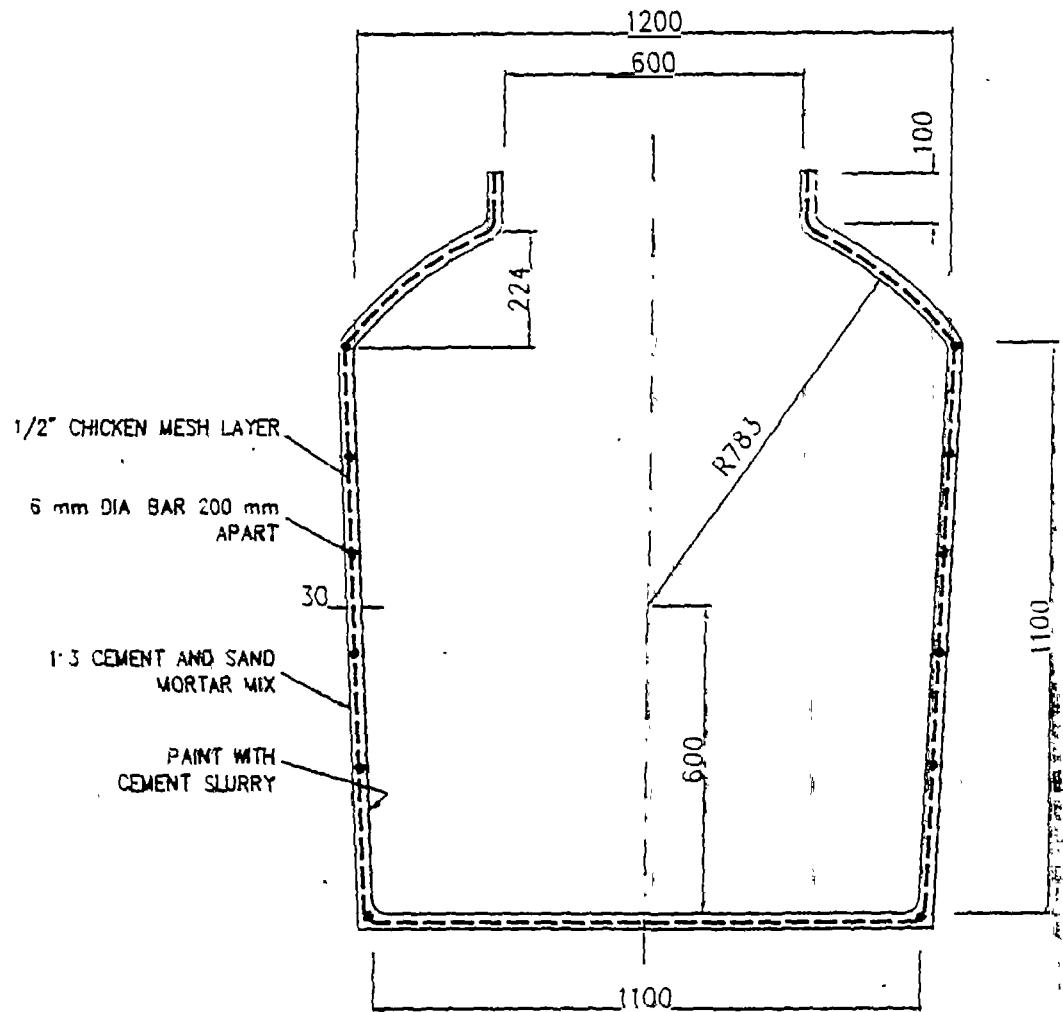
GRAPH - Z
 ANNEX - 10





GRAPH - N
ANNEX - 10





Ministry of Housing, Construction & Public Utilities	
Community Water Supply & Sanitation Project	
1.1 CLM CEMENT JAR	
Designed	KDH.
Drawn	MFA.R
Scale	1:15
Date	



RHIC NETWORK PRIORITY: Asbestos Roofing and Safety

by Dan Campbell, RHIC Manager

RHIC periodically receives requests for information and advice on the potential negative health impacts on drinking water harvested from roofs made from asbestos/cement (A/C) sheeting. Such roofing sheets are common in many countries and offer important advantages such as ease of local manufacture, durability, and relatively low prices. Because of the very limited information available on health issues of rainwater harvesting from asbestos roofing, RHIC invites readers to share any information you may have on this important topic. RHIC would like to learn of any policies or experiences in water consumption from A/C roofs from the RHIC network.

Some experts advocate that materials containing asbestos should never be used as roofing material because asbestos fibers can be loosened if roofing sheets are cut or damaged, causing the potential for human ingestion. Asbestos research has centered on human hazards due to ingestion through the lungs by breathing, and clearly demonstrated that this is hazardous to human health, causing cancer, gastro-intestinal tract and pulmonary fibrosis. Research is much more limited on human ingestion of asbestos through the alimentary system by drinking or eating. In fact, RHIC staff have not identified any viable information or research on the health consequences of human consumption of rainwater that contains asbestos fibers.

Asbestos is a generic name for a group of six naturally occurring hydrated polysilicate minerals (amosite, chrysotile, tremolite, actinolite, anthophyllite, and crocidolite). Asbestos/cement pipe contains an average of 170g of asbestos per kg (80% chrysotile and 20% crocidolite). These minerals separate into microscopic fibers that are heat resistant, flexible, durable, and virtually indestructible in most uses. Asbestos fibers are very stable in the environment, do not evaporate into air or dissolve in water, and do not break down over time.

Due to these stable characteristics, asbestos fibers have been used in a wide range of products such as water and sewage pipes, roofing sheets, electrical insulators, and heating insulation. Asbestos is commonly found in most domestic water supplies. Typical asbestos concentrations in rivers and lakes are considered to be about 1 million fibers per liter.

• • • •

Slow sand and gravel filters can remove up to 90% of asbestos fibers and other particulate matter and can be designed to serve small communities as well as individual families.

For information on filter design contact RHIC.

• • • •

Asbestos levels also depend upon neighboring industrial sources. In Canada, the asbestos content of untreated water from the Ottawa River has been reported to be 9.5 million fibers per liter. Based on surveys in Canada, it was found that about 5 percent of the Canadian public consume water with asbestos concentration exceeding 10 million fibers per liter and about 0.6 percent consume water with concentrations exceeding 100 million fibers per liter. Levels range up to 2000 million fibers per liter in some asbestos mining communities.

According to the World Health Organization (WHO), 1984 guidelines on drinking water quality, the most effective method for removal involves chemical coagulation with iron salts and polyelectrolytes followed by filtration. Ordinary sand filtration removes about 90 percent of the individual asbestos fibers from water supplies.

One of the few studies available on rainwater quality from asbestos roofing was conducted in Thailand in 1989. This study showed that E. coli. levels were considerably higher in runoff from A/C roofs than from galvanized iron. Some research indicates this is because sunlight is more effective in killing bacteria on metal surfaces than on A/C surfaces.

In addition to the above research, the RHIC document collection includes records of one rainwater harvesting project that was influenced by the use of A/C roofing. In the late 1980's, the U.S. Agency for International Development in Honduras decided not to include rainwater catchments on rural schools because the Ministry of Education insisted on using locally manufactured A/C roofing for reasons of cost savings and job creation by using local products.

In the U.S., a great deal of research has been conducted by the Environmental Protection Agency (EPA) and other organizations on the health impacts of consuming water from asbestos-cement pipes. On July 12, 1989, under the US Toxic Substances Control Act (TSCA), the EPA banned most asbestos-containing products, including A/C pipe. A/C pipe, however, was included in the ban because of the risk posed by exposure to *airborne* asbestos during A/C pipe manufacture, transport and installation. The EPA concluded that consumption of drinking water transported by A/C pipelines *posed no significant health risk because of the pipe material* and that existing A/C pipelines did not need to be removed because of the ban.

The current EPA drinking water standard for asbestos, which became effective in July 1992, is set at 7 million fibers/liter for fibers longer than 10mm. The 1984 WHO guidelines do not contain a guideline for asbestos in water supplies. WHO directives state that:

continued on page 12



RHIC NETWORK NEWS

- Dr. Al-Homoud is looking for information and experts on the design and construction of ponds and small desert dams which can be used for water harvesting in the desert. His address is: Dr. Azm S. Al-Homoud, Assistant Professor, Civil Engineering Dept., Jordan University of Science & Technology, PO Box 3030, Irbid, Jordan, Phone: 295111, FAX: 295123.
- Mr. Nissen-Petersen has recently left Botswana for Namibia to work for 6 months on a UNICEF water tank and well program. He can be reached at: Erik Nissen-Petersen, ASAL Consultants Ltd., PO Box 867, Kitui, Kenya, Phone: 0141-22706 & 22123, FAX: 0141-22571 & 2-740524.
- In South Africa, a local non-governmental organization known as SAWIC maintains a bibliographic database of nearly 200,000 references and is interested in receiving research and project reports from other organizations involved in rainwater harvesting. The Centre publishes 2 journals, entitled *WATER SA* and the *SA Water Bulletin*, which are available on request. For further information, contact: Angela Rethman, Project Manager, South African Water Information Centre (SAWIC), PO Box 395, Pretoria 0001, South Africa, Phone: (012) 841-2048, FAX: (012) 86-2869.
- Brian Skinner is seeking information on wire-reinforced cement mortar tanks or jars that have been well-tried under field conditions. This includes plain wire or barbed wire reinforced containers as well as those using ferrocement. He also is seeking construction details of unreinforced mortar jars. Please contact him as soon as possible if you have information. Brian Skinner, WEDC, Loughborough University of Technology, Leicestershire, LE11 3TU, England, Phone: (44) 509-222392, FAX: (44) 509-211079.
- Alan Fewkes is developing a microcomputer software program for sizing rainwater catchment systems and he is keenly interested in relevant information and contacts with others who may also be interested. Alan Fewkes, Faculty of Environmental Studies, Nottingham Polytechnic, Burton Street, Nottingham NG1 4BU, United Kingdom, Phone: (0602) 418418, FAX: (0602) 484266
- Todd Boulanger seeks information on agencies that fund community workshops on rainwater catchments, water quality, and environmental monitoring. He is also interested in reports and data on the lead concentrations of different types of building materials. If you can assist, contact Todd at the following address: Todd Boulanger, Water Resources Research Center, University of Hawaii at Manoa, Holmes Hall 283, 2540 Dole Street, Honolulu, Hawaii 96822, Phone: (808) 956-7381, FAX: (808) 956-6870
- The International Association for Environmental Hydrology (IAEH) is new association created to encourage effective communication across all countries and between all disciplines that relate to water and the environment. It promotes links between the scientific community and practicing environmental hydrologists and water professionals. The Association publishes the *Journal of Environmental Hydrology* and the *Environmental Hydrology Report* which are both available at no cost to association members. Membership fees are \$96 per year for non-students. For further information, contact: Roger Peebles, IAEH, PO Box 1088, Alexandria, Virginia 22313, USA, Phone: (703) 683-9768, FAX: (703) 683-6137.

Network Priority, continued from page 7

"the health hazards associated with occupational exposure to airborne asbestos are well documented. The harmful effects, however, of swallowed asbestos on human health have not been determined. Studies in progress should permit a more complete evaluation of any hazard resulting from the swallowing of asbestos, but available data are, at present, insufficient to determine whether a guideline value is needed. The hypothesis that ingested asbestos fibers cause cancer cannot be ruled out at the present time."

With such uncertainty about the use of asbestos cement roofing materials and water pipes and the potential health risks, it is especially important that the results of diverse field experience and research become available for analysis. Please assist in this issue by sharing with RHIC your experiences and information on this topic. ○



WATER AND SANITATION FOR HEALTH PROJECT

For additional information about activities and reports highlighted in this issue, contact:

WASH Operations Center
1611 North Kent Street, Room 1001
Arlington, Virginia 22209 USA

Water and Sanitation for Health Project, Contract No. DPE 5973-Z-00-8081-00, Project No. 836-1249. Sponsored by the Office of Health, Bureau for Research and Development, U.S. Agency for International Development, Washington, DC 20523.

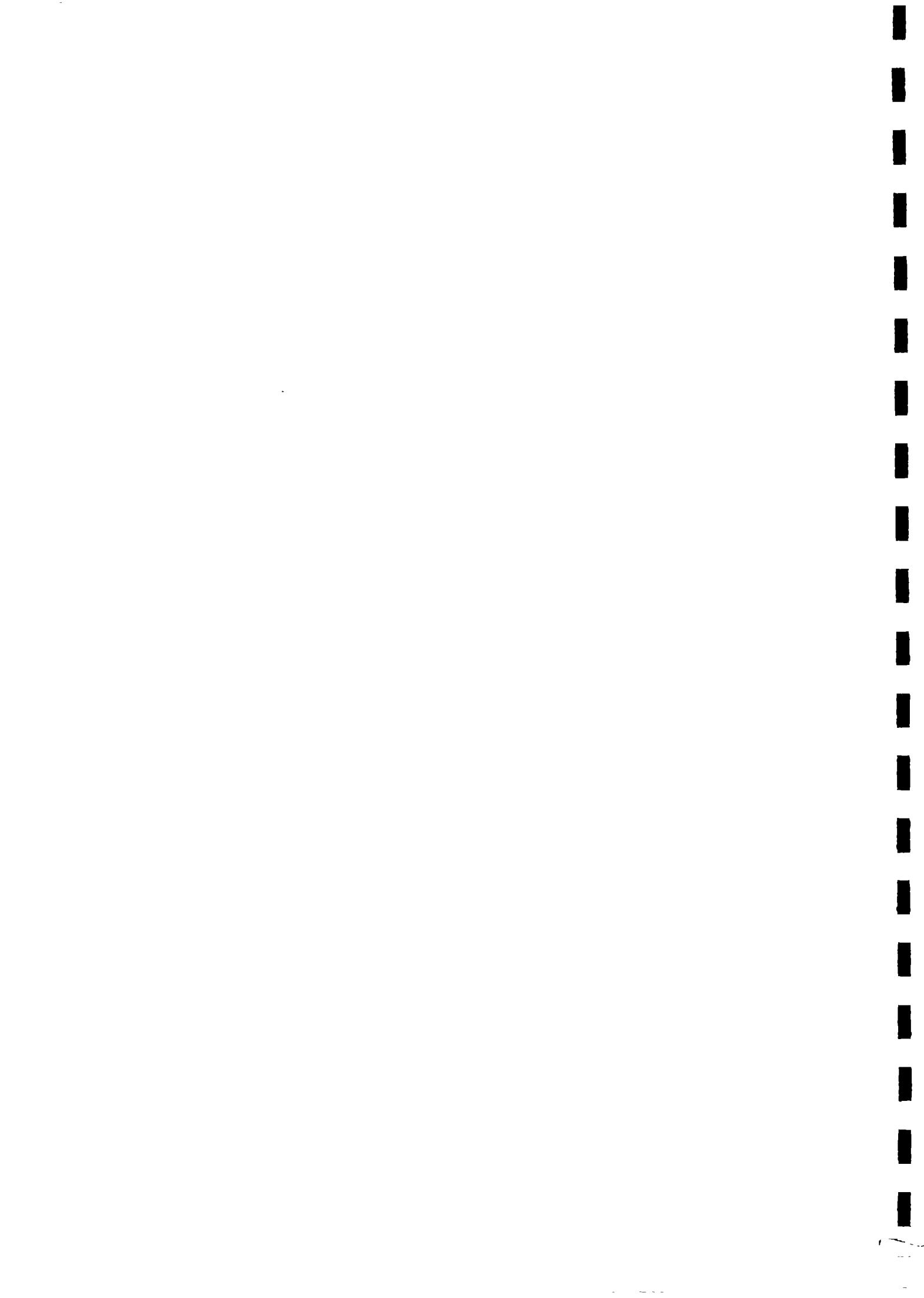


Cement Jar 1.1 M^3

Trial Tank build at NERD Centre
Ja-Ela, May 95

Description	Actuals used in the trial				Estimate Possible to do with		Householder Cost	CWSSP Cost
	Unit	Unit Cost	Qty	Cost	Qty	Cost		
Cement	Bag	265	4	1060	2.5	663		663
Sand	ft^3	4	10	40	10	40		40
1/2" Chicken Mesh	ft^2	4	80	320	80	320		320
6"m Rods	length	25	9	225	3	75		75
				1645				
Skill Labour	HR	22	24	528	8	176		176
Unskill Labour	HR	12.5	24	300	48	600	600	
				828				
Welding				200		NIL		
					2673	1874	600	1274
							HH	CWSSP
							32%	68%
Cost per Liter				2.43		1.87	.55	1.16

CONCLUSION: Cost is above CWSSP criteria, of 1.08 per liter maximum cost per liter can be brought down by building Jars of larger capacity (eg. 1.5 M^3) and more



**5, 8 & 10M³ BRICK DOME TANKS
QUANTITIES AND COSTS (1995)**

VOLUME	FLOOR	WALL	DOME	1:3 PLASTER 1:2			QTY	UNIT COST	COST	REMARK
				COAT I	NEAT CEMENT	COAT II				
5M³ H 4' D 7'6"	Area (ft ²)	53	99	54	260	210	210			
		Cement Bag	2	1.5	1.6	1.6	0.4	1.5	8.6	265 2279 – Transport not included
		Brick No	–	560	190	–	–	–	750 1.5 1125	– Dome volume not taken
		Sand ft ³	5	10	5	7	–	6	33 3.5 116	– Dome thickness 2" brick
		Metal 3/4" ft ³	6	–	–	–	3	9	18 162	– Transport not included
		Mason HR	2	4	6	6	4	6	28 22 616	– Dome thickness 2" brick
		Labour HR	6	24	18	18	12	18	96 12.5 1200	Cost Rs. 1.10/Lit 5498
8M³ H 4' D 9'6"	Area (ft ²)	81	124	85	375	286	286			
		Cement Bag	3	2	2.5	2.3	0.5	2	12.3 265 3259	
		Brick No	–	700	800	–	–	–	1000 1.5 1500	300 450
		Sand ft ³	8	13	8	10	–	8.2	47.2 3.5 165	
		Metal 3/4" ft ³	9	–	–	–	4	–	13 18 234	– Dome thickness 4" Brick
		Mason HR	3	5	9	9	5	8	39 22 858	
		Labour HR	9	30	28	26	16	24	133 12.5 1663	Cost Rs. 1.02/Lit 8129
10M³ H 5' D 9'6"	Area (ft ²)	81	160	85	405	316	316			
		Cement Bag	3	2.4	2.5	2.5	0.7	2.5	13.6 265 3604	– Dome thickness 4" Brick
		Brick No	–	905	600	–	–	–	1505 1.5 2258	
		Sand ft ³	8	16	8	11	–	10	53 3.5 186	
		Metal 3/4" ft ³	9	–	–	–	4	–	13 18 234	
		Mason HR	3	6	9	9	6.5	10	44 22 968	
		Labour HR	9	39	28	28	20	30	154 12.5 1925	Cost Rs. 0.92/Lit 9175



APPENDIX I

RAINWATER HARVESTING SYSTEM COST ANALYSIS. SYSTEM CONSISTS OF 5M³ TANK & 60M² CATCHMENT

(1995) Rs.

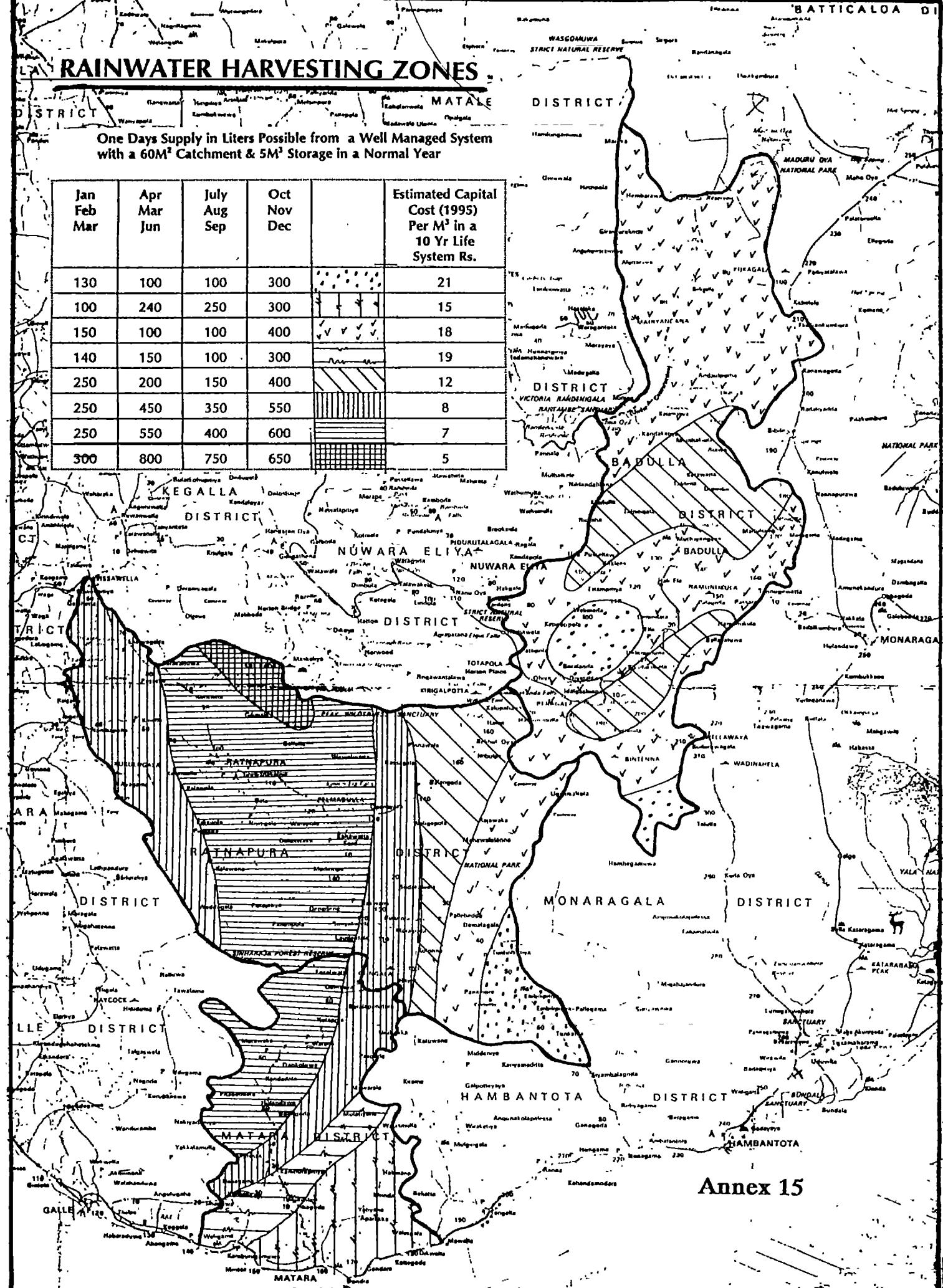
	Ferro Cement Tank CWSSP Cost	Ferro Cement Tank HH Cost	Brick Dome Tank CWSSP Cost	Brick Dome Tank HH Cost	Material for Home Made Pump	Material for low cost Gutter for 60M ² RF	Material for Standard Gutter for 60M ² RF	Low Cost Ground Catchment 30M ²	Labour for Low Cost Gutter	Labour for Standard Gutters	Labour for The Pump	Transport	Total Costs
	5500	1400	4300	1300 + 1000	450	850	2250	1550	200	400	100	500	
I	5500						2250			400			8150
II	5500					850			200				6550
III	5500						2250			400	500		8650
IV		4300			450		2250			400	100		7500
V		4300			450		850		200		100		5900
VI		4300			450		850		200		100	500	6400
VII		4300			450						100		4850



RAINFALL HARVESTING ZONES

One Days Supply in Liters Possible from a Well Managed System
with a 60M² Catchment & 5M³ Storage in a Normal Year

Jan Feb Mar	Apr May Jun	July Aug Sep	Oct Nov Dec		Estimated Capital Cost (1995) Per M ³ in a 10 Yr Life System Rs.
130	100	100	300		21
100	240	250	300		15
150	100	100	400	V V V V V	18
140	150	100	300	W W W W W	19
250	200	150	400	H H H H H	12
250	450	350	550	G G G G G	8
250	550	400	600	S S S S S	7
300	800	750	650	██████████	5



Annex 15

